

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Samstag Sommerdrive - Atzmännig - 23.07.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	3	105		-420	0	5	10	104 S 4C +1	T7	650	33	9	10	102 N 2SA +2	C2	180	50	
1	12	110	O 3C +2	TD	8	5	7	111		650	33	9	4	103 N 3SA =	K6	400	58	
1	2	103		-170	17	5	4	105		650	33	9	3	101 N 3SA +1	C2	430	75	
1	13	112	O 3C =	PA	25	5	3	103 N 3SA +2	P2	660	54	9	1	110 N 3SA +1	C2	430	75	
1	6	111	N 3P -1	CA	33	5	11	106 N 3SA +2	P4	660	54	9	13	108 N 3SA +1	C2	430	75	
1	1	101	O 3C -1	TD	58	5	2	101 S 4C +2	P4	680	79	9	12	106 N 3SA +2	C2	460	92	
1	11	108	O 4C -1	TD	58	5	1	112 S 4C +2	P3	680	79	9	5	105 N 3SA +3	C2	490	100	
1	10	106	O 4C -1	TD	58	5	8	113 S 4C +2	P4	680	79	10	11	104 N 4C -3	P3	-300	0	
1	9	104	O 3C -1	P10	58	5	5	107		680	79	10	13	108 N 4C -2	P4	-200	12	
1	4	107		50	58	5	13	110 N 3SA +3	P9	690	100	10	8	111		-200	12	
1	7	113	O 4C -2	TD	83	6	13	110 O 6SA =	C10	-1440	4	10	2	112 W 3P =	T8	-140	25	
1	5	109		170	92	6	11	106 W 6SA =	T3	-1440	4	10	4	103 N 4C -1	P3	-100	42	
1	8	102	W 4C X -2	PD	300	100	6	6	109		-1390	17	10	12	106 N 4C -1	P3	-100	42
2	13	112	W 1SA +2	T3	-150	4	6	9	102 O 3SA +3	P10	-690	25	10	7	109		-100	42
2	4	107		-150	4	6	5	107		-630	33	10	10	102		0	58	
2	12	110	W 1SA +1	KA	-120	33	6	2	101 O 5K +1	T9	-620	50	10	5	105 W 3P -1	T8	100	71
2	10	106	O 2SA =	P5	-120	33	6	1	112 O 5K +1	C6	-620	50	10	6	107		100	71
2	9	104	W 1SA +1	P7	-120	33	6	4	105		-620	50	10	3	101 N 3C =	PB	140	88
2	8	102	W 1SA +1	KA	-120	33	6	7	111		-210	67	10	9	113		140	88
2	6	111	W 1SA +1	T3	-120	33	6	3	103 O 3K +2	T9	-150	75	10	1	110 W 4P X -1	T8	200	100
2	7	113	W 1SA -1	T2	50	67	6	8	113		0	83	11	6	106 S 2SA -4	C8	-200	0
2	5	109		50	67	6	10	104 W 6SA -1	C2	100	92	11	13	107 W 2C +1	TD	-140	12	
2	3	105		50	67	6	12	108 O 6SA -4	P6	400	100	11	10	101		-140	12	
2	1	101	W 1SA -2	T3	100	88	7	4	104 O 3SA +1	CD	-630	0	11	9	112		-110	25
2	2	103		100	88	7	13	109 O 2SA +2	CD	-180	12	11	2	111 N 3K -2	C2	-100	38	
2	11	108	O 1P X -3	T5	500	100	7	12	107 O 2SA +2	P4	-180	12	11	12	105 S 2P -2	KA	-100	38
3	2	102	W 3SA +3	C10	-690	12	7	11	105 O 2SA +1	CD	-150	29	11	1	109 S 2SA -1	T4	-50	58
3	1	113	W 3SA +3	CB	-690	12	7	5	106		-150	29	11	8	110		-50	58
3	11	107	W 3SA +3	CB	-690	12	7	7	110		-140	42	11	7	108		-50	58
3	6	110		-690	12	7	2	113 O 2SA =	CD	-120	50	11	5	104 W 1C -1	KD	50	79	
3	5	108		-660	33	7	8	112		-100	58	11	11	103 W 2C -1	KD	50	79	
3	7	112	W 4P +1	K7	-650	46	7	9	101 O 2T =	KA	-90	67	11	4	102 S 2SA =	C7	120	92
3	4	106		-650	46	7	3	102 S 2C =	K9	110	83	11	3	113 S 2SA +1	C7	150	100	
3	3	104		-500	58	7	1	111 S 2C =	K6	110	83	12	1	109 W 4P =	C2	-420	4	
3	9	103	W 2SA +4	C10	-240	67	7	6	108		110	83	12	9	112		-420	4
3	8	101	W 3P +1	C5	-170	75	7	10	103 W 3T -2	CK	200	100	12	5	104 W 1P +3	T4	-170	17
3	13	111	W 3SA -1	CA	100	83	8	8	112		-50	8	12	8	110		-140	25
3	12	109	W 3SA -2	CB	200	96	8	6	108		-50	8	12	13	107 W 2SA =	T6	-120	33
3	10	105	O 3SA -2	C6	200	96	8	5	106		-50	8	12	2	111 W 2C =	KB	-110	46
4	9	103	W 3SA +2	CK	-660	0	8	9	101		0	25	12	10	101		-110	46
4	2	102	W 3SA +1	C4	-630	42	8	12	107 W 4T -2	KA	100	33	12	6	106 W 2SA -1	T5	50	62
4	1	113	W 3SA +1	C4	-630	42	8	4	104 N 3K =	T7	110	50	12	3	113 W 4P -1	T5	50	62
4	13	111	W 3SA +1	C4	-630	42	8	13	109 N 3K =	T5	110	50	12	7	108		120	75
4	12	109	O 3SA +1	C4	-630	42	8	7	110		110	50	12	4	102 W 3SA -3	T5	150	88
4	11	107	W 3SA +1	CK	-630	42	8	2	113 S 1SA +1	TB	120	71	12	11	103 W 2SA -3	T5	150	88
4	8	101	O 3SA +1	T2	-630	42	8	10	103 S 1SA +1	T9	120	71	12	12	105 W 3SA -4	T5	200	100
4	6	110		-630	42	8	11	105 S 1SA +2	P10	150	83	13	3	112 O 3SA +2	C4	-660	12	
4	5	108		-630	42	8	1	111 S 1SA +3	P10	180	92	13	12	104 O 3SA +2	P10	-660	12	
4	3	104		-630	42	8	3	102 O 4T X -4	C8	800	100	13	10	113		-660	12	
4	4	106		-240	83	9	11	104 N 3SA -1	K6	-50	0	13	8	109		-660	12	
4	7	112		0	92	9	9	113		140	12	13	4	101 O 3SA +1	C4	-630	46	
4	10	105	O 2SA -2	C4	200	100	9	6	107		140	12	13	2	110 O 3SA +1	C4	-630	46
5	6	109		110	0	9	2	112 N 2SA +1	C2	150	29	13	13	106 O 3SA +1	P10	-630	46	
5	9	102	N 2SA =	K2	120	8	9	8	111		150	29	13	9	111		-630	46
5	12	108	N 3SA +1	C5	630	17	9	7	109		170	42	13	7	107 O 3SA =	CB	-600	83

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
13	6	105	O 3SA = K8	-600	83	17	5	101 N 1SA +3 P3	180	100		22	9	107 N 4P X -1 KA	-100	12	
13	5	103	O 3SA = C4	-600	83	18	13	104		-110	0	22	1	104		170	25
13	1	108	W 3SA = C4	-600	83	18	9	109 N 4C -1 C10	-100	12		22	11	111 S 4P = K6	420	42	
13	11	102		-600	83	18	1	106 N 3C -1 K2	-100	12		22	6	101 S 4P = TA	420	42	
14	9	111		-150	4	18	8	107 O 3P -1 C5	50	29		22	5	112 S 4P = KB	420	42	
14	8	109		-150	4	18	11	113		50	29	22	8	105 S 4P +1 K6	450	75	
14	2	110	O 3T = CA	-110	17	18	3	110 O 4P X -1 T5	100	42		22	7	103 S 4P +1 K4	450	75	
14	5	103	W 1SA = P4	-90	25	18	7	105 N 3C = T10	140	58		22	3	108 S 4P +1 TA	450	75	
14	7	107	S 2K -1 TB	-50	46	18	5	101 N 2C +1 K2	140	58		22	2	106		450	75
14	6	105	S 2K -1 TB	-50	46	18	12	102		140	58	22	13	102		450	75
14	4	101	S 3K -1 T4	-50	46	18	6	103 N 2C +2 C4	170	83		22	12	113		520	100
14	11	102		-50	46	18	2	108 N 2C +2 K2	170	83		23	6	113 O 3SA +2 P10	-660	0	
14	12	104		0	67	18	10	111		170	83	23	4	109 W 4C +1 PD	-650	12	
14	1	108	O 3T -1 CA	50	79	18	4	112 N 4C = P4	620	100		23	3	107		-650	12
14	10	113		50	79	19	11	112		-150	0	23	9	106 O 3SA +1 P10	-630	25	
14	13	106	S 2K = PB	90	92	19	10	110 W 3C = K4	-140	8		23	7	102 N 2P -2 C6	-200	42	
14	3	112	O 3T -2 CA	100	100	19	12	101		-110	17	23	2	105		-200	42
15	8	108	S 4C -2 TA	-200	4	19	3	109 N 3P -2 T7	-100	25		23	1	103		-200	42
15	11	101		-200	4	19	13	103		-50	33	23	12	112 N 2P -1 C6	-100	62	
15	7	106	N 4C -1 K4	-100	17	19	6	102 N 1P = C5	80	42		23	5	111 N 2P -1 KA	-100	62	
15	5	102	W 3K -1 C9	50	25	19	9	108 W 3C -1 K4	100	62		23	11	110 O 4C -1 T4	100	79	
15	6	104	W 4K -2 PA	100	42	19	7	104 W 3C -1 K4	100	62		23	13	101		100	79
15	1	107	W 4K -2 C9	100	42	19	5	113 W 3C -1 K4	100	62		23	10	108 O 2SA -2 T5	200	96	
15	12	103		100	42	19	2	107 W 4C -1 K4	100	62		23	8	104 W 6C -2 PD	200	96	
15	4	113	S 3C = TA	140	62	19	1	105		110	83	24	4	109 N 4P -1 KK	-50	0	
15	13	105	N 3P = K2	140	62	19	4	111 N 2P +1 C5	140	92		24	9	106 O 4T -1 P10	50	8	
15	2	109	W 3SA -3 P10	150	83	19	8	106 W 3C -2 P6	200	100		24	10	108 N 3P +1 KK	170	17	
15	10	112		150	83	20	10	110 W 2P +1 P7	-140	12		24	13	101		200	25
15	9	110		150	83	20	6	102 W 2P +1 C6	-140	12		24	12	112 N 4P = KK	420	58	
15	3	111	S 2C X +1 P6	870	100	20	5	113 W 2P +1 TK	-140	12		24	11	110 N 4P = KK	420	58	
16	6	104	W 1K X = PK	-140	0	20	11	112		-140	12	24	8	104 N 4P = KK	420	58	
16	2	109	W 2C = PK	-110	8	20	9	108 W 2P = T6	-110	54		24	7	102 N 4P = KK	420	58	
16	10	112		-50	21	20	8	106 W 2P = C7	-110	54		24	6	113 N 4P = TA	420	58	
16	9	110		-50	21	20	7	104 W 2P = TK	-110	54		24	2	105		420	58
16	13	105		0	33	20	3	109 W 2P = TK	-110	54		24	1	103		420	58
16	5	102	N 1SA = K8	90	46	20	2	107 W 2P = C7	-110	54		24	5	111 N 4P +1 KK	450	92	
16	1	107	S 1SA = K3	90	46	20	13	103		-110	54	24	3	107		590	100
16	12	103		140	62	20	4	111 O 3P -1 T7	100	92		25	11	109 O 4C = K2	-620	4	
16	11	101		140	62	20	1	105		100	92	25	1	102		-620	4
16	8	108	N 1SA +2 K8	150	79	20	12	101		100	92	25	10	107 O 3SA = K2	-600	21	
16	7	106	N 1SA +2 K6	150	79	21	11	111 W 4P +1 TD	-450	8		25	3	106		-600	21
16	4	113	S 2P +2 K3	170	96	21	9	107 W 4P +1 TD	-450	8		25	9	105 O 2C +2 P4	-170	42	
16	3	111	N 2P +2 CD	170	96	21	4	110 W 4P +1 TD	-450	8		25	5	110 O 2C +2 K2	-170	42	
17	11	113		-460	0	21	5	112 W 4P = TD	-420	29		25	4	108		-170	42
17	3	110	O 2C +1 K5	-140	8	21	3	108 W 4P = C2	-420	29		25	13	113 O 2C +1 K2	-140	62	
17	13	104		-50	21	21	10	109 W 3P +2 KB	-200	46		25	2	104		-140	62
17	12	102		-50	21	21	13	102		-200	46	25	8	103 W 2SA = KA	-120	75	
17	6	103	W 2SA -1 P6	50	38	21	8	105 W 3P +1 C2	-170	75		25	12	111 O 4C -1 T10	100	92	
17	4	112	O 2C -1 TD	50	38	21	6	101 W 3P +1 C2	-170	75		25	7	101 O 3C -1 KB	100	92	
17	7	105	W 2P -2 T7	100	54	21	2	106		-170	75	25	6	112 O 4C -1 T10	100	92	
17	1	106	W 3P X -1 KA	100	54	21	1	104		-170	75	26	8	103 W 5C +2 T2	-710	0	
17	2	108	N 3K = P3	110	71	21	12	113		-170	75	26	13	113 W 4C +1 T3	-650	25	
17	10	111		110	71	21	7	103 O 5K -2 P7	100	100		26	10	107 W 4C +1 T3	-650	25	
17	8	107	N 4K = P3	130	83	22	4	110 O 5K = PK	-600	0		26	6	112 W 4C +1 P5	-650	25	
17	9	109	S 2SA +1 P5	150	92	22	10	109 S 4P X -1 K8	-100	12		26	3	106		-650	25

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz
26	1	102		-650	25
26	12	111	S 5T X -2 KA	-500	54
26	2	104		-500	54
26	9	105	S 5T -2 KA	-200	71
26	4	108		-200	71
26	11	109	S 4T -1 CA	-100	88
26	5	110	S 4T -1 KA	-100	88
26	7	101	S 3T = CA	110	100