

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 25.08.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
1	9	108	W 5T X =	P7 -550	0	7	9	106	W 4P +1	C6 -650	6	13	4	103	S 4C +1	K10 650	56
1	4	107	W 4T X =	P7 -510	12	7	3	103	W 4P =	T5 -620	38	13	3	101	N 4C +1	C4 650	56
1	2	103	S 4P X -3	KA -500	25	7	6	109	W 4P =	T7 -620	38	13	2	108	N 4P +1	T6 650	56
1	8	106	O 4K +1	K9 -150	38	7	5	107	W 4P =	KA -620	38	13	1	106	N 4C +1	P9 650	56
1	7	104	W 4T =	PD -130	56	7	2	101	N 5T X -1	KB -200	75	13	9	104	N 4P +1	TD 650	56
1	6	102	W 4T =	P10 -130	56	7	7	102	W 3P +2	KA -200	75	13	8	102	N 4C +1	TD 650	56
1	1	101	S 4P X -1	C10 -100	75	7	4	105	N 5T X -1	CA -200	75	13	7	109	N 4P +1	TD 650	56
1	5	109	W 5T -1	PD 50	94	7	8	104	W 3P +1	KA -170	100	14	6	107	N 4P -3	TA -150	0
1	3	105	W 5T -1	PD 50	94	8	2	101	S 3C =	T10 140	12	14	8	102	N 4C -2	TA -100	12
2	7	104	W 3SA +2	T9 -460	0	8	9	106	N 2C +1	T9 140	12	14	5	105	N 3SA -1	K5 -50	38
2	1	101	W 4P +1	TB -450	25	8	5	107	S 3C =	T5 140	12	14	1	106	N 3C -1	P9 -50	38
2	8	106	W 4P +1	T7 -450	25	8	3	103	S 2C +2	T4 170	50	14	7	109	N 2C -1	TA -50	38
2	6	102	W 4P +1	TB -450	25	8	8	104	S 2C +2	T4 170	50	14	4	103	N 3C =	P4 140	69
2	9	108	W 3SA +1	TB -430	62	8	7	102	S 2C +2	T8 170	50	14	3	101	N 2C +1	TA 140	69
2	5	109	W 3SA +1	T9 -430	62	8	1	108	S 3C +2	T4 200	88	14	2	108	N 3C +1	KA 170	94
2	4	107	W 3SA +1	T9 -430	62	8	6	109	S 2C +3	TB 200	88	14	9	104	N 3C +1	KA 170	94
2	3	105	O 4P =	CK -420	88	8	4	105	S 3C +2	T10 200	88	15	4	103	N 4C X -2	K7 -500	0
2	2	103	O 3C +1	T2 -170	100	9	2	101	N 5K X -2	P5 -300	0	15	3	101	W 4P =	CA -420	12
3	7	104	W 1SA +3	T9 -180	0	9	1	108	W 3P =	C7 -140	38	15	5	105	W 3P +1	CA -170	25
3	1	101	W 1SA =	P2 -90	38	9	9	106	W 3P =	C7 -140	38	15	2	108	W 3P =	CA -140	56
3	8	106	W 1SA =	P2 -90	38	9	6	109	W 2P +1	KD -140	38	15	1	106	O 2P +1	C4 -140	56
3	6	102	W 1SA =	P2 -90	38	9	5	107	W 3P =	C7 -140	38	15	8	102	O 3P =	C2 -140	56
3	3	105	W 1SA =	P2 -90	38	9	4	105	W 2P +1	K8 -140	38	15	7	109	O 3P =	CD -140	56
3	2	103	W 1SA =	PK -90	38	9	3	103	N 3T -2	PB -100	81	15	9	104	O 2P =	C4 -110	88
3	9	108	W 1SA -1	T4 100	88	9	7	102	N 4K X -1	P2 -100	81	15	6	107	O 4P -1	C8 50	100
3	5	109	W 1SA -1	P2 100	88	9	8	104	W 3P -1	KD 100	100	16	1	105	N 5K X -4	C9 -800	0
3	4	107	W 2SA -1	P2 100	88	10	2	109	O 3SA +1	T2 -630	0	16	7	108	W 4P +1	KK -650	12
4	2	102	N 4P =	T6 620	31	10	9	105	O 3SA =	T3 -600	25	16	5	104	W 4P =	KK -620	31
4	1	109	S 4P =	T3 620	31	10	7	101	O 3SA =	K6 -600	25	16	9	103	W 4P =	KK -620	31
4	9	107	S 4P =	K2 620	31	10	5	106	O 3SA =	T2 -600	25	16	3	109	W 2P =	KK -110	50
4	6	101	S 4P =	T3 620	31	10	4	104	O 3SA -1	K6 100	62	16	6	106	W 4P -1	KK 100	69
4	5	108	N 4P =	C6 620	31	10	3	102	W 3C -1	T8 100	62	16	8	101	W 4P -1	KK 100	69
4	3	104	N 4P =	C10 620	31	10	6	108	W 1SA -1	K3 100	62	16	4	102	W 4P -2	KK 200	94
4	8	105	S 4P +1	T3 650	88	10	8	103	W 4C -2	T8 200	88	16	2	107	W 5P -2	KK 200	94
4	7	103	N 4P +1	C6 650	88	10	1	107	O 3SA -3	KK 300	100	17	9	103	S 3SA -4	P10 -200	0
4	4	106	S 5P =	KB 650	88	11	7	101	S 3SA -3	TB -150	0	17	6	106	N 3SA -3	CK -150	19
5	2	102	S 3SA -1	T3 -100	0	11	9	105	N 3K -2	P3 -100	19	17	8	101	N 3SA -3	PD -150	19
5	6	101	S 2SA =	T3 120	12	11	8	103	S 3C -2	TB -100	19	17	4	102	S 3T -2	C9 -100	38
5	7	103	S 2K +2	C9 130	31	11	2	109	N 2K -1	P3 -50	44	17	1	105	S 1SA -1	P10 -50	50
5	5	108	S 3K +1	P5 130	31	11	5	106	N 3K -1	P10 -50	44	17	5	104	W 2P -2	TK 100	69
5	4	106	S 3K +2	P10 150	50	11	4	104	N 2K =	P10 90	75	17	7	108	O 2SA -2	K10 100	69
5	1	109	S 3SA =	T3 600	81	11	3	102	N 2K =	P10 90	75	17	3	109	N 2SA =	CK 120	88
5	9	107	S 3SA =	T3 600	81	11	1	107	N 2K =	T2 90	75	17	2	107	W 3P X -2	KB 300	100
5	8	105	S 5K =	TA 600	81	11	6	108	N 2K +1	T2 110	100	18	7	108	S 1SA -2	T2 -200	0
5	3	104	S 3SA =	P5 600	81	12	4	104	N 3T -2	K3 -200	6	18	8	101	O 2C =	K4 -110	12
6	1	109	W 4P =	C10 -620	12	12	2	109	N 2K -2	K6 -200	6	18	5	104	S 1SA -1	T5 -100	31
6	8	105	W 4P =	T2 -620	12	12	8	103	O 1SA +2	P3 -150	25	18	2	107	S 1T -1	CA -100	31
6	6	101	O 4P =	CA -620	12	12	9	105	O 1SA +1	P2 -120	38	18	1	105	W 2SA -1	TB 50	50
6	5	108	W 1P +1	K7 -110	38	12	3	102	O 1SA =	P3 -90	75	18	6	106	S 1SA =	C2 90	75
6	7	103	O 3SA -1	C5 100	56	12	1	107	O 1SA =	P3 -90	75	18	3	109	S 1SA =	C2 90	75
6	3	104	W 4P -1	C10 100	56	12	7	101	O 1SA =	P3 -90	75	18	9	103	S 1SA =	CA 90	75
6	9	107	W 4P -2	C10 200	81	12	6	108	O 1SA =	P3 -90	75	18	4	102	S 1SA +1	CA 120	100
6	4	106	W 4P -2	C7 200	81	12	5	106	O 1SA =	P5 -90	75	19	8	109	N 6SA -1	K6 -50	0
6	2	102	W 4P -3	T2 300	100	13	6	107	N 4P =	TD 620	0	19	6	105	S 3SA +1	TB 430	12
7	1	108	W 5P =	C6 -650	6	13	5	105	N 4P +1	T5 650	56	19	7	107	N 4P +1	K4 450	38

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
19	5	103	N 4P +1	K5	450	38	25	5	101 S 5C -2	KA	-100	38
19	9	102	N 4P +1	TD	450	38	25	4	108 S 5C -1	KA	-50	69
19	4	101	N 3SA +2	TD	460	69	25	3	106 S 4C -1	KA	-50	69
19	1	104	N 3SA +2	K8	460	69	25	6	103 S 4C =	KA	420	94
19	2	106	N 4P +2	TD	480	88	25	1	102 S 4C =	KA	420	94
19	3	108	S 3SA +3	T6	490	100	26	4	108 N 3C -1	C9	-100	6
20	6	105	S 3SA -1	T6	-100	6	26	2	104 N 3SA -1	T6	-100	6
20	8	109	S 3SA -1	T6	-100	6	26	9	109 N 2K +3	TA	150	44
20	9	102	N 3C =	K9	140	25	26	7	105 N 2K +3	C6	150	44
20	4	101	N 3P +1	K9	170	38	26	6	103 N 3K +2	P2	150	44
20	1	104	N 2P +4	K9	230	50	26	3	106 N 2K +3	C9	150	44
20	7	107	N 4P =	K9	620	81	26	5	101 S 3K +3	TK	170	81
20	5	103	N 4P =	K9	620	81	26	1	102 N 4K +2	C6	170	81
20	3	108	N 4P =	T10	620	81	26	8	107 S 5K =	TK	600	100
20	2	106	N 4C =	K9	620	81	27	9	109 O 3SA +4	P2	-520	12
21	5	103	O 4P =	T5	-420	0	27	6	103 W 3SA +4	C3	-520	12
21	4	101	O 2P +1	CK	-140	19	27	3	106 O 3SA +4	P2	-520	12
21	8	109	O 2P +1	T10	-140	19	27	8	107 W 3SA +3	C3	-490	38
21	7	107	O 4P -1	CK	50	69	27	5	101 O 3SA +2	T5	-460	56
21	6	105	O 4P -1	C5	50	69	27	1	102 O 3SA +2	T3	-460	56
21	3	108	O 4P -1	CK	50	69	27	7	105 O 3SA +1	T2	-430	81
21	2	106	O 4P -1	CK	50	69	27	2	104 O 3SA +1	P5	-430	81
21	1	104	O 4P -1	CK	50	69	27	4	108 W 6K -1	T6	50	100
21	9	102	O 4P -1	T3	50	69						
22	1	103	N 5P X -4	KA	-800	0						
22	7	106	O 4C +2	PA	-680	38						
22	6	104	O 4C +2	PA	-680	38						
22	5	102	O 4C +2	PA	-680	38						
22	2	105	O 5C +1	PA	-680	38						
22	9	101	O 4C +2	K9	-680	38						
22	8	108	O 4C +1	K9	-650	81						
22	3	107	O 4C +1	TD	-650	81						
22	4	109	S 4P X -2	CD	-300	100						
23	9	101	S 4C -1	PA	-100	0						
23	7	106	O 3T -1	CA	100	12						
23	6	104	N 2C =	TA	110	25						
23	1	103	N 2C +1	TA	140	38						
23	8	108	N 2C +2	TA	170	56						
23	2	105	N 2C +2	TA	170	56						
23	4	109	S 3C +2	PA	200	81						
23	3	107	N 2C +3	TA	200	81						
23	5	102	N 4C =	TA	620	100						
24	9	101	W 3P +1	C9	-170	0						
24	7	106	W 3P =	CK	-140	38						
24	6	104	W 3P =	C9	-140	38						
24	5	102	W 3P =	CK	-140	38						
24	2	105	W 3P =	CA	-140	38						
24	1	103	W 3P =	C8	-140	38						
24	8	108	W 2P =	C8	-110	75						
24	4	109	S 2C -1	KK	-50	88						
24	3	107	W 4P -2	CK	100	100						
25	2	104	W 4P X =	CA	-790	0						
25	7	105	W 4P +1	CA	-650	12						
25	9	109	S 5C -2	KA	-100	38						
25	8	107	S 4C X -1	KA	-100	38						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.