

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 24.05.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	12	108	O 3SA =	P2	-400	0	6	14	110 N 3SA +2	T5	460	5	11	6	106 W 6P =	TA	-980	10
1	14	112	O 3T =	K5	-110	10	6	8	113 S 3SA +2	T7	460	5	11	15	109 W 6P =	TA	-980	10
1	9	102	W 3C -1	K8	50	25	6	3	103 N 4C +2	T8	480	55	11	14	107 W 6P =	TA	-980	10
1	8	115	O 4T -1	C2	50	25	6	2	101 N 4C +2	T5	480	55	11	5	104 W 4P +3	K6	-510	60
1	13	110	O 4T X -1	P2	100	50	6	1	114 N 4C +2	K4	480	55	11	4	102 W 4P +3	K6	-510	60
1	11	106	O 4T -2	K5	100	50	6	15	112 N 4C +2	PB	480	55	11	3	115 W 4P +3	K6	-510	60
1	10	104	W 3C -2	K7	100	50	6	12	106 N 4C +2	C4	480	55	11	1	111 W 4P +3	C4	-510	60
1	15	114	W 3C -3	K2	150	75	6	11	104 N 4C +2	PB	480	55	11	13	105 O 4P +3	T4	-510	60
1	6	111	O 4T -3	KK	150	75	6	10	102 N 4C +2	TD	480	55	11	12	103 W 4P +3	K6	-510	60
1	7	113	W 3C -4	K2	200	90	6	9	115 N 4C +2	PB	480	55	11	11	101 W 4P +3	C10	-510	60
1	1	101	W 4C X -4	P4	800	100	6	13	108 N 6C =	K4	980	100	11	2	113 W 4P +1	K6	-450	100
2	14	112	N 6SA -1	C2	-100	0	7	12	105 O 4C =	K7	-620	0	12	2	113 N 2SA -2	KA	-200	0
2	8	115	S 5K =	P4	600	10	7	2	115 W 3SA =	K5	-600	15	12	4	102 O 3K +1	P3	-130	15
2	13	110	S 3SA +2	C8	660	35	7	11	103 W 3SA =	K3	-600	15	12	15	109 O 3K +1	P3	-130	15
2	11	106	S 3SA +2	C5	660	35	7	13	107 O 3P +2	T5	-200	30	12	5	104 O 2C =	P3	-110	40
2	9	102	N 3SA +2	C2	660	35	7	15	111 O 2P +1	K7	-140	45	12	13	105 O 3K =	P3	-110	40
2	7	113	S 3SA +2	C3	660	35	7	10	101 O 2P +1	K7	-140	45	12	12	103 O 2C =	P3	-110	40
2	1	101	N 3SA +3	P2	690	75	7	3	102 O 2C =	K7	-110	70	12	3	115 N 2SA -1	KA	-100	65
2	12	108	N 3SA +3	P2	690	75	7	1	113 O 2C =	K7	-110	70	12	14	107 S 2P -1	C4	-100	65
2	10	104	N 3SA +3	C7	690	75	7	9	114 O 2C =	TA	-110	70	12	6	106 O 2C -1	K10	50	90
2	6	111	S 3SA +3	P10	690	75	7	4	104		0	90	12	1	111 O 2C -1	K10	50	90
2	15	114	N 6SA =	K4	1440	100	7	14	109 W 3SA -1	TK	100	100	12	11	101 O 3K -1	C9	50	90
3	11	105	S 5SA -3	T4	-150	0	8	4	104 N 4C -1	T10	-50	5	13	5	103 W 3P +1	KK	-170	5
3	1	115	S 3SA -1	KB	-50	10	8	14	109 N 4C -1	T10	-50	5	13	3	114 W 2P +2	TK	-170	5
3	8	114	S 1K =	C4	70	20	8	2	115 S 3SA =	PB	400	20	13	12	102 O 2C =	K8	-110	20
3	2	102	S 1T +1	C4	90	30	8	12	105 S 3SA +1	PB	430	45	13	6	105 O 2C -1	P8	100	45
3	13	109	S 2SA =	T2	120	40	8	11	103 S 3SA +1	C3	430	45	13	2	112 W 3P -1	C4	100	45
3	14	111	S 1K +3	C6	130	50	8	10	101 S 3SA +1	PB	430	45	13	15	108 W 3P -1	K3	100	45
3	7	112	S 2K +3	T2	150	60	8	9	114 S 3SA +1	PB	430	45	13	14	106 W 4P -1	K3	100	45
3	9	101	S 2SA +2	C4	180	70	8	3	102 S 3SA +2	PB	460	85	13	4	101 S 3K =	C7	110	70
3	12	107	S 3SA =	KB	400	85	8	1	113 S 3SA +2	K5	460	85	13	7	107 W 3P -2	T5	200	85
3	10	103	S 3SA =	C6	400	85	8	15	111 S 3SA +2	PB	460	85	13	13	104 O 2C -2	K6	200	85
3	15	113	S 3SA +1	T5	430	100	8	13	107 S 3SA +2	PB	460	85	13	1	110 W 4P -3	P3	300	100
4	14	111	W 4C +2	PB	-680	10	9	5	105 N 3K +1	PA	130	25	14	5	103 N3SAX-3	C9	-500	0
4	12	107	W 4C +2	P5	-680	10	9	4	103 N 3K +1	TA	130	25	14	14	106 O 2C +1	PA	-140	10
4	10	103	W 4C +2	PB	-680	10	9	15	110 N 3K +1	TA	130	25	14	1	110 O 2C =	PA	-110	20
4	1	115	W 4C +1	PB	-650	50	9	14	108 N 3K +1	TA	130	25	14	7	107 S 3K -1	C6	-50	35
4	13	109	W 4C +1	K7	-650	50	9	12	104 N 3K +1	PA	130	25	14	13	104 N 3SA -1	T4	-50	35
4	11	105	W 4C +1	K7	-650	50	9	11	102 N 3K +1	PA	130	25	14	6	105 O 3C -1	P8	50	55
4	9	101	W 4C +1	P10	-650	50	9	3	101 N 3K +2	PA	150	70	14	4	101 O 3C -1	PA	50	55
4	8	114	W 4C +1	K7	-650	50	9	2	114 N 3K +2	PA	150	70	14	3	114 O 3C -2	T5	100	75
4	2	102	W 4C =	PB	-620	85	9	1	112 N 3K +2	TA	150	70	14	2	112 O 2C -2	PA	100	75
4	7	112	W 4C =	PB	-620	85	9	13	106 W 4C X -1	KA	200	90	14	12	102 N 2SA +1	CB	150	90
4	15	113	O 4C -1	PA	100	100	9	10	115 W 3C X -3	KA	800	100	14	15	108 N 2SA +3	CB	210	100
5	9	115	N 3SA -3	T2	-300	0	10	15	110 N 4P -3	CA	-300	0	15	8	108 S 3P -3	T8	-300	0
5	12	106	S 1SA -2	P8	-200	15	10	3	101 N 3P -1	CA	-100	15	15	5	102 W 3K +1	P3	-130	15
5	10	102	S 3SA -2	C3	-200	15	10	11	102 S 1SA -1	K3	-100	15	15	14	105 W 3K +1	TA	-130	15
5	13	108	W 2P =	TD	-110	30	10	2	114 S 1SA =	K3	90	40	15	2	111 S 3T -1	KA	-100	40
5	1	114	S 3SA -1	P8	-100	40	10	1	112 S 1SA =	K3	90	40	15	1	109 S 3SA -1	KA	-100	40
5	3	103	N 2K +1	C9	110	75	10	10	115 S 1SA =	T4	90	40	15	15	107 S 2P -1	T8	-100	40
5	2	101	N 2K +1	C2	110	75	10	4	103 N 2P =	CA	110	65	15	3	113 N 3T =	K8	110	65
5	15	112	S 3T =	PA	110	75	10	14	108 N 1P +1	CA	110	65	15	13	103 N 2C =	KD	110	65
5	14	110	N 3K =	P10	110	75	10	5	105 S 1SA +1	K2	120	85	15	7	106 S 2SA =	K5	120	85
5	11	104	S 3T =	K10	110	75	10	12	104 S 2SA =	K3	120	85	15	4	115 S 2SA =	K7	120	85
5	8	113	S 2T +1	PA	110	75	10	13	106 O 3SA -2	TK	200	100	15	6	104 S 3T +1	CA	130	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 24.05.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
16	7	106	O 3C = TB	-140	5	21	4	112	W 6SA = KA	-990	0	26	13	113	S 3SA -1 T7	-100	15
16	15	107	O 3C = TB	-140	5	21	11	111	O 3SA +3 C5	-490	35	26	12	111	N 3SA -1 CB	-100	15
16	2	111	W 2K +2 T4	-130	20	21	8	105	W 3SA +3 C2	-490	35	26	11	109	N 3T -1 CA	-100	15
16	1	109	W 3K = TK	-110	30	21	7	103	W 3SA +3 CB	-490	35	26	9	105	N 3SA -1 CB	-100	15
16	13	103	S 4T -2 CA	-100	40	21	6	101	W 3SA +3 CB	-490	35	26	4	110	N 3T = T6	110	40
16	6	104	S 4T -1 CA	-50	50	21	5	114	O 3SA +3 C5	-490	35	26	10	107	N 3SA = C10	600	70
16	8	108	O 4C -1 KA	100	75	21	2	108	W 3SA +3 CB	-490	35	26	8	103	N 3SA = C9	600	70
16	5	102	O 4C -1 KA	100	75	21	10	109	W 3SA +2 P2	-460	85	26	7	101	N 3SA = C9	600	70
16	3	113	O 3C -1 TB	100	75	21	9	107	W 3SA +2 K2	-460	85	26	5	112	N 3SA = C6	600	70
16	14	105	O 4C -1 KA	100	75	21	3	110	O 3SA +2 C4	-460	85	26	3	108	N 3SA = CB	600	70
16	4	115	O 5C -3 PA	300	100	21	1	106	O 3SA +2 C5	-460	85	26	6	114	N 3SA +2 P2	660	100
17	9	109	S 3SA +2 P4	460	0	22	11	111	W 6P = CA	-1430	0	27	14	114	O 4SA +1 KA	-460	0
17	2	110	N 3SA +3 C5	490	15	22	10	109	W 4P +2 CA	-680	30	27	11	108	W 4P +1 P2	-450	30
17	14	104	N 3SA +3 C5	490	15	22	8	105	W 4P +2 CA	-680	30	27	10	106	W 4P +1 K4	-450	30
17	8	107	N 6SA = C6	990	60	22	5	114	W 4P +2 CA	-680	30	27	9	104	W 4P +1 K6	-450	30
17	7	105	S 6SA = C3	990	60	22	4	112	W 5P +1 CA	-680	30	27	7	115	W 4P +1 C9	-450	30
17	6	103	N 6SA = C5	990	60	22	1	106	W 5P +1 CA	-680	30	27	4	109	W 4P +1 K6	-450	30
17	5	101	S 6SA = P4	990	60	22	9	107	W 5P = CA	-650	65	27	12	110	O 3SA +1 C4	-430	60
17	4	114	N 6SA = P7	990	60	22	6	101	W 4P +1 CA	-650	65	27	13	112	W 4P = K6	-420	75
17	3	112	N 6SA = C5	990	60	22	2	108	W 4P = CA	-620	80	27	8	102	W 4P = P2	-420	75
17	1	108	N 6SA = C5	990	60	22	7	103	N 5C -2 PK	-100	95	27	6	113	W 2K +1 T3	-110	90
17	15	106	N 6SA +1 C5	1020	100	22	3	110	N 5C X -1 T9	-100	95	27	5	111	W 6P X -1 C3	100	100
18	14	104	W 4P X -1 K5	100	0	23	12	112	W 3SA +2 T6	-660	20	28	13	112	W 5C = K4	-450	15
18	8	107	S 4K +2 C2	170	15	23	11	110	O 3SA +2 T4	-660	20	28	9	104	O 4C +1 P9	-450	15
18	2	110	S 4K +2 C2	170	15	23	7	102	W 3SA +2 TB	-660	20	28	7	115	W 4C +1 PD	-450	15
18	7	105	W 4P X -2 KD	300	30	23	4	111	W 3SA +2 T6	-660	20	28	4	109	W 4C +1 TA	-450	15
18	4	114	S 5K +1 C2	620	40	23	2	107	W 3SA +2 TB	-660	20	28	10	106	W 5K +1 C9	-420	45
18	5	101	S 5K +2 PA	640	50	23	10	108	W 4C +1 T7	-650	55	28	8	102	W 5K +1 C9	-420	45
18	15	106	N 4C +2 P8	680	60	23	3	109	W 4C +1 KA	-650	55	28	12	110	N 4P -3 CK	-300	60
18	3	112	N 3SA +3 P5	690	70	23	9	106	W 3SA +1 K2	-630	80	28	14	114	N 4P -2 KD	-200	70
18	6	103	N 5C +2 P10	710	85	23	8	104	W 3SA +1 T6	-630	80	28	5	111	W 3K +3 C9	-170	80
18	1	108	N 5C +2 P10	710	85	23	6	115	W 3SA +1 TB	-630	80	28	11	108	N 3P -1 CK	-100	90
18	9	109	N 3SA +4 P10	720	100	23	5	113	W 2C = P10	-110	100	28	6	113	N 3P +1 K9	170	100
19	15	105	S 4C X -2 T8	-300	0	24	7	102	S 2C -1 P2	-50	15	29	13	111	W 2K +2 TD	-130	5
19	7	104	S 4C -3 P2	-150	10	24	6	115	N 3SA -1 C3	-50	15	29	5	110	W 4K = TD	-130	5
19	9	108	S 4C -2 P3	-100	40	24	5	113	N 3SA -1 C7	-50	15	29	12	109	W 3K = PA	-110	25
19	6	102	S 3C -2 T5	-100	40	24	4	111	N 2SA -1 PA	-50	15	29	8	101	W 3K = PA	-110	25
19	3	111	S 4C -2 K2	-100	40	24	9	106	N 1SA = PA	90	40	29	15	115	N 3P -1 K6	-100	55
19	2	109	S 4C -2 P2	-100	40	24	8	104	W 2T -2 KA	100	55	29	14	113	N 3P -1 K6	-100	55
19	1	107	N 4C -2 T8	-100	40	24	3	109	W 1SAX -1 KA	100	55	29	10	105	N 3P -1 K6	-100	55
19	10	110	S 4C -1 P2	-50	80	24	12	112	N 2SA = K6	120	75	29	7	114	N 3P -1 K2	-100	55
19	8	106	S 3C -1 T8	-50	80	24	2	107	N 2SA = PA	120	75	29	11	107	N 2P = K6	110	85
19	5	115	S 3C -1 P2	-50	80	24	11	110	N 1SA +2 PA	150	90	29	6	112	N 2P = K6	110	85
19	4	113	S 3C +1 P2	170	100	24	10	108	W 2T X -3 KA	500	100	29	9	103	S 3P = KA	140	100
20	2	109	O 1T +5 C8	-170	0	25	12	111	N 4C -1 P8	-50	15	30	15	115	O 4C +2 KA	-480	20
20	7	104	O 4T = CA	-130	20	25	9	105	N 3C -1 P8	-50	15	30	13	111	O 4C +2 KA	-480	20
20	6	102	O 4T = C2	-130	20	25	8	103	N 4C -1 P8	-50	15	30	12	109	O 4C +2 KA	-480	20
20	15	105	O 4T = C3	-130	20	25	6	114	N 4C -1 P2	-50	15	30	6	112	O 4C +2 KA	-480	20
20	5	115	O 3T = P4	-110	40	25	4	110	N 3C = PA	140	40	30	5	110	O 4C +2 KA	-480	20
20	3	111	O 1SA = P7	-90	50	25	13	113	N 3C +1 P8	170	55	30	14	113	W 3SA +2 TD	-460	70
20	8	106	O 4T -1 T8	100	65	25	7	101	N 3C +1 P8	170	55	30	11	107	W 3SA +2 T2	-460	70
20	1	107	W 4T -1 CA	100	65	25	11	109	N 4C = P8	420	85	30	9	103	W 3SA +2 TD	-460	70
20	10	110	N 3C +1 TA	170	85	25	10	107	N 4C = K9	420	85	30	8	101	O 3SA +2 KA	-460	70
20	9	108	N 3C +1 TA	170	85	25	5	112	N 4C = P8	420	85	30	7	114	W 3SA +2 T5	-460	70
20	4	113	O 2SA -2 P2	200	100	25	3	108	N 4C = P8	420	85	30	10	105	W 4P = K7	-420	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.