

# NS-Resultate Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 19.04.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
1	1	101	N 4K -2	T8	-100	21	23	3	105	N 4P -1	C4	-100	21	24	6	104	O 2P +1	CA	-140	54
2	1	101	S 5K =	TA	600	71	24	3	105	O 2P +1	CA	-140	54	1	7	105	N 2T -1	K4	-50	62
3	1	101	W 2C +2	KK	-170	42	4	4	105	S 4C +2	T4	680	75	2	7	105	S 5K =	TA	600	71
4	1	108	S 4C +2	T2	680	75	5	4	105	O 3K =	T2	-110	58	3	7	105	O 2P -1	T3	100	79
5	1	108	W 1P +2	TA	-140	29	6	4	105	O 3K =	CA	-110	21	4	7	104	S 4C +2	T2	680	75
6	1	108	S 3C -2	K8	-100	54	10	4	104	W 4C -1	PA	100	38	5	7	104	O 2C =	T10	-110	58
7	1	107	S 3SA =	CA	600	92	11	4	104	N 4C =	KA	420	83	6	7	104	O 3K =	CA	-110	21
8	1	107	N 6P +1	C4	1010	71	12	4	104	N 4C +1	KD	650	33	7	7	102	N 2T +2	KA	130	75
9	1	107	N 4C =	KA	420	92	13	4	103	O 2SA -1	T3	100	50	8	7	102	N 6P +1	C10	1010	71
13	1	104	O 2SA =	P10	-120	8	14	4	103	O 3C +1	K2	-170	4	9	7	102	N 4C =	KA	420	92
14	1	104	O 4C -3	PB	150	85	15	4	103	S 4C +2	PA	680	46	10	7	101	W 4P -2	C4	200	67
15	1	104	S 4C +2	PA	680	46	16	4	102	O 4P =	T2	-620	67	11	7	101	N 5C =	K3	450	100
16	1	103	W 4P +1	T5	-650	21	17	4	102	S 3P +1	K7	170	83	12	7	101	S 3SA +3	C2	690	88
17	1	103	S 3P =	K7	140	62	18	4	102	O 2C +1	PK	-140	12	13	7	108	W 3SA -2	C3	200	88
18	1	103	O 3C -1	KA	50	67	19	4	101	S 3P +1	TA	170	71	14	7	108	N 4P X -1	CA	-100	15
19	1	102	S 3P +1	C6	170	71	20	4	101	N 2P =	CK	110	79	15	7	108	S 6C =	PA	1430	88
20	1	102	S 2P =	K5	110	79	21	4	101	S 4P +1	KB	650	33	19	7	107	N 3SA =	C5	400	92
21	1	102	S 3SA +2	T2	660	62	22	4	107	O 3K +1	CB	-130	62	20	7	107	N 2P =	CK	110	79
4	2	102	S 4C +1	T4	650	38	23	4	107	S 4P -1	CA	-100	21	21	7	107	S 3SA +2	C5	660	62
5	2	102	O 1K +2	T5	-110	58	24	4	107	S 2C -2	P8	-100	96	1	8	107	N 2K -2	PA	-100	21
6	2	102	O 2K =	CA	-90	71	1	5	108	O 2P -1	T9	50	88	2	8	107	S 6C -2	TA	-200	4
7	2	101	S 3SA +1	C4	630	100	2	5	108	S 4C +2	TA	680	100	3	8	107	W 4C -1	T9	100	79
8	2	101	N 4P +3	C10	510	17	3	5	108	W 4C +1	T5	-650	12	7	8	105	W 3C =	TA	-140	25
9	2	101	S 4C -1	K2	-50	17	4	5	107	S 4C +2	T2	680	75	8	8	105	N 6P +1	P8	1010	71
10	2	108	W 4P -2	K10	200	67	5	5	107	O 2C =	K8	-110	58	9	8	105	N 3C =	KA	140	62
11	2	108	O 4P +1	CA	-450	0	6	5	107	N 3C -1	PD	-50	83	10	8	103	W 1P +1	K10	-110	12
12	2	108	S 2SA +2	P9	180	8	13	5	105	W 3SA -1	C3	100	50	11	8	103	N 4C -1	TD	-50	33
13	2	107	O 3SA -1	T3	100	50	14	5	105	N 3P =	CA	140	69	12	8	103	S 3SA +2	C2	660	54
14	2	107	O 3C -1	PB	50	42	15	5	105	S 4C +2	PA	680	46	13	8	102	W 1SA -1	C3	100	50
15	2	107	S 4C +2	PA	680	46	16	5	104	W 4P =	K2	-620	67	14	8	102	O 3C -2	PB	100	54
16	2	105	W 4P +1	C9	-650	21	17	5	104	W 2SA =	C6	-120	8	15	8	102	S 4C +2	PA	680	46
17	2	105	O 3K +1	P4	-130	0	18	5	104	O 2C =	PK	-110	38	16	8	101	O 4P =	C7	-620	67
18	2	105	S 2SA -1	CB	-100	50	19	5	103	O 3C =	C10	-140	8	17	8	101	W 5T -4	P3	200	96
19	2	104	S 4P =	TA	420	100	20	5	103	O 2C +2	KB	-170	17	18	8	101	S 1SA +2	K3	150	100
20	2	104	N 3P -1	CK	-100	46	21	5	103	S 3SA +1	C5	630	25	22	8	108	W 2C +2	T8	-170	25
21	2	104	N 2K +2	C3	130	0	22	5	102	O 3P =	TA	-140	46	23	8	108	S 3P +1	CA	170	79
22	2	103	W 4C =	K7	-620	8	23	5	102	S 4P -1	CA	-100	21	24	8	108	O 4T =	CA	-130	71
23	2	103	S 4P -1	CA	-100	21	24	5	102	O 2P =	CA	-110	83	1	201	301	O 2K =	TK	-90	42
24	2	103	S 3C -3	P8	-150	38	1	6	103	W 2P -1	C2	50	88	2	201	301	S 3K +2	TA	150	33
1	3	104	N 1SA -1	P3	-50	62	2	6	103	S 5K =	TA	600	71	3	201	301	W 4C -2	T5	200	100
2	3	104	N 2C +2	T3	170	42	3	6	103	W 4C +1	T4	-650	12	4	201	308	S 4C +2	T4	680	75
3	3	104	W 4C +2	TK	-680	0	4	6	101	N 4C +2	TA	680	75	5	201	308	O 2SA +1	T2	-150	17
7	3	103	N 4T =	KA	130	75	5	6	101	W 2P =	TA	-110	58	6	201	308	O 2K =	CA	-90	71
8	3	103	S 4P +3	KB	510	17	6	6	101	S 3C -2	KD	-100	54	7	201	307	W 2C =	TA	-110	42
9	3	103	S 4C -1	P9	-50	17	7	6	108	W 3C =	TA	-140	25	8	201	307	N 4P +3	C3	510	17
10	3	102	W 2P -1	K10	100	38	8	6	108	N 6P +1	TB	1010	71	9	201	307	S 3C =	K7	140	62
11	3	102	N 4C =	KA	420	83	9	6	108	N 3C =	KA	140	62	10	201	306	W 3P =	T3	-140	0
12	3	102	S 3SA +2	T9	660	54	10	6	107	W 4P -4	T3	400	100	11	201	306	O 4P -1	CA	50	50
13	3	101	W 2SA -1	C3	100	50	11	6	107	O 4P X -1	CA	100	58	12	201	306	S 3SA +2	C2	660	54
14	3	101	N 4P -1	CA	-50	27	12	6	107	S 3SA +3	C2	690	88	13	201	304	W 3SA -1	P5	100	50
15	3	101	N 5K -1	PB	-100	0	19	6	105	S 3P -1	C6	-50	25	14	201	304	O 3C +1	PB	-170	4
16	3	108	W 4P =	K7	-620	67	20	6	105	S 3T -1	CB	-100	46	15	201	304	S 5C +1	PA	680	46
17	3	108	O 5K -2	P5	100	38	21	6	105	N 3SA +2	C3	660	62	16	201	303	O 3P =	C6	-140	92
18	3	108	O 3C =	K9	-140	12	22	6	104	W 4C -1	T9	100	88	17	201	303	O 3T =	P4	-110	17
22	3	105	O 4C -1	P9	100	88	23	6	104	S 3P =	CA	140	50	18	201	303	O 3C -1	PK	50	67

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
19	201	302	O 4C -2	PA	200	83	14	204	303 N 2P +2	CA	170	92	3	207	305 W 4C =	CB	-620	29
20	201	302	S 3T -1	C4	-100	46	15	204	303 S 4C +2	PA	680	46	4	207	304 S 3C +3	TD	230	8
21	201	302	S 3SA +3	P10	690	96	16	204	302 W 4P =	T5	-620	67	5	207	304 W 4P -1	TA	50	88
4	202	302	S 3C +3	CD	230	8	17	204	302 S 3P =	K7	140	62	6	207	304 O 1SA -2	C3	200	96
5	202	302	O 2T -2	T10	100	100	18	204	302 O 2C =	PK	-110	38	7	207	302 N 5T -1	KA	-100	50
6	202	302	O 2K +1	CA	-110	21	19	204	301 S 3P =	C9	140	54	8	207	302 N 6P +1	TB	1010	71
7	202	301	N 3T +1	KA	130	75	20	204	301 O 2C +3	KB	-200	0	9	207	302 O 4P -1	CK	100	42
8	202	301	N 6P +1	TB	1010	71	21	204	301 S 3SA +3	T2	690	96	10	207	301 O 4C -1	K4	100	38
9	202	301	N 4C -1	KA	-50	17	22	204	307 O 5K -1	CB	100	88	11	207	301 S 3C +2	KA	200	67
10	202	308	W 4P -3	K10	300	88	23	204	307 S 3P +1	CA	170	79	12	207	301 S 6C -2	CB	-200	0
11	202	308	N 4C =	KA	420	83	24	204	307 O 3T +1	CA	-130	71	13	207	308 O 2K =	C10	-90	15
12	202	308	S 3SA +1	C2	630	25	1	205	308 N 1SA +1	K4	120	100	14	207	308 N 4P =	CA	420	100
13	202	307	O 3SA =	P9	-600	0	2	205	308 N 4C +1	TD	650	92	15	207	308 S 6C =	PA	1430	88
14	202	307	O 3C -1	PB	50	42	3	205	308 W 3C =	T5	-140	54	19	207	307 O 4C -1	TD	100	42
15	202	307	S 5C +1	PA	680	46	4	205	307 S 3C +3	TD	230	8	20	207	307 O 3C +1	T4	-170	17
16	202	305	O 4P +1	T2	-650	21	5	205	307 O 2T -1	T2	50	88	21	207	307 S 3SA +2	K4	660	62
17	202	305	O 3K -2	C3	100	38	6	205	307 O 2K +1	CA	-110	21	22	207	306 W 4C -1	T9	100	88
18	202	305	O 4C -2	PK	100	83	7	205	306 W 4C =	TA	-620	0	23	207	306 S 3P =	CA	140	50
19	202	304	S 3P -1	T5	-50	25	8	205	306 N 6P +1	C4	1010	71	24	207	306 O 2P +2	CA	-170	17
20	202	304	N 3P -1	CK	-100	46	9	205	306 S 3C =	P9	140	62	1	208	307 N 4T -1	CA	-50	62
21	202	304	S 3SA +2	T5	660	62	13	205	305 W 3SA -1	C4	100	50	2	208	307 S 5K =	TA	600	71
22	202	303	O 3K +2	C5	-150	33	14	205	305 N 3P =	CA	140	69	3	208	307 W 4C -1	P2	100	79
23	202	303	S 3P +1	CA	170	79	15	205	305 S 4C +2	PA	680	46	4	208	306 S 3C +4	T4	260	25
24	202	303	S 3C -3	TB	-150	38	16	205	304 W 4P +1	T5	-650	21	5	208	306 O 3SA =	C3	-400	8
1	203	304	N 3SA -2	P3	-100	21	17	205	304 O 4T -2	P7	100	38	6	208	306 O 2K +1	CA	-110	21
2	203	304	N 3SA -2	TD	-200	4	18	205	304 O 2C +1	PK	-140	12	7	208	305 W 4C -1	TA	100	58
3	203	304	W 4C =	KK	-620	29	19	205	303 S 2P +1	TA	140	54	8	208	305 N 6P +1	C9	1010	71
7	203	303	W 3C =	TA	-140	25	20	205	303 N 2P +1	CD	140	100	9	208	305 N 4C -1	KA	-50	17
8	203	303	N 4P +3	K9	510	17	21	205	303 S 3SA +2	K4	660	62	10	208	303 W 3P -3	K10	300	88
9	203	303	S 4C =	K7	420	92	22	205	302 W 4C =	T9	-620	8	11	208	303 N 4C -1	P8	-50	33
10	203	302	W 4P -1	K5	100	38	23	205	302 S 3P =	CA	140	50	12	208	303 S 3SA +3	C2	690	88
11	203	302	W 4P =	K3	-420	12	24	205	302 S 3C -4	P8	-200	0	13	208	302 W 3SA -2	C2	200	88
12	203	302	S 3SA =	C2	600	17	1	206	303 N 3T -2	CA	-100	21	14	208	302 N 3P =	CA	140	69
13	203	301	O 3K -1	C10	100	50	2	206	303 S 3C +2	TA	200	50	15	208	302 S 6C +1	K6	1460	100
14	203	301	N 3P -1	CA	-50	27	3	206	303 W 3C =	KK	-140	54	16	208	301 O 4P +1	C8	-650	21
15	203	301	S 4C =	PA	620	8	4	206	301 S 4C +1	T8	650	38	17	208	301 O 4K -3	T9	150	75
16	203	308	W 3SA -1	T3	100	100	5	206	301 W 4P =	TA	-420	0	18	208	301 S 3K =	CB	110	92
17	203	308	O 4K -4	P4	200	96	6	206	301 O 3SA -2	CA	200	96	22	208	308 O 3K +1	CB	-130	62
18	203	308	O 3C -1	KA	50	67	7	206	308 W 3C +1	TA	-170	8	23	208	308 S 2P +2	CA	170	79
19	203	306	O 3C +2	PB	-200	0	8	206	308 N 4P +3	C4	510	17	24	208	308 S 2C -2	P8	-100	96
20	203	306	O 2C +2	KB	-170	17	9	206	308 S 4C -1	K7	-50	17						
21	203	306	N 5K =	TA	600	12	10	206	307 W 4P -2	T3	200	67						
22	203	305	W 2C +1	T9	-140	46	11	206	307 W 4P =	K3	-420	12						
23	203	305	S 4P -3	CA	-300	0	12	206	307 S 3SA +2	T6	660	54						
24	203	305	O 3P +1	CA	-170	17	16	206	306 W 4P +1	T3	-650	21						
1	204	306	W 2P =	C2	-110	0	17	206	306 W 2SA -2	P3	100	38						
2	204	306	S 3K +1	TA	130	25	18	206	306 O 2C +1	KA	-140	12						
3	204	306	W 4C -1	T4	100	79	19	206	305 S 3P -1	CB	-50	25						
4	204	305	S 4C +2	TD	680	75	20	206	305 S 2P =	C2	110	79						
5	204	305	W 1P +2	C5	-140	29	21	206	305 N 5K =	C3	600	12						
6	204	305	O 2K +1	CA	-110	21	22	206	304 W 4C =	P9	-620	8						
10	204	304	W 1P +1	K10	-110	12	23	206	304 S 2P +3	CA	200	100						
11	204	304	N 4C -1	KA	-50	33	24	206	304 O 3P +1	CA	-170	17						
12	204	304	S 3SA +3	C9	690	88	1	207	305 N 4T -1	CA	-50	62						
13	204	303	O 2SA -3	T10	300	100	2	207	305 S 5K -1	TA	-100	17						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

# **OW-Resultate Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 19.04.2016**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
1	1	101	N 4K -2	T8	100	79	17	1	103	S 3P =	K7	-140	38	6	5	107	N 3C -1	PD	50	17
2	1	101	S 5K =	TA	-600	29	18	1	103	O 3C -1	KA	-50	33	7	1	107	S 3SA =	CA	-600	8
3	1	101	W 2C +2	KK	170	58	19	5	103	O 3C =	C10	140	92	8	1	107	N 6P +1	C4	-1010	29
4	6	101	N 4C +2	TA	-680	25	20	5	103	O 2C +2	KB	170	83	9	1	107	N 4C =	KA	-420	8
5	6	101	W 2P =	TA	110	42	21	5	103	S 3SA +1	C5	-630	75	10	6	107	W 4P -4	T3	-400	0
6	6	101	S 3C -2	KD	100	46	22	2	103	W 4C =	K7	620	92	11	6	107	O 4P X -1	CA	-100	42
7	2	101	S 3SA +1	C4	-630	0	23	2	103	S 4P -1	CA	100	79	12	6	107	S 3SA +3	C2	-690	12
8	2	101	N 4P +3	C10	-510	83	24	2	103	S 3C -3	P8	150	62	13	2	107	O 3SA -1	T3	-100	50
9	2	101	S 4C -1	K2	50	83	1	3	104	N 1SA -1	P3	50	38	14	2	107	O 3C -1	PB	-50	58
10	7	101	W 4P -2	C4	-200	33	2	3	104	N 2C +2	T3	-170	58	15	2	107	S 4C +2	PA	-680	54
11	7	101	N 5C =	K3	-450	0	3	3	104	W 4C +2	TK	680	100	19	7	107	N 3SA =	C5	-400	8
12	7	101	S 3SA +3	C2	-690	12	4	7	104	S 4C +2	T2	-680	25	20	7	107	N 2P =	CK	-110	21
13	3	101	W 2SA -1	C3	-100	50	5	7	104	O 2C =	T10	110	42	21	7	107	S 3SA +2	C5	-660	38
14	3	101	N 4P -1	CA	50	73	6	7	104	O 3K =	CA	110	79	22	4	107	O 3K +1	CB	130	38
15	3	101	N 5K -1	PB	100	100	10	4	104	W 4C -1	PA	-100	62	23	4	107	S 4P -1	CA	100	79
16	8	101	O 4P =	C7	620	33	11	4	104	N 4C =	KA	-420	17	24	4	107	S 2C -2	P8	100	4
17	8	101	W 5T -4	P3	-200	4	12	4	104	N 4C +1	KD	-650	67	1	5	108	O 2P -1	T9	-50	12
18	8	101	S 1SA +2	K3	-150	0	13	1	104	O 2SA =	P10	120	92	2	5	108	S 4C +2	TA	-680	0
19	4	101	S 3P +1	TA	-170	29	14	1	104	O 4C -3	PB	-150	15	3	5	108	W 4C +1	T5	650	88
20	4	101	N 2P =	CK	-110	21	15	1	104	S 4C +2	PA	-680	54	4	1	108	S 4C +2	T2	-680	25
21	4	101	S 4P +1	KB	-650	67	16	5	104	W 4P =	K2	620	33	5	1	108	W 1P +2	TA	140	71
4	2	102	S 4C +1	T4	-650	62	17	5	104	W 2SA =	C6	120	92	6	1	108	S 3C -2	K8	100	46
5	2	102	O 1K +2	T5	110	42	18	5	104	O 2C =	PK	110	62	7	6	108	W 3C =	TA	140	75
6	2	102	O 2K =	CA	90	29	19	2	104	S 4P =	TA	-420	0	8	6	108	N 6P +1	TB	-1010	29
7	7	102	N 2T +2	KA	-130	25	20	2	104	N 3P -1	CK	100	54	9	6	108	N 3C =	KA	-140	38
8	7	102	N 6P +1	C10	-1010	29	21	2	104	N 2K +2	C3	-130	100	10	2	108	W 4P -2	K10	-200	33
9	7	102	N 4C =	KA	-420	8	22	6	104	W 4C -1	T9	-100	12	11	2	108	O 4P +1	CA	450	100
10	3	102	W 2P -1	K10	-100	62	23	6	104	S 3P =	CA	-140	50	12	2	108	S 2SA +2	P9	-180	92
11	3	102	N 4C =	KA	-420	17	24	6	104	O 2P +1	CA	140	46	13	7	108	W 3SA -2	C3	-200	12
12	3	102	S 3SA +2	T9	-660	46	1	7	105	N 2T -1	K4	50	38	14	7	108	N 4P X -1	CA	100	85
13	8	102	W 1SA -1	C3	-100	50	2	7	105	S 5K =	TA	-600	29	15	7	108	S 6C =	PA	-1430	12
14	8	102	O 3C -2	PB	-100	46	3	7	105	O 2P -1	T3	-100	21	16	3	108	W 4P =	K7	620	33
15	8	102	S 4C +2	PA	-680	54	4	4	105	S 4C +2	T4	-680	25	17	3	108	O 5K -2	P5	-100	62
16	4	102	O 4P =	T2	620	33	5	4	105	O 3K =	T2	110	42	18	3	108	O 3C =	K9	140	88
17	4	102	S 3P +1	K7	-170	17	6	4	105	O 3K =	CA	110	79	22	8	108	W 2C +2	T8	170	75
18	4	102	O 2C +1	PK	140	88	7	8	105	W 3C =	TA	140	75	23	8	108	S 3P +1	CA	-170	21
19	1	102	S 3P +1	C6	-170	29	8	8	105	N 6P +1	P8	-1010	29	24	8	108	O 4T =	CA	130	29
20	1	102	S 2P =	K5	-110	21	9	8	105	N 3C =	KA	-140	38	1	201	301	O 2K =	TK	90	58
21	1	102	S 3SA +2	T2	-660	38	13	5	105	W 3SA -1	C3	-100	50	2	201	301	S 3K +2	TA	-150	67
22	5	102	O 3P =	TA	140	54	14	5	105	N 3P =	CA	-140	31	3	201	301	W 4C -2	T5	-200	0
23	5	102	S 4P -1	CA	100	79	15	5	105	S 4C +2	PA	-680	54	4	206	301	S 4C +1	T8	-650	62
24	5	102	O 2P =	CA	110	17	16	2	105	W 4P +1	C9	650	79	5	206	301	W 4P =	TA	420	100
1	6	103	W 2P -1	C2	-50	12	17	2	105	O 3K +1	P4	130	100	6	206	301	O 3SA -2	CA	-200	4
2	6	103	S 5K =	TA	-600	29	18	2	105	S 2SA -1	CB	100	50	7	202	301	N 3T +1	KA	-130	25
3	6	103	W 4C +1	T4	650	88	19	6	105	S 3P -1	C6	50	75	8	202	301	N 6P +1	TB	-1010	29
7	3	103	N 4T =	KA	-130	25	20	6	105	S 3T -1	CB	100	54	9	202	301	N 4C -1	KA	50	83
8	3	103	S 4P +3	KB	-510	83	21	6	105	N 3SA +2	C3	-660	38	10	207	301	O 4C -1	K4	-100	62
9	3	103	S 4C -1	P9	50	83	22	3	105	O 4C -1	P9	-100	12	11	207	301	S 3C +2	KA	-200	33
10	8	103	W 1P +1	K10	110	88	23	3	105	N 4P -1	C4	100	79	12	207	301	S 6C -2	CB	200	100
11	8	103	N 4C -1	TD	50	67	24	3	105	O 2P +1	CA	140	46	13	203	301	O 3K -1	C10	-100	50
12	8	103	S 3SA +2	C2	-660	46	1	8	107	N 2K -2	PA	100	79	14	203	301	N 3P -1	CA	50	73
13	4	103	O 2SA -1	T3	-100	50	2	8	107	S 6C -2	TA	200	96	15	203	301	S 4C =	PA	-620	92
14	4	103	O 3C +1	K2	170	96	3	8	107	W 4C -1	T9	-100	21	16	208	301	O 4P +1	C8	650	79
15	4	103	S 4C +2	PA	-680	54	4	5	107	S 4C +2	T2	-680	25	17	208	301	O 4K -3	T9	-150	25
16	1	103	W 4P +1	T5	650	79	5	5	107	O 2C =	K8	110	42	18	208	301	S 3K =	CB	-110	8

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.



# OW-Resultate Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 19.04.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
19	204	301	S 3P =	C9	-140	46	14	201	304	O 3C +1	PB	170	96	3	208	307	W 4C -1	P2	-100	21
20	204	301	O 2C +3	KB	200	100	15	201	304	S 5C +1	PA	-680	54	4	205	307	S 3C +3	TD	-230	92
21	204	301	S 3SA +3	T2	-690	4	16	205	304	W 4P +1	T5	650	79	5	205	307	O 2T -1	T2	-50	12
4	202	302	S 3C +3	CD	-230	92	17	205	304	O 4T -2	P7	-100	62	6	205	307	O 2K +1	CA	110	79
5	202	302	O 2T -2	T10	-100	0	18	205	304	O 2C +1	PK	140	88	7	201	307	W 2C =	TA	110	58
6	202	302	O 2K +1	CA	110	79	19	202	304	S 3P -1	T5	50	75	8	201	307	N 4P +3	C3	-510	83
7	207	302	N 5T -1	KA	100	50	20	202	304	N 3P -1	CK	100	54	9	201	307	S 3C =	K7	-140	38
8	207	302	N 6P +1	TB	-1010	29	21	202	304	S 3SA +2	T5	-660	38	10	206	307	W 4P -2	T3	-200	33
9	207	302	O 4P -1	CK	-100	58	22	206	304	W 4C =	P9	620	92	11	206	307	W 4P =	K3	420	88
10	203	302	W 4P -1	K5	-100	62	23	206	304	S 2P +3	CA	-200	0	12	206	307	S 3SA +2	T6	-660	46
11	203	302	W 4P =	K3	420	88	24	206	304	O 3P +1	CA	170	83	13	202	307	O 3SA =	P9	600	100
12	203	302	S 3SA =	C2	-600	83	1	207	305	N 4T -1	CA	50	38	14	202	307	O 3C -1	PB	-50	58
13	208	302	W 3SA -2	C2	-200	12	2	207	305	S 5K -1	TA	100	83	15	202	307	S 5C +1	PA	-680	54
14	208	302	N 3P =	CA	-140	31	3	207	305	W 4C =	CB	620	71	19	207	307	O 4C -1	TD	-100	58
15	208	302	S 6C +1	K6	-1460	0	4	204	305	S 4C +2	TD	-680	25	20	207	307	O 3C +1	T4	170	83
16	204	302	W 4P =	T5	620	33	5	204	305	W 1P +2	C5	140	71	21	207	307	S 3SA +2	K4	-660	38
17	204	302	S 3P =	K7	-140	38	6	204	305	O 2K +1	CA	110	79	22	204	307	O 5K -1	CB	-100	12
18	204	302	O 2C =	PK	110	62	7	208	305	W 4C -1	TA	-100	42	23	204	307	S 3P +1	CA	-170	21
19	201	302	O 4C -2	PA	-200	17	8	208	305	N 6P +1	C9	-1010	29	24	204	307	O 3T +1	CA	130	29
20	201	302	S 3T -1	C4	100	54	9	208	305	N 4C -1	KA	50	83	1	205	308	N 1SA +1	K4	-120	0
21	201	302	S 3SA +3	P10	-690	4	13	205	305	W 3SA -1	C4	-100	50	2	205	308	N 4C +1	TD	-650	8
22	205	302	W 4C =	T9	620	92	14	205	305	N 3P =	CA	-140	31	3	205	308	W 3C =	T5	140	46
23	205	302	S 3P =	CA	-140	50	15	205	305	S 4C +2	PA	-680	54	4	201	308	S 4C +2	T4	-680	25
24	205	302	S 3C -4	P8	200	100	16	202	305	O 4P +1	T2	650	79	5	201	308	O 2SA +1	T2	150	83
1	206	303	N 3T -2	CA	100	79	17	202	305	O 3K -2	C3	-100	62	6	201	308	O 2K =	CA	90	29
2	206	303	S 3C +2	TA	-200	50	18	202	305	O 4C -2	PK	-100	17	7	206	308	W 3C +1	TA	170	92
3	206	303	W 3C =	KK	140	46	19	206	305	S 3P -1	CB	50	75	8	206	308	N 4P +3	C4	-510	83
7	203	303	W 3C =	TA	140	75	20	206	305	S 2P =	C2	-110	21	9	206	308	S 4C -1	K7	50	83
8	203	303	N 4P +3	K9	-510	83	21	206	305	N 5K =	C3	-600	88	10	202	308	W 4P -3	K10	-300	12
9	203	303	S 4C =	K7	-420	8	22	203	305	W 2C +1	T9	140	54	11	202	308	N 4C =	KA	-420	17
10	208	303	W 3P -3	K10	-300	12	23	203	305	S 4P -3	CA	300	100	12	202	308	S 3SA +1	C2	-630	75
11	208	303	N 4C -1	P8	50	67	24	203	305	O 3P +1	CA	170	83	13	207	308	O 2K =	C10	90	85
12	208	303	S 3SA +3	C2	-690	12	1	204	306	W 2P =	C2	110	100	14	207	308	N 4P =	CA	-420	0
13	204	303	O 2SA -3	T10	-300	0	2	204	306	S 3K +1	TA	-130	75	15	207	308	S 6C =	PA	-1430	12
14	204	303	N 2P +2	CA	-170	8	3	204	306	W 4C -1	T4	-100	21	16	203	308	W 3SA -1	T3	-100	0
15	204	303	S 4C +2	PA	-680	54	4	208	306	S 3C +4	T4	-260	75	17	203	308	O 4K -4	P4	-200	4
16	201	303	O 3P =	C6	140	8	5	208	306	O 3SA =	C3	400	92	18	203	308	O 3C -1	KA	-50	33
17	201	303	O 3T =	P4	110	83	6	208	306	O 2K +1	CA	110	79	22	208	308	O 3K +1	CB	130	38
18	201	303	O 3C -1	PK	-50	33	7	205	306	W 4C =	TA	620	100	23	208	308	S 2P +2	CA	-170	21
19	205	303	S 2P +1	TA	-140	46	8	205	306	N 6P +1	C4	-1010	29	24	208	308	S 2C -2	P8	100	4
20	205	303	N 2P +1	CD	-140	0	9	205	306	S 3C =	P9	-140	38							
21	205	303	S 3SA +2	K4	-660	38	10	201	306	W 3P =	T3	140	100							
22	202	303	O 3K +2	C5	150	67	11	201	306	O 4P -1	CA	-50	50							
23	202	303	S 3P +1	CA	-170	21	12	201	306	S 3SA +2	C2	-660	46							
24	202	303	S 3C -3	TB	150	62	16	206	306	W 4P +1	T3	650	79							
1	203	304	N 3SA -2	P3	100	79	17	206	306	W 2SA -2	P3	-100	62							
2	203	304	N 3SA -2	TD	200	96	18	206	306	O 2C +1	KA	140	88							
3	203	304	W 4C =	KK	620	71	19	203	306	O 3C +2	PB	200	100							
4	207	304	S 3C +3	TD	-230	92	20	203	306	O 2C +2	KB	170	83							
5	207	304	W 4P -1	TA	-50	12	21	203	306	N 5K =	TA	-600	88							
6	207	304	O 1SA -2	C3	-200	4	22	207	306	W 4C -1	T9	-100	12							
10	204	304	W 1P +1	K10	110	88	23	207	306	S 3P =	CA	-140	50							
11	204	304	N 4C -1	KA	50	67	24	207	306	O 2P +2	CA	170	83							
12	204	304	S 3SA +3	C9	-690	12	1	208	307	N 4T -1	CA	50	38							
13	201	304	W 3SA -1	P5	-100	50	2	208	307	S 5K =	TA	-600	29							

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.