

# NS-Resultate Mitchell-Turnier Samstag - Mensa, Pfäffikon - 17.09.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	N 1SA +1	K2	120	62	2	3	104 O 4C +1	TD	-450	25	3	5	108 W 1SA -1	K4	100	0
2	1	101	O 4C =	TD	-420	56	3	3	104 W 1SA -2	C2	200	81	4	5	107 W 2T +3	CK	-150	0
3	1	101	N 1SA +1	P10	120	25	7	3	103 S 2P =	CA	110	88	5	5	107 W 3K +2	CA	-150	44
4	1	110	N 3P +1	T5	170	62	8	3	103 O 3SA +4	P9	-520	25	6	5	107 N 1SA -2	KB	-100	6
5	1	110	N 3C =	PA	140	88	9	3	103 N 4C +1	P10	450	69	7	5	106 W 2C =	KB	-110	19
6	1	110	N 1SA =	K6	90	56	10	3	102 W 1SA -2	C9	200	94	8	5	106 O 3SA +3	P9	-490	44
7	1	109	W 3C -1	PA	100	69	11	3	102 N 2C +2	PB	170	25	9	5	106 S 3C +1	P6	170	12
8	1	109	O 3SA +1	P9	-430	81	12	3	102 S 4P -1	KK	-100	25	13	5	105 S 1C +2	PA	140	69
9	1	109	N 3SA +2	P8	460	94	13	3	101 N 1P +2	T6	140	69	14	5	105 S 6SA -4	T5	-200	0
10	1	108	S 2C -2	P2	-200	0	14	3	101 S 6SA -1	T5	-50	50	15	5	105 N 3P -2	C7	-200	38
11	1	108	N 4P +1	K5	450	75	15	3	101 N 4P -3	KD	-300	6	16	5	104 S 2SA =	K2	120	31
12	1	108	S 4P +1	K7	650	69	16	3	110 N 3C =	PB	140	50	17	5	104 N 3SA +1	C6	430	44
13	1	107	O 2K -2	TA	200	100	17	3	110 S 3SA +2	C10	460	81	18	5	104 O 3T +1	P10	-130	44
14	1	107	S 3SA +2	T5	460	88	18	3	110 S 4P -2	TK	-200	19	19	5	103 N 2P +2	C2	170	12
15	1	107	N 2P =	C4	110	69	19	3	109 N 4P +1	C5	450	62	20	5	103 W 3SA -1	P8	100	44
16	1	105	S 2SA +1	T3	150	75	20	3	109 W 3SA -4	P8	400	100	21	5	103 N 2SA -1	CK	-100	44
17	1	105	S 5K =	CB	400	25	21	3	109 N 3SA -2	CK	-200	12	22	5	102 W 1SA +1	P7	-120	56
18	1	105	S 3P -1	TK	-100	75	22	3	107 W 1SA +1	P7	-120	56	23	5	102 W 4K -1	TB	100	12
19	1	104	N 4P =	T10	420	38	23	3	107 N 4P -1	TD	-100	0	24	5	102 N 2SA =	C8	120	25
20	1	104	W 3SA -1	PB	100	44	24	3	107 S 3P +1	T10	170	38	25	5	101 N 2SA -1	C4	-50	0
21	1	104	S 5K =	PK	600	69	25	3	106 S 2P =	T2	110	25	26	5	101 O 3K -1	C3	100	94
22	1	103	W 1SA +1	P7	-120	56	26	3	106 W 3SA +1	P10	-630	69	27	5	101 N 4C +1	PA	450	38
23	1	103	N 3P =	K4	140	25	27	3	106 O 3P X -4	C8	800	100	28	5	109 W 2SA -1	C10	50	31
24	1	103	S 4P =	T10	420	81	28	3	105 O 4P -1	KA	50	31	29	5	109 W 3K -1	C10	100	75
25	1	102	N 1SA +2	T6	150	94	29	3	105 S 3C -2	TK	-200	12	30	5	109 O 3SA -2	C10	100	100
26	1	102	O 3SA +2	C3	-660	25	30	3	105 N 3K -4	C2	-200	25	1	6	110 N 1SA +1	T2	120	62
27	1	102	N 4C +1	PA	450	38	1	4	106 N1SAX+2	C7	380	100	2	6	110 O 4C +2	TD	-480	0
4	2	102	N 2P +3	T5	200	75	2	4	106 O 5C -1	KA	50	100	3	6	110 N 2SA =	PD	120	25
5	2	102	N 2C -1	K10	-100	62	3	4	106 O 2P -2	T4	200	81	4	6	109 W 4T -1	PK	100	38
6	2	102	N 1SA +1	K9	120	88	4	4	105 S 5P -1	TA	-100	12	5	6	109 N 3C =	PA	140	88
7	2	101	W 2C -1	KB	100	69	5	4	105 W 3K +2	CA	-150	44	6	6	109 W 2C -2	PA	200	100
8	2	101	W 3SA +3	T5	-490	44	6	4	105 N 1SA =	K6	90	56	7	6	108 W 2C =	KB	-110	19
9	2	101	N 4C =	T7	420	31	10	4	104 O 2T =	CB	-90	38	8	6	108 O 6SA +1	P6	-1020	0
10	2	110	S 1SA -1	P2	-100	19	11	4	104 N 4P -1	C9	-50	12	9	6	108 S 4C =	P4	420	31
11	2	110	N 2P +3	T2	200	38	12	4	104 N 5T -1	CK	-100	25	10	6	107 W 1SA -2	CB	200	94
12	2	110	S 4SA +1	KK	660	88	13	4	103 O 2K =	CK	-90	6	11	6	107 N 4P +1	K6	450	75
13	2	109	S 1SA +1	K6	120	50	14	4	103 S 6SA -1	K3	-50	50	12	6	107 S 3P +1	C2	170	50
14	2	109	S 6SA =	TB	990	100	15	4	103 N 3P -2	P8	-200	38	16	6	106 S 2SA -1	K2	-50	6
15	2	109	N 2P =	C6	110	69	16	4	102 S 1SA +2	KK	150	75	17	6	106 W 3C -2	K6	100	0
16	2	108	S 3SA -1	K2	-50	6	17	4	102 N 3SA +1	C8	430	44	18	6	106 S 3P -1	TK	-100	75
17	2	108	N 3SA +3	C2	490	100	18	4	102 S 3P -1	TK	-100	75	19	6	105 S 3SA -1	C4	-50	0
18	2	108	O 4T =	P10	-130	44	19	4	101 N 4P +1	C6	450	62	20	6	105 W 3SA =	PB	-600	19
19	2	106	S 2SA +4	C4	240	25	20	4	101 W 3SA -2	PB	200	75	21	6	105 S 5K -1	C6	-100	44
20	2	106	W 3SA -2	PB	200	75	21	4	101 N 3SA -2	CK	-200	12	22	6	104 W 1SA +1	T5	-120	56
21	2	106	N 3SA =	P6	600	69	22	4	110 W 1C +1	T7	-110	88	23	6	104 O 3C -3	T3	300	75
22	2	105	W 1SA +3	P7	-180	0	23	4	110 S 3T +2	K2	150	44	24	6	104 W 3C =	PB	-140	0
23	2	105	N 3SA =	C5	600	88	24	4	110 N 5T =	C5	400	50	25	6	103 N 2SA +1	T5	150	94
24	2	105	S 4P =	T10	420	81	25	4	108 N 2K +1	C4	110	25	26	6	103 O 3SA +2	C3	-660	25
25	2	104	N 1SA +1	T6	120	56	26	4	108 O 3SA +2	C3	-660	25	27	6	103 N 4C +1	PA	450	38
26	2	104	W 3SA +1	P10	-630	69	27	4	108 N 4C +1	PA	450	38	28	6	102 O 4P -1	KA	50	31
27	2	104	N 4C +2	PA	480	88	28	4	107 O 4P -1	KA	50	31	29	6	102 S 2C =	TK	110	88
28	2	103	O 5P X -1	KA	100	75	29	4	107 O 3K =	TD	-110	44	30	6	102 W 2P +2	KA	-170	50
29	2	103	W 4K -2	C10	200	100	30	4	107 N 3K -4	C2	-200	25	1	7	103 N 1SA +1	C7	120	62
30	2	103	N 2K -3	PK	-150	69	1	5	108 N 1SA -3	C7	-150	0	2	7	103 O 4C =	PB	-420	56
1	3	104	S 1SA -1	P6	-50	12	2	5	108 O 3C +3	PB	-230	88	3	7	103 W 1SA -2	C2	200	81

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
4	7	101	N 2P +1	TK	140	50	5	9	106 N 4C -2	PA	-200	25
5	7	101	N 3C =	K3	140	88	6	9	106 W 1SA =	PA	-90	25
6	7	101	N 1SA =	KB	90	56	7	9	105 N 2K +2	C4	130	100
7	7	110	W 2C =	PA	-110	19	8	9	105 O 6SA =	T3	-990	12
8	7	110	O 3SA +1	P9	-430	81	9	9	105 S 3SA +1	T3	430	50
9	7	110	S 3SA +2	P6	460	94	10	9	103 S 2C =	KD	110	56
10	7	109	N 1SA +2	P10	150	75	11	9	103 N 4C -2	PB	-100	0
11	7	109	N 5P +1	K10	480	100	12	9	103 N 5T -1	KB	-100	25
12	7	109	S 4P +1	K9	650	69	13	9	102 S 2C +2	PA	170	88
13	7	108	N 2T =	KB	90	25	14	9	102 S 6SA -1	T5	-50	50
14	7	108	S 6SA -2	T5	-100	12	15	9	102 N 3P +1	CD	170	100
15	7	108	N 2P +1	T6	140	88	16	9	101 S 2SA +1	K2	150	75
19	7	107	S 3SA +3	K5	490	100	17	9	101 S 2K +4	CB	170	12
20	7	107	W 3SA -2	PB	200	75	18	9	101 S 4P -2	TK	-200	19
21	7	107	N 3SA -2	CK	-200	12	19	9	110 N 4P +1	C3	450	62
22	7	106	W 1SA +2	P7	-150	19	20	9	110 W 3SA +1	PB	-630	0
23	7	106	N 3P +2	K4	200	62	21	9	110 S 5K +1	CD	620	94
24	7	106	N 3SA -1	K7	-50	12	25	9	109 N 1SA +1	TB	120	56
25	7	105	N 2K +1	C4	110	25	26	9	109 O 3K -1	P7	100	94
26	7	105	O 3SA +2	C3	-660	25	27	9	109 N 4C +1	PA	450	38
27	7	105	N 4C +1	T4	450	38	28	9	108 O 4P -2	KA	100	75
28	7	104	O 4P -2	C4	100	75	29	9	108 O 2P =	CK	-110	44
29	7	104	W 3K =	C10	-110	44	30	9	108 N 3K X -3	C2	-500	0
30	7	104	N 2K -1	C2	-50	88	1	10	109 W 2C -1	TA	50	25
1	8	105	S 2P =	T6	110	38	2	10	109 S 4P -3	C2	-300	75
2	8	105	O 4C +1	TD	-450	25	3	10	109 S 3C =	P2	140	50
3	8	105	N 2SA =	PD	120	25	4	10	108 N 4P =	TK	620	100
4	8	104	W 3T X -2	T9	500	88	5	10	108 N 4C -3	PA	-300	6
5	8	104	N 4C -3	PA	-300	6	6	10	108 N 2SA -2	T7	-100	6
6	8	104	N 1SA =	K4	90	56	7	10	107 W 2C =	PA	-110	19
7	8	102	N 1SA =	K6	90	50	8	10	107 W 3SA +2	T5	-460	62
8	8	102	O 5K =	C7	-400	100	9	10	107 S 4C +1	P6	450	69
9	8	102	S 4C -1	P6	-50	0	10	10	106 N 1SA -1	T6	-100	19
10	8	101	S 2C =	KD	110	56	11	10	106 N 4P +1	K6	450	75
11	8	101	N 4P =	T7	420	50	12	10	106 S 4P X =	CB	790	100
12	8	101	S 6P -2	C9	-200	0	13	10	104 W 1SA =	T10	-90	6
13	8	110	S 1C +1	KK	110	38	14	10	104 S 6SA -1	T5	-50	50
14	8	110	S 6SA -1	T6	-50	50	15	10	104 N 3P -2	C9	-200	38
15	8	110	N 4P -3	KD	-300	6	16	10	103 S 2SA =	K2	120	31
16	8	109	S 3SA =	K6	400	100	17	10	103 N 4P +1	C4	450	62
17	8	109	S 3SA +2	TA	460	81	18	10	103 O 4C -2	P9	100	100
18	8	109	S 5P -3	TK	-300	0	19	10	102 S 3SA +2	TK	460	88
22	8	108	W 1SA -1	P4	100	100	20	10	102 W 3SA =	PB	-600	19
23	8	108	N 4P +1	KD	650	100	21	10	102 S 5K +1	T8	620	94
24	8	108	S 4P =	C9	420	81	22	10	101 W 1SA +2	P7	-150	19
25	8	107	N 3K +1	C5	130	75	23	10	101 S 2T +3	CD	150	44
26	8	107	O 3SA +2	C3	-660	25	24	10	101 S 4P =	T2	420	81
27	8	107	N 4C +1	TB	450	38	28	10	110 W 3SA +1	K5	-430	0
28	8	106	O 4P X -2	KA	300	100	29	10	110 W 3K =	C10	-110	44
29	8	106	O 2P X =	CK	-670	0	30	10	110 N 3K -4	C2	-200	25
30	8	106	N 3K -3	C6	-150	69						
1	9	107	N 1SA +2	C7	150	88						
2	9	107	O 4C +1	K9	-450	25						
3	9	107	W 1SA -2	T3	200	81						
4	9	106	W 2T =	P6	-90	25						

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
1	1	101	N 1SA +1 K2	-120	38	2	7	103	O 4C = PB	420	44	3	8	105	N 2SA = PD	-120	75
2	1	101	O 4C = TD	420	44	3	7	103	W 1SA -2 C2	-200	19	4	4	105	S 5P -1 TA	100	88
3	1	101	N 1SA +1 P10	-120	75	7	3	103	S 2P = CA	-110	12	5	4	105	W 3K +2 CA	150	56
4	7	101	N 2P +1 TK	-140	50	8	3	103	O 3SA +4 P9	520	75	6	4	105	N 1SA = K6	-90	44
5	7	101	N 3C = K3	-140	12	9	3	103	N 4C +1 P10	-450	31	7	9	105	N 2K +2 C4	-130	0
6	7	101	N 1SA = KB	-90	44	10	9	103	S 2C = KD	-110	44	8	9	105	O 6SA = T3	990	88
7	2	101	W 2C -1 KB	-100	31	11	9	103	N 4C -2 PB	100	100	9	9	105	S 3SA +1 T3	-430	50
8	2	101	W 3SA +3 T5	490	56	12	9	103	N 5T -1 KB	100	75	13	5	105	S 1C +2 PA	-140	31
9	2	101	N 4C = T7	-420	69	13	4	103	O 2K = CK	90	94	14	5	105	S 6SA -4 T5	200	100
10	8	101	S 2C = KD	-110	44	14	4	103	S 6SA -1 K3	50	50	15	5	105	N 3P -2 C7	200	62
11	8	101	N 4P = T7	-420	50	15	4	103	N 3P -2 P8	200	62	16	1	105	S 2SA +1 T3	-150	25
12	8	101	S 6P -2 C9	200	100	16	10	103	S 2SA = K2	-120	69	17	1	105	S 5K = CB	-400	75
13	3	101	N 1P +2 T6	-140	31	17	10	103	N 4P +1 C4	-450	38	18	1	105	S 3P -1 TK	100	25
14	3	101	S 6SA -1 T5	50	50	18	10	103	O 4C -2 P9	-100	0	19	6	105	S 3SA -1 C4	50	100
15	3	101	N 4P -3 KD	300	94	19	5	103	N 2P +2 C2	-170	88	20	6	105	W 3SA = PB	600	81
16	9	101	S 2SA +1 K2	-150	25	20	5	103	W 3SA -1 P8	-100	56	21	6	105	S 5K -1 C6	100	56
17	9	101	S 2K +4 CB	-170	88	21	5	103	N 2SA -1 CK	100	56	22	2	105	W 1SA +3 P7	180	100
18	9	101	S 4P -2 TK	200	81	22	1	103	W 1SA +1 P7	120	44	23	2	105	N 3SA = C5	-600	12
19	4	101	N 4P +1 C6	-450	38	23	1	103	N 3P = K4	-140	75	24	2	105	S 4P = T10	-420	19
20	4	101	W 3SA -2 PB	-200	25	24	1	103	S 4P = T10	-420	19	25	7	105	N 2K +1 C4	-110	75
21	4	101	N 3SA -2 CK	200	88	25	6	103	N 2SA +1 T5	-150	6	26	7	105	O 3SA +2 C3	660	75
22	10	101	W 1SA +2 P7	150	81	26	6	103	O 3SA +2 C3	660	75	27	7	105	N 4C +1 T4	-450	62
23	10	101	S 2T +3 CD	-150	56	27	6	103	N 4C +1 PA	-450	62	28	3	105	O 4P -1 KA	-50	69
24	10	101	S 4P = T2	-420	19	28	2	103	O 5P X -1 KA	-100	25	29	3	105	S 3C -2 TK	200	88
25	5	101	N 2SA -1 C4	50	100	29	2	103	W 4K -2 C10	-200	0	30	3	105	N 3K -4 C2	200	75
26	5	101	O 3K -1 C3	-100	6	30	2	103	N 2K -3 PK	150	31	1	4	106	N1SAX+2 C7	-380	0
27	5	101	N 4C +1 PA	-450	62	1	3	104	S 1SA -1 P6	50	88	2	4	106	O 5C -1 KA	-50	0
4	2	102	N 2P +3 T5	-200	25	2	3	104	O 4C +1 TD	450	75	3	4	106	O 2P -2 T4	-200	19
5	2	102	N 2C -1 K10	100	38	3	3	104	W 1SA -2 C2	-200	19	4	9	106	W 2T = P6	90	75
6	2	102	N 1SA +1 K9	-120	12	4	8	104	W 3T X -2 T9	-500	12	5	9	106	N 4C -2 PA	200	75
7	8	102	N 1SA = K6	-90	50	5	8	104	N 4C -3 PA	300	94	6	9	106	W 1SA = PA	90	75
8	8	102	O 5K = C7	400	0	6	8	104	N 1SA = K4	-90	44	7	5	106	W 2C = KB	110	81
9	8	102	S 4C -1 P6	50	100	10	4	104	O 2T = CB	90	62	8	5	106	O 3SA +3 P9	490	56
10	3	102	W 1SA -2 C9	-200	6	11	4	104	N 4P -1 C9	50	88	9	5	106	S 3C +1 P6	-170	88
11	3	102	N 2C +2 PB	-170	75	12	4	104	N 5T -1 CK	100	75	10	10	106	N 1SA -1 T6	100	81
12	3	102	S 4P -1 KK	100	75	13	10	104	W 1SA = T10	90	94	11	10	106	N 4P +1 K6	-450	25
13	9	102	S 2C +2 PA	-170	12	14	10	104	S 6SA -1 T5	50	50	12	10	106	S 4P X = CB	-790	0
14	9	102	S 6SA -1 T5	50	50	15	10	104	N 3P -2 C9	200	62	16	6	106	S 2SA -1 K2	50	94
15	9	102	N 3P +1 CD	-170	0	16	5	104	S 2SA = K2	-120	69	17	6	106	W 3C -2 K6	-100	100
16	4	102	S 1SA +2 KK	-150	25	17	5	104	N 3SA +1 C6	-430	56	18	6	106	S 3P -1 TK	100	25
17	4	102	N 3SA +1 C8	-430	56	18	5	104	O 3T +1 P10	130	56	19	2	106	S 2SA +4 C4	-240	75
18	4	102	S 3P -1 TK	100	25	19	1	104	N 4P = T10	-420	62	20	2	106	W 3SA -2 PB	-200	25
19	10	102	S 3SA +2 TK	-460	12	20	1	104	W 3SA -1 PB	-100	56	21	2	106	N 3SA = P6	-600	31
20	10	102	W 3SA = PB	600	81	21	1	104	S 5K = PK	-600	31	22	7	106	W 1SA +2 P7	150	81
21	10	102	S 5K +1 T8	-620	6	22	6	104	W 1SA +1 T5	120	44	23	7	106	N 3P +2 K4	-200	38
22	5	102	W 1SA +1 P7	120	44	23	6	104	O 3C -3 T3	-300	25	24	7	106	N 3SA -1 K7	50	88
23	5	102	W 4K -1 TB	-100	88	24	6	104	W 3C = PB	140	100	25	3	106	S 2P = T2	-110	75
24	5	102	N 2SA = C8	-120	75	25	2	104	N 1SA +1 T6	-120	44	26	3	106	W 3SA +1P10	630	31
25	1	102	N 1SA +2 T6	-150	6	26	2	104	W 3SA +1P10	630	31	27	3	106	O 3P X -4 C8	-800	0
26	1	102	O 3SA +2 C3	660	75	27	2	104	N 4C +2 PA	-480	12	28	8	106	O 4P X -2 KA	-300	0
27	1	102	N 4C +1 PA	-450	62	28	7	104	O 4P -2 C4	-100	25	29	8	106	O 2P X = CK	670	100
28	6	102	O 4P -1 KA	-50	69	29	7	104	W 3K = C10	110	56	30	8	106	N 3K -3 C6	150	31
29	6	102	S 2C = TK	-110	12	30	7	104	N 2K -1 C2	50	12	1	9	107	N 1SA +2 C7	-150	12
30	6	102	W 2P +2 KA	170	50	1	8	105	S 2P = T6	-110	62	2	9	107	O 4C +1 K9	450	75
1	7	103	N 1SA +1 C7	-120	38	2	8	105	O 4C +1 TD	450	75	3	9	107	W 1SA -2 T3	-200	19

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

# OW-Resultate Mitchell-Turnier Samstag - Mensa, Pfäffikon - 17.09.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
4	5	107	W 2T +3	CK	150	100	5	6	109 N 3C =	PA	-140	12
5	5	107	W 3K +2	CA	150	56	6	6	109 W 2C -2	PA	-200	0
6	5	107	N 1SA -2	KB	100	94	7	1	109 W 3C -1	PA	-100	31
7	10	107	W 2C =	PA	110	81	8	1	109 O 3SA +1	P9	430	19
8	10	107	W 3SA +2	T5	460	38	9	1	109 N 3SA +2	P8	-460	6
9	10	107	S 4C +1	P6	-450	31	10	7	109 N 1SA +2	P10	-150	25
10	6	107	W 1SA -2	CB	-200	6	11	7	109 N 5P +1	K10	-480	0
11	6	107	N 4P +1	K6	-450	25	12	7	109 S 4P +1	K9	-650	31
12	6	107	S 3P +1	C2	-170	50	13	2	109 S 1SA +1	K6	-120	50
13	1	107	O 2K -2	TA	-200	0	14	2	109 S 6SA =	TB	-990	0
14	1	107	S 3SA +2	T5	-460	12	15	2	109 N 2P =	C6	-110	31
15	1	107	N 2P =	C4	-110	31	16	8	109 S 3SA =	K6	-400	0
19	7	107	S 3SA +3	K5	-490	0	17	8	109 S 3SA +2	TA	-460	19
20	7	107	W 3SA -2	PB	-200	25	18	8	109 S 5P -3	TK	300	100
21	7	107	N 3SA -2	CK	200	88	19	3	109 N 4P +1	C5	-450	38
22	3	107	W 1SA +1	P7	120	44	20	3	109 W 3SA -4	P8	-400	0
23	3	107	N 4P -1	TD	100	100	21	3	109 N 3SA -2	CK	200	88
24	3	107	S 3P +1	T10	-170	62	25	9	109 N 1SA +1	TB	-120	44
25	8	107	N 3K +1	C5	-130	25	26	9	109 O 3K -1	P7	-100	6
26	8	107	O 3SA +2	C3	660	75	27	9	109 N 4C +1	PA	-450	62
27	8	107	N 4C +1	TB	-450	62	28	5	109 W 2SA -1	C10	-50	69
28	4	107	O 4P -1	KA	-50	69	29	5	109 W 3K -1	C10	-100	25
29	4	107	O 3K =	TD	110	56	30	5	109 O 3SA -2	C10	-100	0
30	4	107	N 3K -4	C2	200	75	1	6	110 N 1SA +1	T2	-120	38
1	5	108	N 1SA -3	C7	150	100	2	6	110 O 4C +2	TD	480	100
2	5	108	O 3C +3	PB	230	12	3	6	110 N 2SA =	PD	-120	75
3	5	108	W 1SA -1	K4	-100	100	4	1	110 N 3P +1	T5	-170	38
4	10	108	N 4P =	TK	-620	0	5	1	110 N 3C =	PA	-140	12
5	10	108	N 4C -3	PA	300	94	6	1	110 N 1SA =	K6	-90	44
6	10	108	N 2SA -2	T7	100	94	7	7	110 W 2C =	PA	110	81
7	6	108	W 2C =	KB	110	81	8	7	110 O 3SA +1	P9	430	19
8	6	108	O 6SA +1	P6	1020	100	9	7	110 S 3SA +2	P6	-460	6
9	6	108	S 4C =	P4	-420	69	10	2	110 S 1SA -1	P2	100	81
10	1	108	S 2C -2	P2	200	100	11	2	110 N 2P +3	T2	-200	62
11	1	108	N 4P +1	K5	-450	25	12	2	110 S 4SA +1	KK	-660	12
12	1	108	S 4P +1	K7	-650	31	13	8	110 S 1C +1	KK	-110	62
13	7	108	N 2T =	KB	-90	75	14	8	110 S 6SA -1	T6	50	50
14	7	108	S 6SA -2	T5	100	88	15	8	110 N 4P -3	KD	300	94
15	7	108	N 2P +1	T6	-140	12	16	3	110 N 3C =	PB	-140	50
16	2	108	S 3SA -1	K2	50	94	17	3	110 S 3SA +2	C10	-460	19
17	2	108	N 3SA +3	C2	-490	0	18	3	110 S 4P -2	TK	200	81
18	2	108	O 4T =	P10	130	56	19	9	110 N 4P +1	C3	-450	38
22	8	108	W 1SA -1	P4	-100	0	20	9	110 W 3SA +1	PB	630	100
23	8	108	N 4P +1	KD	-650	0	21	9	110 S 5K +1	CD	-620	6
24	8	108	S 4P =	C9	-420	19	22	4	110 W 1C +1	T7	110	12
25	4	108	N 2K +1	C4	-110	75	23	4	110 S 3T +2	K2	-150	56
26	4	108	O 3SA +2	C3	660	75	24	4	110 N 5T =	C5	-400	50
27	4	108	N 4C +1	PA	-450	62	28	10	110 W 3SA +1	K5	430	100
28	9	108	O 4P -2	KA	-100	25	29	10	110 W 3K =	C10	110	56
29	9	108	O 2P =	CK	110	56	30	10	110 N 3K -4	C2	200	75
30	9	108	N 3K X -3	C2	500	100						
1	10	109	W 2C -1	TA	-50	75						
2	10	109	S 4P -3	C2	300	25						
3	10	109	S 3C =	P2	-140	50						
4	6	109	W 4T -1	PK	-100	62						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.