

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 05.07.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	13	111	N 4C -1	TD	-50	5	6	6	108 O 2K +3	C3	-150	0	11	5	104 N 2SA -3	T4	-150	0
1	8	114	N 4C -1	TD	-50	5	6	9	114 N 3C -2	P2	-100	10	11	4	102 N 3T -1	C6	-50	15
1	9	103	N 2C +1	T7	140	35	6	14	111 W 2T =	KA	-90	20	11	12	103 N 3T -1	KA	-50	15
1	7	112	N 2C +1	T6	140	35	6	2	101 S 3C -1	PD	-50	40	11	2	112 W 2C -1	T3	50	50
1	6	110	N 2C +1	T7	140	35	6	1	113 S 4P -1	TA	-50	40	11	14	108 O 2P -1	TA	50	50
1	5	108	N 2C +1	TD	140	35	6	12	107 S 3C -1	PD	-50	40	11	13	105 W 2C -1	K10	50	50
1	1	101	N 3C +1	P2	170	75	6	8	112 O 2K -1	PA	100	60	11	10	113 W 2C -1	K6	50	50
1	14	113	N 2C +2	TD	170	75	6	3	103 S 3C =	TA	140	80	11	9	111 W 2C -1	K6	50	50
1	12	109	N 1C +3	TD	170	75	6	13	109 S 2C +1	TA	140	80	11	3	114 W 3C -2	TK	100	85
1	4	106	N 2C +2	P4	170	75	6	10	102 S 3C =	TA	140	80	11	1	110 W 2C -2	T8	100	85
1	10	105	W 4P -4	K7	200	100	6	7	110 W 2T -3	C4	300	100	11	6	106 S 1SA +1	P9	120	100
2	4	106	N 2T -4	C10	-400	0	7	14	110 W 3SA +2	K5	-660	5	12	9	111 O 6T +1	P6	-940	0
2	12	109	N 2T -2	CA	-200	10	7	8	111 W 3SA +2	K5	-660	5	12	4	102 W 3SA +4	C3	-520	15
2	9	103	N 2C -1	PA	-100	25	7	3	102 W 3SA +1	P3	-630	30	12	3	114 W 3SA +4	K5	-520	15
2	7	112	N 2SA -1	TB	-100	25	7	13	108 O 3SA +1	C8	-630	30	12	6	106 O 3SA +2	K2	-460	40
2	1	101	W 2K -1	TA	50	40	7	9	113 W 3SA +1	C3	-630	30	12	1	110 O 3SA +2	K2	-460	40
2	8	114	N 1SA =	C4	90	50	7	4	104 O 3SA =	P3	-600	60	12	13	105 O 3SA +2	K5	-460	40
2	14	113	O 2C -2	T5	100	65	7	2	114 W 3SA =	K5	-600	60	12	2	112 O 3T +2	P3	-150	65
2	13	111	O 2C -2	KA	100	65	7	7	109 O 3SA =	P3	-600	60	12	12	103 O 3T +2	K9	-150	65
2	10	105	N 1SA +1	TB	120	90	7	1	112 W 2SA +3	C3	-210	80	12	5	104 O 6T -1	K2	50	90
2	6	110	N 2SA =	C5	120	90	7	12	106 W 1SA +2	T10	-150	90	12	14	108 O 6SA -1	K4	50	90
2	5	108	N 1SA +1	C4	120	90	7	10	101 W 3SA -1	P3	100	100	12	10	113 W 6SA -1	KA	50	90
3	9	101	O 6C =	K6	-1430	0	8	1	112 O 5C =	TA	-450	5	13	7	107 S 4P -2	CB	-200	0
3	2	102	O 3SA +3	K2	-690	20	8	14	110 O 4P +1	TA	-450	5	13	5	103 S 1P +1	CB	110	25
3	14	112	O 3SA +3	P2	-690	20	8	4	104 O 4P =	TA	-420	20	13	1	109 S 1P +1	CB	110	25
3	6	109	O 3SA +3	P2	-690	20	8	10	101 S 5T X -2	CK	-300	30	13	12	102 S 1P +1	CB	110	25
3	1	114	O 4C +2	T3	-680	50	8	2	114 S 5T -2	P3	-100	40	13	10	112 S 1P +1	CB	110	25
3	12	108	O 4C +2	T3	-680	50	8	3	102 S 5T -1	CK	-50	60	13	14	106 S 1P +2	CB	140	50
3	10	104	O 4C +2	P2	-680	50	8	8	111 S 5T -1	PK	-50	60	13	6	105 S 2SA +1	K8	150	70
3	5	107	O 3SA +2	P2	-660	70	8	7	109 S 5T -1	CK	-50	60	13	3	113 S 2SA +1	K10	150	70
3	8	113	W 3SA +1	T5	-630	80	8	13	108 O 4P -1	TA	50	85	13	13	104 S 2SA +1	K8	150	70
3	13	110	O 3SA =	T3	-600	90	8	9	113 O 5P -1	TA	50	85	13	4	101 S 3SA =	K8	600	95
3	7	111	W 6SA -1	TD	100	100	8	12	106 S 3T +1	P3	130	100	13	2	111 N 3SA =	C3	600	95
4	1	114	S 6SA -2	P6	-200	0	9	14	109 N 2SA +1	C3	150	0	14	10	112 O 4C X +1	KK	-690	0
4	10	104	S 6SA -1	C7	-100	10	9	5	105 N 3SA =	T3	400	35	14	12	102 O 4C =	KK	-420	10
4	9	101	N 4K =	TB	130	20	9	4	103 N 3SA =	T2	400	35	14	7	107 O 2C +3	P3	-200	30
4	14	112	N 3K +2	TB	150	30	9	3	101 N 3SA =	C3	400	35	14	3	113 O 2C +3	T4	-200	30
4	6	109	N 3K +3	P7	170	40	9	1	111 N 3SA =	T3	400	35	14	13	104 O 2C +3	K4	-200	30
4	13	110	N 5K =	P5	600	65	9	13	107 N 3SA =	T8	400	35	14	6	105 O 2C +2	K4	-170	70
4	8	113	S 3SA =	T2	600	65	9	8	110 N 3SA =	T5	400	35	14	5	103 O 3C +1	KB	-170	70
4	7	111	S 3SA =	T2	600	65	9	2	113 N 4P =	T2	420	70	14	4	101 O 2C +2	P8	-170	70
4	5	107	S 3SA =	T2	600	65	9	12	104 N 3SA +1	TB	430	85	14	2	111 O 2C +2	T2	-170	70
4	2	102	N 3SA +2	C2	660	95	9	9	112 N 3SA +1	T2	430	85	14	1	109 O 3C +1	KK	-170	70
4	12	108	N 3SA +2	P8	660	95	9	10	114 N 3SA +2	T3	460	100	14	14	106 O 3C =	TA	-140	100
5	3	103	O 1SA -1	K8	50	10	10	8	110 W 3SA +3	K5	-690	0	15	12	101 O 2SA +1	K4	-150	0
5	7	110	O 2C -1	TA	50	10	10	5	105 O 4C +2	T8	-680	20	15	5	102 W 3C =	T6	-140	10
5	6	108	W 2P -1	K10	50	10	10	4	103 O 4C +2	TK	-680	20	15	8	108 N 3K -1	T8	-100	20
5	14	111	W 3T -2	K5	100	35	10	1	111 W 4C +2	K6	-680	20	15	6	104 W 4C -1	K6	50	30
5	8	112	O 3C -2	PA	100	35	10	13	107 O 4C +1	P9	-650	55	15	4	114 W 4P -2	K6	100	55
5	2	101	S 3K =	PK	110	65	10	12	104 W 4C +1	P9	-650	55	15	2	110 W 4C -2	K3	100	55
5	13	109	S 3K =	PK	110	65	10	10	114 W 4C +1	P9	-650	55	15	1	107 W 4C -2	K9	100	55
5	12	107	S 3K =	PK	110	65	10	9	112 O 4C +1	P4	-650	55	15	13	103 W 3SA -2	K3	100	55
5	10	102	S 3K =	PK	110	65	10	14	109 W 3SA +1	K3	-630	80	15	7	106 W 3T -3	K6	150	80
5	1	113	W 3P -3	K10	150	95	10	3	101 O 4C =	P6	-620	90	15	3	112 W 4C X -2	TA	300	90
5	9	114	W 4T -3	K10	150	95	10	2	113 W 6SA -1	K5	100	100	15	14	105 O 6T X -6	K4	1400	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 05.07.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
16	6	104	O 3SA +3 P2	-690	0	20	7	104 S 3SA +2 KK	660	86		25	5	110 S 5T -1 KA	-50	75	
16	8	108	W 3C = TA	-140	20	20	4	112 S 3SA +2 K7	660	86		25	2	104 S 4T -1 KA	-50	75	
16	7	106	W 3C = TA	-140	20	20	2	107 S 3SA +2 KK	660	86		25	10	107 S 4T = KA	130	95	
16	14	105	W 3C = TA	-140	20	20	1	105 S 3SA +2 K7	660	86		25	3	106 N 4T = PA	130	95	
16	13	103	O 2SA = P10	-120	40	21	14	102 S 3SA -3 K5	-300	0		26	9	105 O 4P +1 C2	-650	0	
16	2	110	W 3K = TA	-110	50	21	9	107 W 2K +1 TD	-110	15		26	12	111 O 4P = KA	-620	35	
16	4	114	O 4C -1 P10	100	60	21	6	101 W 3K = TD	-110	15		26	10	107 O 4P = C2	-620	35	
16	5	102	W 4C -2 TA	200	85	21	4	110 S 2SA -1 K9	-100	40		26	8	103 O 4P = KA	-620	35	
16	3	112	O 3SA -2 PD	200	85	21	3	108 S 1SA -1 K5	-100	40		26	7	101 O 4P = CB	-620	35	
16	1	107	O 4C -2 P10	200	85	21	1	104 S 3T -1 K8	-100	40		26	4	108 O 4P = C3	-620	35	
16	12	101	W 4C -2 TA	200	85	21	2	106 W 1SA -1 TD	50	60		26	2	104 O 4P = C2	-620	35	
17	7	105	W 2P +1 C10	-140	0	21	5	113 S 2C = K9	110	70		26	13	113 O 2P +2 TA	-170	70	
17	14	104	W 1P +1 C10	-110	9	21	8	105 S 2SA = P6	120	80		26	6	112 O 4P -1 CB	100	90	
17	5	101	S 2C -2 TD	-100	23	21	10	109 S 1SA X = K9	180	90		26	5	110 O 5P -1 KA	100	90	
17	13	102	S 3C -2 P8	-100	23	21	7	103 O 2C -4 T6	200	100		26	3	106 O 4P -1 KA	100	90	
17	2	108	S 2C -1 TD	-50	36	22	5	113 S 6SA -1 CA	-50	0		27	3	105 N 3SA -4 K4	-200	0	
17	6	103	W 2SA -1 K7	50	50	22	6	101 S 3K +1 T5	130	10		27	8	102 S 2C -3 P7	-150	10	
17	4	113	W 2SA -1 C10	50	50	22	8	105 S 3SA +2 C6	460	30		27	14	114 S 1SA -2 P3	-100	35	
17	3	111	O 3SA -2 C6	100	68	22	4	110 N 3SA +2 T8	460	30		27	12	110 S 1SA -2 P3	-100	35	
17	12	114	O 2K -2 PA	100	68	22	1	104 N 3SA +2 T7	460	30		27	9	104 S 1SA -2 P6	-100	35	
17	9	109	S 2C = P8	110	86	22	10	109 N 3SA +3 T7	490	70		27	4	107 S 1SA -2 P3	-100	35	
17	8	107	S 2C = KD	110	86	22	9	107 S 3SA +3 C10	490	70		27	7	113 S 1SA -1 K4	-50	70	
17	1	106	S 2C +1 K5	140	100	22	3	108 N 3SA +3 T8	490	70		27	6	111 N 1P -1 C4	-50	70	
18	7	105	O 3SA +3 T6	-490	5	22	2	106 N 3SA +3 T10	490	70		27	5	109 S 1SA -1 K7	-50	70	
18	3	111	O 3SA +3 K6	-490	5	22	14	102 N 3SA +3 T3	490	70		27	13	112 S 1SA = C5	90	95	
18	8	107	W 4P +2 K9	-480	23	22	7	103 S 6SA = CA	990	100		27	10	106 S 1SA = K10	90	95	
18	13	102	W 4P +2 TB	-480	23	23	8	104 N 4P -2 C6	-200	10		28	14	114 W 4C +1 K5	-450	15	
18	6	103	O 3SA +2 T3	-460	45	23	6	114 N 4P -2 C6	-200	10		28	8	102 W 4C +1 K5	-450	15	
18	4	113	O 3SA +2 K4	-460	45	23	5	111 N 4P -2 C6	-200	10		28	6	111 W 4C +1 T9	-450	15	
18	2	108	O 3SA +2 T6	-460	45	23	12	112 N 3SA -1 C6	-100	40		28	3	105 W 4C +1 KK	-450	15	
18	5	101	W 4P +1 TB	-450	64	23	7	102 N 4P -1 C6	-100	40		28	12	110 W 4C = P2	-420	55	
18	12	114	O 3SA +1 K4	-430	73	23	1	103 N 4P -1 C6	-100	40		28	10	106 W 4C = T8	-420	55	
18	14	104	O 3SA = T6	-400	82	23	4	109 N 3P = TA	140	60		28	9	104 W 4C = P6	-420	55	
18	9	109	O 1C +2 T7	-140	91	23	9	106 N 4P = TA	620	80		28	4	107 W 4C = K5	-420	55	
18	1	106	O 4C -2 K4	100	100	23	3	107 N 4P = K9	620	80		28	7	113 W 3C +1 P2	-170	80	
19	2	107	S 3SA -4 T7	-200	0	23	2	105 N 4P = C8	620	80		28	13	112 W 4C -1 T9	50	95	
19	8	106	N 3SA -3 T5	-150	9	23	10	108 N 4P +1 C6	650	100		28	5	109 W 4C -1 P2	50	95	
19	3	109	N 2C -1 K7	-50	23	24	12	112 S 5T -2 KA	-100	0							
19	13	101	S 2C -1 K9	-50	23	24	4	109 S 4T -1 PA	-50	15							
19	5	114	N 1P = C4	80	41	24	1	103 S 5T -1 PA	-50	15							
19	1	105	N 1P = TB	80	41	24	10	108 S 4T = PA	130	35							
19	6	102	N 1K +1 C2	90	59	24	7	102 S 3T +1 PA	130	35							
19	4	112	N 1SA = P7	90	59	24	9	106 S 3T +2 PA	150	55							
19	10	110	N 1K +2 P7	110	82	24	5	111 S 3T +2 PA	150	55							
19	9	108	N 1P +1 TB	110	82	24	2	105 S 3T +3 PA	170	70							
19	7	104	N 1K +2 TB	110	82	24	8	104 N 2SA +3 KK	210	80							
19	14	103	O2SAX-4 K2	1100	100	24	3	107 N 3SA +1 PB	430	90							
20	6	102	N 4C -1 K4	-100	0	24	6	114 S 3T X = PA	470	100							
20	14	103	W 3K -1 CA	100	9	25	7	101 W 4K X + TA	-910	0							
20	5	114	S 4T = KK	130	23	25	9	105 O 5C = KD	-650	15							
20	3	109	S 4T = KK	130	23	25	6	112 O 5C = TD	-650	15							
20	9	108	S 4T +1 K6	150	36	25	12	111 W 5K +1 TA	-620	30							
20	8	106	S 2SA +3 KK	210	45	25	13	113 W 4K +1 TA	-150	45							
20	10	110	S 5T +1 KK	620	55	25	8	103 O 4K +1 TA	-150	45							
20	13	101	S 3SA +1 KK	630	64	25	4	108 S 5T -2 KA	-100	60							

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.