

# Board-Anschriften (aus Sicht NS), Mitchell-Turnier Samstag - Mensa, Pfäffikon - 23.04.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz					
1	10	107	N 2SA -1	T6	-50	7	7	9	102	O 2SA -2	C2	200	100	14	12	107	O 3P +1	C2	-170	93
1	8	103	S 3SA -1	CK	-50	7	8	3	103	N 4K +1	TD	150	0	14	10	102	O 3P +1	C5	-170	93
1	12	111	N 1C +1	T5	110	29	8	1	111	N 4K +2	K10	170	21	15	2	111	W 3K X =	P7	-470	0
1	5	108	N 2SA =	K8	120	43	8	10	105	N 3K +3	T6	170	21	15	11	104	W 3SA +1	CK	-430	14
1	6	110	N 3C =	K3	140	57	8	9	102	N 5K =	PA	400	43	15	4	103	O 3SA =	T8	-400	29
1	11	109	N 1C +3	TB	170	79	8	12	109	N 5K +1	PA	420	71	15	1	109	W 1SA +2	K6	-150	43
1	9	105	S 2P +2	K9	170	79	8	11	107	N 5K +1	PA	420	71	15	5	105	O 3SA -1	PD	50	71
1	1	101	N 4C =	K5	420	100	8	7	110	N 5K +1	PA	420	71	15	3	101	W 2SA -1	P5	50	71
2	12	111	O 4P +3	CB	-510	7	8	2	101	N 6K =	PA	920	100	15	10	102	W 3SA -1	K8	50	71
2	9	105	O 5P +2	C7	-510	7	9	7	110	S 3SA -1	K7	-50	0	15	12	107	W 3SA -2	C4	100	100
2	6	110	O 4P +2	CB	-480	29	9	3	103	S 3SA =	C8	400	29	16	12	105	O 2C =	PA	-110	0
2	1	101	O 5P =	K10	-450	64	9	2	101	N 3SA =	T2	400	29	16	10	101	N 1SA -2	C4	-100	14
2	11	109	O 5P =	K10	-450	64	9	10	105	S 3SA =	C2	400	29	16	1	108	N 3K -1	T2	-50	36
2	10	107	O 4P +1	K2	-450	64	9	1	111	S 3SA +1	P9	430	79	16	11	103	N 3K -1	T2	-50	36
2	5	108	O 4P +1	K5	-450	64	9	12	109	S 3SA +1	C9	430	79	16	5	104	N 2K +1	T2	110	64
2	8	103	O 6P -1	K10	50	100	9	11	107	S 3SA +1	C2	430	79	16	4	102	N 3K =	T2	110	64
3	1	101	W 2C +1	TK	-140	7	9	9	102	S 3SA +1	T9	430	79	16	2	110	N 3K +1	T2	130	86
3	6	110	W 2C +1	TK	-140	7	10	8	111	O 3SA +3	C2	-690	0	16	6	106	O 3C -2	PA	200	100
3	12	111	W 3C -1	TK	100	57	10	4	104	O 3SA +2	P4	-660	14	17	4	102	O 1C =	KK	-80	0
3	11	109	W 2C -1	P3	100	57	10	1	110	O 5T =	P8	-600	29	17	12	105	O 2C -1	T9	50	14
3	9	105	W 2C -1	K4	100	57	10	12	108	O 3T +1	K6	-130	50	17	6	106	S 2SA +1	C7	150	64
3	8	103	W 2C -1	K5	100	57	10	9	101	O 4T =	P4	-130	50	17	5	104	S 2SA +1	C7	150	64
3	5	108	W 3C -1	TK	100	57	10	10	103	O 3T =	C5	-110	71	17	2	110	N 2SA +1	C7	150	64
3	10	107	W 2C -2	K4	200	100	10	11	106	N 3P -1	TB	-100	86	17	1	108	S 1SA +2	C7	150	64
4	8	101	S 3P -2	CA	-200	0	10	3	102	O 3SA -1	P8	100	100	17	11	103	S 1SA +2	C7	150	64
4	2	102	W 2C =	T7	-110	14	11	12	108	N 4P X -2	K8	-300	0	17	10	101	S 2SA +1	C7	150	64
4	11	108	W 3C -1	T8	100	50	11	8	111	W 4T =	P8	-130	14	18	10	101	O 2SA =	P5	-120	0
4	10	106	W 3C -1	T7	100	50	11	10	103	W 5T -1	KA	50	36	18	4	102	O 1SA =	P2	-90	14
4	7	111	W 4C -1	KA	100	50	11	9	101	O 5T -1	CA	50	36	18	6	106	O 2SA -1	P2	50	43
4	6	109	W 4C -1	KB	100	50	11	4	104	O 5T X -1	CA	100	57	18	1	108	O 2SA -1	PB	50	43
4	12	110	N 2K +1	C4	110	86	11	11	106	S 4K =	PA	130	71	18	12	105	O 2SA -1	P2	50	43
4	9	104	S 3P +1	CA	170	100	11	3	102	N 3P =	K8	140	86	18	5	104	O 3SA -2	P2	100	79
5	2	102	N 2C +1	P10	140	50	11	1	110	N 2P +2	TA	170	100	18	2	110	O 3SA -2	P2	100	79
5	12	110	S 2C +1	P6	140	50	12	4	104	N 3C -3	P10	-300	0	18	11	103	O 3SA -4	P2	200	100
5	11	108	N 2C +1	TK	140	50	12	12	108	N 3C -2	P10	-200	21	19	4	101	S 3P -4	TA	-200	0
5	10	106	N 2C +1	KA	140	50	12	9	101	N 3C -2	P10	-200	21	19	6	105	W 3T =	K7	-110	19
5	9	104	N 2C +1	P2	140	50	12	10	103	N 2C -1	P10	-100	43	19	1	106	W 3T =	C6	-110	19
5	8	101	N 2C +1	P10	140	50	12	1	110	W 1P =	K8	-80	57	19	7	107	N 3K =	TK	110	44
5	7	111	N 2C +1	K3	140	50	12	3	102	W 3SA -1	C2	50	71	19	5	103	N 1P +1	C9	110	44
5	6	109	N 2C +1	TK	140	50	12	8	111	O 4T -2	C10	100	86	19	12	104	S 3C =	TA	140	62
6	9	104	W 4P +1	KA	-650	0	12	11	106	N 2C =	TA	110	100	19	11	102	N 1SA +3	K5	180	75
6	11	108	W 3P +2	KA	-200	14	13	5	105	N 3K +1	C9	130	29	19	3	111	W 5T X -3	KA	800	94
6	6	109	W 3P +1	C4	-170	29	13	4	103	N 3K +1	T7	130	29	19	2	109	W 4T X -3	KA	800	94
6	2	102	W 3P =	KA	-140	57	13	1	109	N 3K +1	C2	130	29	20	5	103	O 1C +1	P8	-110	0
6	10	106	W 3P =	KA	-140	57	13	11	104	N 2K +2	C6	130	29	20	7	107	N 2P -1	C3	-100	44
6	7	111	W 3P =	KA	-140	57	13	10	102	N 3K +1	C9	130	29	20	6	105	N 2P -1	C3	-100	44
6	12	110	W 4P -1	KA	100	86	13	3	101	N 1SA +3	C5	180	79	20	3	111	N 2P -1	TA	-100	44
6	8	101	O 4T -2	C2	200	100	13	12	107	N 1SA +3	C2	180	79	20	1	106	N 2P -1	TA	-100	44
7	1	111	O 3SA =	C2	-600	0	13	2	111	O 4C X -3	TA	800	100	20	12	104	N 2P -1	C3	-100	44
7	3	103	O 2SA +1	C5	-150	14	14	5	105	O 4P +1	KD	-450	14	20	11	102	N 2P -1	C3	-100	44
7	2	101	O 2T +1	C2	-110	36	14	3	101	O 4P +1	C4	-450	14	20	4	101	N 2P =	C3	110	88
7	12	109	O 2T +1	C2	-110	36	14	2	111	O 4P +1	C5	-450	14	20	2	109	N 3P =	C2	140	100
7	11	107	O 3SA -1	PD	100	71	14	4	103	O 3P +2	C4	-200	57	21	5	103	W 2C X =	PA	-470	0
7	10	105	O 3SA -1	C3	100	71	14	1	109	O 3P +2	PA	-200	57	21	4	101	N 2SA -2	C3	-200	12
7	7	110	O 3SA -1	C2	100	71	14	11	104	O 3P +2	C2	-200	57	21	2	109	N 3SA -1	C3	-100	25

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Samstag - Mensa, Pfäffikon - 23.04.2016**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
21	6	105	N 2SA =	K6	120	44	27	3	108 O 4C -1	K10	50	75	34	10	108 N 3P +1	P6	170	29
21	3	111	N 2SA =	C8	120	44	27	2	106 O 4C X -2	P5	300	100	34	8	104 N 4C =	C3	620	50
21	7	107	N 2SA +1	K2	150	62	28	6	102 N 2SA -2	C8	-200	0	34	5	109 N 4P =	T4	620	50
21	1	106	N 2SA +2	C3	180	75	28	9	108 W 1SA =	K3	-90	14	34	9	106 N 4P +1	KA	650	79
21	12	104	N 3SA =	C3	600	88	28	10	110 W 2K -1	T4	50	43	34	7	102 N 4P +1	T6	650	79
21	11	102	N 3SA +1	TA	630	100	28	8	106 W 1SA -1	K3	50	43	34	11	110 N 4P +2	KB	680	100
22	7	106	N 1SA -2	T6	-100	7	28	3	107 O 2K -1	T5	50	43	35	10	108 N 2P +2	T4	170	7
22	6	104	N 3C -2	P6	-100	7	28	4	109 O 4P -2	TD	100	71	35	5	109 N 2P +2	CA	170	7
22	2	107	N 1SA -1	T6	-50	29	28	7	104 W 3SA -3	T4	150	86	35	8	104 N 2P +3	K6	200	29
22	1	105	N 1SA =	T6	90	43	28	2	105 S 3SA =	TA	600	100	35	9	106 N 4P =	CA	420	64
22	8	108	N 3C =	P6	140	71	29	9	108 S 4C -1	PA	-100	7	35	7	102 N 4P =	CA	420	64
22	5	102	N 3C =	KK	140	71	29	2	105 N 6C -1	K9	-100	7	35	6	111 N 4P =	T4	420	64
22	3	110	N 3C =	P9	140	71	29	8	106 O 3P -1	C4	100	29	35	4	107 N 4P =	CA	420	64
22	12	103	N 3C +1	KK	170	100	29	4	109 S 3C =	PA	140	43	35	11	110 N 4P +1	CA	450	100
23	6	104	W 3SA =	K6	-600	0	29	3	107 N 1T +4	KK	150	57	36	4	107 S 4K X -4	TA	-1100	0
23	5	102	O 1C +3	KD	-170	14	29	7	104 W 4P -2	CK	200	71	36	8	104 W 4P +1	C2	-650	21
23	8	108	W 2SA +1	T8	-150	36	29	10	110 S 4C +1	PA	650	93	36	5	109 W 4P +1	C5	-650	21
23	12	103	O 2SA +1	T7	-150	36	29	6	102 S 4C +1	PA	650	93	36	11	110 W 4P =	C2	-620	57
23	3	110	O 1SA +1	P5	-120	64	30	4	109 W 4C =	KD	-420	0	36	10	108 W 4P =	T2	-620	57
23	1	105	O 1SA +1	T3	-120	64	30	3	107 W 3C +1	KD	-170	14	36	6	111 W 4P =	C3	-620	57
23	7	106	O 2K =	T7	-90	86	30	9	108 N 1SA -3	T5	-150	36	36	7	102 W 3P +1	C2	-170	86
23	2	107	O 3K -1	P2	100	100	30	2	105 N 3P -3	TD	-150	36	36	9	106 W 4P -1	C3	100	100
24	6	104	S 3SA -1	CB	-50	7	30	10	110 W 2C +1	KD	-140	64						
24	2	107	N 2K -1	C5	-50	7	30	8	106 W 2C +1	TD	-140	64						
24	3	110	S 1SA +1	K5	120	36	30	6	102 S 2P -2	CA	-100	86						
24	12	103	S 1SA +1	C9	120	36	30	7	104 S 3K -1	CA	-50	100						
24	8	108	S 2SA +1	CB	150	71	31	7	103 S 4C -2	P4	-200	6						
24	5	102	S 2SA +1	CB	150	71	31	6	101 S 4C -2	T8	-200	6						
24	1	105	S 2SA +1	C4	150	71	31	11	111 S 4C -1	T8	-100	44						
24	7	106	S 3SA =	C4	400	100	31	9	107 S 3C -1	T2	-100	44						
25	5	101	O 4C +2	PK	-680	0	31	8	105 S 4C -1	T2	-100	44						
25	7	105	O 4C +1	PK	-650	25	31	5	110 S 4C -1	T8	-100	44						
25	4	111	O 4C +1	PK	-650	25	31	10	109 S 3C =	T8	140	88						
25	3	108	O 4C +1	PK	-650	25	31	4	108 S 2C +1	T8	140	88						
25	9	109	O 4C =	PK	-620	56	31	3	106 S 2C +1	T2	140	88						
25	8	107	O 4C =	PK	-620	56	32	7	103 N 3P -1	CA	-50	6						
25	1	104	O 3C +2	PK	-200	75	32	6	101 N 3P -1	CA	-50	6						
25	6	103	O 3C +1	PK	-170	94	32	4	108 O 3C -1	PD	100	25						
25	2	106	O 3C +1	P5	-170	94	32	11	111 N 2P =	P5	110	38						
26	7	105	O 3SA +1	T3	-630	6	32	10	109 N 2P +1	CA	140	56						
26	5	101	O 3SA +1	T3	-630	6	32	9	107 N 2P +1	CA	140	56						
26	9	109	O 3SA =	P6	-600	38	32	8	105 N 3P +1	CA	170	88						
26	6	103	W 5K =	CA	-600	38	32	5	110 N 3P +1	C10	170	88						
26	4	111	O 5K =	C6	-600	38	32	3	106 N 2P +2	CA	170	88						
26	2	106	N 4P -1	KA	-100	62	33	8	105 W 4C +3	P8	-510	6						
26	8	107	O 3SA -1	P9	100	88	33	5	110 W 4C +3	P8	-510	6						
26	3	108	W 5K -1	CA	100	88	33	10	109 O 3SA +3	P9	-490	25						
26	1	104	O 3SA -1	P9	100	88	33	9	107 W 4C +1	P2	-450	38						
27	9	109	W 3SA +1	P4	-430	6	33	11	111 W 4C =	P8	-420	62						
27	6	103	W 3SA +1	K4	-430	6	33	4	108 W 4C =	P8	-420	62						
27	5	101	O 4C =	K10	-420	25	33	3	106 W 4C =	K4	-420	62						
27	7	105	W 3SA =	KD	-400	44	33	7	103 W 3C +3	P8	-230	94						
27	1	104	W 3SA =	K4	-400	44	33	6	101 W 3C +3	K4	-230	94						
27	8	107	W 3SA -1	K4	50	75	34	6	111 N 4P -2	P6	-200	0						
27	4	111	O 4C -1	K10	50	75	34	4	107 N 2P +1	C3	140	14						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.