

NS-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 18.02.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	S 3T -1	CA	-50	83	4	3	104 W 3P +1	C9	-170	58	7	5	106 S 4C -1	T6	-100	12
2	1	101	N 3C =	KD	140	92	5	3	103 S3SA-2	P10	-200	4	8	5	106 S1SA+2	PA	150	50
3	1	113	O 2P +1	CD	-140	46	6	3	103 N 4C -1	P4	-50	29	9	5	105 O 5C =	KD	-650	33
4	1	113	W 4P -1	C6	100	92	7	3	102 S 3C -1	T6	-100	12	10	5	105 W3SA+3	C4	-690	4
5	1	112	W5PX-3	T7	500	33	8	3	102 S 4T +1	K5	150	50	11	5	104 S 3C +1	PA	170	96
6	1	112	S 5K =	T5	400	58	9	3	101 W 4C =	P5	-620	83	12	5	104 O3SA+3	T8	-490	17
7	1	111	S 4C +3	T6	710	88	10	3	101 W3SA+3	K5	-690	4	13	5	103 N 3P -1	CA	-100	96
8	1	111	S 4T +1	PA	150	50	11	3	113 S 4C -2	PA	-100	38	14	5	103 W 3SA =	C3	-400	62
9	1	110	O 4C =	P4	-620	83	12	3	113 O3SA-1	P4	50	75	15	5	102 W 3T +4	KK	-190	75
10	1	110	W 6C -3	P7	300	100	13	3	112 O 4C +2	PA	-680	4	16	5	102 O 1SA =	T4	-90	8
11	1	109	O4PX-1	TK	100	62	14	3	112 W3SA+1	T4	-430	25	17	5	101 N 6C +1	P6	1010	25
12	1	109	O 3SA =	P4	-400	54	15	3	111 W 6T +1	KK	-940	4	18	5	101 N3SA-1	K5	-100	54
13	1	108	W 5K +1	PD	-620	25	16	3	111 O 1SA =	T4	-90	8	19	5	113 S2CX-3	T6	-500	17
14	1	108	O 6P -3	T8	150	100	17	3	110 N 6C +1	T8	1010	25	20	5	113 W 4C -2	P5	200	96
15	1	107	W 2T +5	KK	-190	75	18	3	110 N3SA-2	K5	-200	29	21	5	112 W 3K +1	PK	-130	29
16	1	107	O1SA-1	K10	100	58	19	3	109 O 3K +2	T2	-150	46	22	5	112 N 3P -1	CA	-50	0
17	1	106	N 7C =	P2	1510	75	20	3	109 W 6T -1	P9	100	67	23	5	111 W 2P =	C5	-110	12
18	1	106	N 4C =	K2	620	100	21	3	108 S 3P =	KA	140	100	24	5	111 O3SA+1	T4	-430	0
19	1	105	W3SA-1	T5	100	88	22	3	108 N 2P +1	P8	140	21	25	5	110 N3SA-3	K6	-150	0
20	1	105	S 3P =	CA	140	83	23	3	107 W 4P -2	C5	200	88	26	5	110 W 3P -2	KA	200	88
21	1	104	W 4K =	PK	-130	29	24	3	107 O3SA-2	C3	100	100	1	6	111 W 4K =	TK	-130	42
22	1	104	N 2P +1	CA	140	21	25	3	106 N2PX-1	T6	-100	25	2	6	111 O 3P -1	C6	50	46
23	1	103	W 2P -1	C5	100	54	26	3	106 W 2P -1	KA	100	54	3	6	110 O 2P +3	CD	-200	21
24	1	103	W 2P +2	K9	-170	33	1	4	107 W 4C +1	TK	-450	8	4	6	110 W 4P =	C6	-620	17
25	1	102	S 2T -1	P8	-50	62	2	4	107 O2SA-1	C9	50	46	5	6	109 N 4C =	PK	620	50
26	1	102	W 2P =	KA	-110	17	3	4	106 O 3P +1	T3	-170	33	6	6	109 N 5C -2	TK	-100	12
1	2	103	S 4T -1	CA	-50	83	4	4	106 W 4P -1	T9	100	92	7	6	108 N 4P +3	C3	710	88
2	2	103	O 2P =	C6	-110	8	5	4	105 N 4C +1	PK	650	83	8	6	108 S 5T =	PA	400	83
3	2	102	S 4K -2	P6	-100	67	6	4	105 S 5K +1	C2	420	75	9	6	107 W 4C +1	P7	-650	33
4	2	102	W 2P +2	C10	-170	58	7	4	104 S 2C +1	PD	140	33	10	6	107 W3SA-1	P7	100	75
5	2	101	N 4C +1	PK	650	83	8	4	104 S 5T =	C7	400	83	11	6	106 W3SA-1	PD	50	50
6	2	101	N 4C -2	T10	-100	12	9	4	103 O 4C +1	KD	-650	33	12	6	106 O 3SA =	P4	-400	54
7	2	113	S 4C +1	K8	650	62	10	4	103 W 4C =	P5	-620	46	13	6	105 N4PX-2	CA	-500	38
8	2	113	S1SA+2	K5	150	50	11	4	102 S 3C =	PA	140	79	14	6	105 O 4P -1	C4	50	83
9	2	112	O 5C =	T10	-650	33	12	4	102 O3SA-1	T3	50	75	15	6	104 W 5T +2	KK	-440	50
10	2	112	W 4C -1	K6	100	75	13	4	101 O 5C +1	PA	-680	4	16	6	104 O1SA-1	C5	100	58
11	2	111	N 2P -2	T3	-100	38	14	4	101 W 4P =	TD	-420	38	17	6	103 N 6C +1	P9	1010	25
12	2	111	O3SA-2	P4	100	96	15	4	113 W 5T +2	KK	-440	50	18	6	103 S3SA-3	T4	-300	12
13	2	110	N 3P -1	CA	-100	96	16	4	113 O1SA-2	C5	200	100	19	6	102 W3SA-1	T5	100	88
14	2	110	W3SA+2	C9	-460	8	17	4	112 S 7SA =	K4	1520	100	20	6	102 W 4T =	P5	-130	38
15	2	109	W 6T +1	KK	-940	4	18	4	112 S 4P -1	KA	-100	54	21	6	101 S 2P =	CA	110	92
16	2	109	O 1SA =	K8	-90	8	19	4	111 W3SA-1	T7	100	88	22	6	101 N 2P +2	CA	170	62
17	2	108	N 6C +1	CB	1010	25	20	4	111 W3SA-2	P10	200	96	23	6	113 W 2P -1	C5	100	54
18	2	108	N3SA-3	KK	-300	12	21	4	110 W 2K +2	CK	-130	29	24	6	113 W 2P +2	C4	-170	33
19	2	107	O 3K +2	PB	-150	46	22	4	110 N 3P +1	CA	170	62	25	6	112 O 3K -1	CK	100	92
20	2	107			0	50	23	4	109 S 2C -1	PA	-100	33	26	6	112 W 2P =	C2	-110	17
21	2	106	W 3K +1	CK	-130	29	24	4	109 O1SA+3	T5	-180	12	1	7	113 N 3P -2	C7	-100	62
22	2	106	N 2P +2	CA	170	62	25	4	108 S 3T -1	P8	-50	62	2	7	113 O 2P -1	C9	50	46
23	2	105	W4PX-1	C5	200	88	26	4	108 W 2P -2	KA	200	88	3	7	112 O 4P -1	KA	100	83
24	2	105	W 2P +2	T3	-170	33	1	5	109 W 4K -1	PA	50	100	4	7	112 W 4P =	K3	-620	17
25	2	104	S 3T -2	P8	-100	25	2	5	109 N 2C -1	PD	-100	21	5	7	111 N 5C -1	PK	-100	17
26	2	104	W 2P -1	T8	100	54	3	5	108 O 4P -1	KA	100	83	6	7	111 S 4K +2	TD	170	42
1	3	105	W 4K +1	TK	-150	29	4	5	108 O 4P =	CA	-620	17	7	7	110 N 3P +4	C3	260	46
2	3	105	N 3C =	KD	140	92	5	5	107 N 4C =	PK	620	50	8	7	110 S 3T +1	K5	130	25
3	3	104	O 2P =	CD	-110	58	6	5	107 N 4C -1	T7	-50	29	9	7	109 W 4C =	T8	-620	83

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
10	7	109	W 6C -2	K5	200	92	13	9	111 N 4P -2	CA	-200	62	16	11	101 O1SA-1	CB	100	58
11	7	108	S4CX-5	PA	-1100	0	14	9	111 W 3SA =	C3	-400	62	17	11	113 N 6C +1	T9	1010	25
12	7	108	O3SA+3	T3	-490	17	15	9	110 W 5T +2	KK	-440	50	18	11	113 N 2SA =	K5	120	79
13	7	107	O 4C +1	PA	-650	17	16	9	110 O1SA-1	T2	100	58	19	11	112 O 3K +2	T2	-150	46
14	7	107	W3SA+2	T4	-460	8	17	9	109 N 7C =	P2	1510	75	20	11	112 O 4T =	KA	-130	38
15	7	106	O3SA+2	P9	-460	25	18	9	109 N 2SA =	K5	120	79	21	11	111 W 4K -1	PK	50	79
16	7	106	O 1T -1	P8	100	58	19	9	108 W3SA+3	C8	-690	4	22	11	111 N 2P +1	CA	140	21
17	7	105	N 7C =	P3	1510	75	20	9	108 W 3C +1	C8	-170	17	23	11	110 W 2P =	C5	-110	12
18	7	105	N2SA-4	KK	-400	0	21	9	107 S 4P -2	KA	-200	0	24	11	110 W 2P +1	P4	-140	50
19	7	104	W3SA+3	C8	-690	4	22	9	107 N 2P +2	CA	170	62	25	11	109 S 3T -2	P8	-100	25
20	7	104	S 3P -2	T6	-200	8	23	9	106 W2PX-1	C6	200	88	26	11	109 W 2P -1	KA	100	54
21	7	103	W 3K +1	PK	-130	29	24	9	106 O 3K -1	C3	50	83	1	12	110 W 4C =	TD	-420	17
22	7	103	N 3P +1	CA	170	62	25	9	105 N 4P -2	K5	-100	25	2	12	110 N 3C -1	KD	-100	21
23	7	102	W 2P -1	C5	100	54	26	9	105 W 3P -1	T8	100	54	3	12	109 O 3P =	CD	-140	46
24	7	102	O 2SA =	T5	-120	58	1	10	106 W 3K =	TK	-110	50	4	12	109 O2SA+2	T2	-180	33
25	7	101	S 2T =	P8	90	83	2	10	106 N4CX-1	KD	-200	0	5	12	108 S 4T +1	PK	150	25
26	7	101	W 2P -1	T5	100	54	3	10	105 O 2P +3	T8	-200	21	6	12	108 S 5K +1	TD	420	75
1	8	102	N 4T -2	C7	-100	62	4	10	105 W 3P +1	C9	-170	58	7	12	107 N 3P +4	C3	260	46
2	8	102	O 3P -2	C9	100	71	5	10	104 N 4C +1	K3	650	83	8	12	107 N 5T +1	P5	420	100
3	8	101	O 4P -2	KA	200	100	6	10	104 S 6K =	TD	920	96	9	12	106 W 4C +1	K3	-650	33
4	8	101	W 4P -1	K3	100	92	7	10	103 S 4C +1	T6	650	62	10	12	106 O3SA+2	PB	-660	25
5	8	113	N 4C =	PK	620	50	8	10	103 S 5T =	K5	400	83	11	12	105 S4CX-2	PA	-300	12
6	8	113	S 6K =	TD	920	96	9	10	102 O 4C +1	KD	-650	33	12	12	105 O3SA+3	P4	-490	17
7	8	112	N 5P +2	C2	710	88	10	10	102 O3SA+2	C10	-660	25	13	12	104 N 4P -2	CA	-200	62
8	8	112	W5PX-1	KA	100	12	11	10	101 S 2C +2	PA	170	96	14	12	104 W 3SA =	TD	-400	62
9	8	111	O 4C +1	KD	-650	33	12	10	101 O3SA-1	K10	50	75	15	12	103 O 2K -1	CD	50	96
10	8	111	W3SA+2	K5	-660	25	13	10	113 W 4K +2	PD	-170	83	16	12	103 O1SA-1	CB	100	58
11	8	110	S 3C =	PA	140	79	14	10	113 W 3SA =	T4	-400	62	17	12	102 N 7C =	P9	1510	75
12	8	110	O3SA+2	PB	-460	42	15	10	112 O6SA-1	K9	50	96	18	12	102 N 3C =	KK	140	92
13	8	109	N 4P -2	CA	-200	62	16	10	112 O1SA-1	CB	100	58	19	12	101 O 3K +1	PB	-130	67
14	8	109	O 4P =	T8	-420	38	17	10	111 N 6C +1	T8	1010	25	20	12	101 W 5T -1	P10	100	67
15	8	108	O3SA+2	CD	-460	25	18	10	111 N3SA-1	KK	-100	54	21	12	113 W 2K +1	CK	-110	62
16	8	108	O1SA-1	K10	100	58	19	10	110 S 2C -4	K5	-200	25	22	12	113 N 3P +1	CA	170	62
17	8	107	N 7C =	P3	1510	75	20	10	110 W 4T +1	P10	-150	25	23	12	112 W 2P =	C5	-110	12
18	8	107	N3SA-1	K5	-100	54	21	10	109 W 3K =	CK	-110	62	24	12	112 O 2K =	C7	-90	67
19	8	106	S 3C -3	K5	-150	46	22	10	109 O 3T -2	P6	200	96	25	12	111 S 3T -2	P8	-100	25
20	8	106	W 5T =	P10	-600	0	23	10	108 W 2P -1	CA	100	54	26	12	111 W 2P =	C2	-110	17
21	8	105	W 4K -1	PK	50	79	24	10	108 O2SA+2	T4	-180	12	1	13	112 W 3K +2	TK	-150	29
22	8	105	N 2P +1	CA	140	21	25	10	107 S 3T -1	C10	-50	62	2	13	112 N 3P =	TD	140	92
23	8	104	W 2P =	C5	-110	12	26	10	107 W 2P -1	KA	100	54	3	13	111 S4KX-3	P6	-500	8
24	8	104	O 3K -1	C3	50	83	1	11	108 S 4T -1	CA	-50	83	4	13	111 O 3P +1	KB	-170	58
25	8	103	S 2T +1	C5	110	100	2	11	108 O 3P -1	C9	50	46	5	13	110 N 5C =	PK	650	83
26	8	103	N2SA-2	P4	-200	0	3	11	107 O 4P -1	CD	100	83	6	13	110 S 5K +1	TD	420	75
1	9	104	W3CX+2	TK	-730	0	4	11	107 W 4P +1	C10	-650	0	7	13	109 S 4C -1	T6	-100	12
2	9	104	O 4P -2	T3	100	71	5	11	106 S 6T -2	CK	-200	4	8	13	109 W4PX-1	K9	100	12
3	9	103	O 4P =	P9	-620	0	6	11	106 S 5C -3	K9	-150	0	9	13	108 O 4C +1	KD	-650	33
4	9	103	W 3P +1	C9	-170	58	7	11	105 S 4C -1	T6	-100	12	10	13	108 W3SA-1	P7	100	75
5	9	102	N 4C +1	PK	650	83	8	11	105 S 4T +1	K5	150	50	11	13	107 W 2SA =	PD	-120	25
6	9	102	O5TX-1	KD	200	50	9	11	104 O 4C +1	KD	-650	33	12	13	107 O 2C -2	K10	100	96
7	9	101	N 4P +3	C8	710	88	10	11	104 W 4C =	P3	-620	46	13	13	106 N4PX-2	CA	-500	38
8	9	101	S3SA-1	P6	-50	0	11	11	103 O 4P -2	TK	100	62	14	13	106 W3SA+2	C3	-460	8
9	9	113	N 3P -2	KA	-100	100	12	11	103 O3SA+3	P4	-490	17	15	13	105 O3SA+2	CD	-460	25
10	9	113	O 5T =	C10	-600	58	13	11	102 N 4P -2	CA	-200	62	16	13	105 O 1K -1	P8	100	58
11	9	112	S4CX-2	PA	-300	12	14	11	102 W3SA-2	TD	100	92	17	13	104 N 6C +1	K6	1010	25
12	9	112	O3SA+3	P6	-490	17	15	11	101 W 3T +4	KK	-190	75	18	13	104 N3SA-2	K5	-200	29

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

NS-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 18.02.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz
19	13	103	W3SA-1 T7	100	88
20	13	103	W3SA-1 P10	100	67
21	13	102	O 4K = CK	-130	29
22	13	102	O 3T -2 PD	200	96
23	13	101	W 2P -2 C5	200	88
24	13	101	O 3K -1 TA	50	83
25	13	113	N 3P -1 CA	-50	62
26	13	113	S 3SA = P8	600	100

OW-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 18.02.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
1	1	101	S 3T -1	CA	50	17	4	9	103	W 3P +1	C9	170	42	7	11	105	S 4C -1	T6	100	88
2	1	101	N 3C =	KD	-140	8	5	3	103	S3SA-2	P10	200	96	8	11	105	S 4T +1	K5	-150	50
3	8	101	O 4P -2	KA	-200	0	6	3	103	N 4C -1	P4	50	71	9	5	105	O 5C =	KD	650	67
4	8	101	W 4P -1	K3	-100	8	7	10	103	S 4C +1	T6	-650	38	10	5	105	W3SA+3	C4	690	96
5	2	101	N 4C +1	PK	-650	17	8	10	103	S 5T =	K5	-400	17	11	12	105	S4CX-2	PA	300	88
6	2	101	N 4C -2	T10	100	88	9	4	103	O 4C +1	KD	650	67	12	12	105	O3SA+3	P4	490	83
7	9	101	N 4P +3	C8	-710	12	10	4	103	W 4C =	P5	620	54	13	6	105	N4PX-2	CA	500	62
8	9	101	S3SA-1	P6	50	100	11	11	103	O 4P -2	TK	-100	38	14	6	105	O 4P -1	C4	-50	17
9	3	101	W 4C =	P5	620	17	12	11	103	O3SA+3	P4	490	83	15	13	105	O3SA+2	CD	460	75
10	3	101	W3SA+3	K5	690	96	13	5	103	N 3P -1	CA	100	4	16	13	105	O 1K -1	P8	-100	42
11	10	101	S 2C +2	PA	-170	4	14	5	103	W 3SA =	C3	400	38	17	7	105	N 7C =	P3	-1510	25
12	10	101	O3SA-1	K10	-50	25	15	12	103	O 2K -1	CD	-50	4	18	7	105	N2SA-4	KK	400	100
13	4	101	O 5C +1	PA	680	96	16	12	103	O1SA-1	CB	-100	42	19	1	105	W3SA-1	T5	-100	12
14	4	101	W 4P =	TD	420	62	17	6	103	N 6C +1	P9	-1010	75	20	1	105	S 3P =	CA	-140	17
15	11	101	W 3T +4	KK	190	25	18	6	103	S3SA-3	T4	300	88	21	8	105	W 4K -1	PK	-50	21
16	11	101	O1SA-1	CB	-100	42	19	13	103	W3SA-1	T7	-100	12	22	8	105	N 2P +1	CA	-140	79
17	5	101	N 6C +1	P6	-1010	75	20	13	103	W3SA-1	P10	-100	33	23	2	105	W4PX-1	C5	-200	12
18	5	101	N3SA-1	K5	100	46	21	7	103	W 3K +1	PK	130	71	24	2	105	W 2P +2	T3	170	67
19	12	101	O 3K +1	PB	130	33	22	7	103	N 3P +1	CA	-170	38	25	9	105	N 4P -2	K5	100	75
20	12	101	W 5T -1	P10	-100	33	23	1	103	W 2P -1	C5	-100	46	26	9	105	W 3P -1	T8	-100	46
21	6	101	S 2P =	CA	-110	8	24	1	103	W 2P +2	K9	170	67	1	10	106	W 3K =	TK	110	50
22	6	101	N 2P +2	CA	-170	38	25	8	103	S 2T +1	C5	-110	0	2	10	106	N4CX-1	KD	200	100
23	13	101	W 2P -2	C5	-200	12	26	8	103	N2SA-2	P4	200	100	3	4	106	O 3P +1	T3	170	67
24	13	101	O 3K -1	TA	-50	17	1	9	104	W3CX+2	TK	730	100	4	4	106	W 4P -1	T9	-100	8
25	7	101	S 2T =	P8	-90	17	2	9	104	O 4P -2	T3	-100	29	5	11	106	S 6T -2	CK	200	96
26	7	101	W 2P -1	T5	-100	46	3	3	104	O 2P =	CD	110	42	6	11	106	S 5C -3	K9	150	100
1	8	102	N 4T -2	C7	100	38	4	3	104	W 3P +1	C9	170	42	7	5	106	S 4C -1	T6	100	88
2	8	102	O 3P -2	C9	-100	29	5	10	104	N 4C +1	K3	-650	17	8	5	106	S1SA+2	PA	-150	50
3	2	102	S 4K -2	P6	100	33	6	10	104	S 6K =	TD	-920	4	9	12	106	W 4C +1	K3	650	67
4	2	102	W 2P +2	C10	170	42	7	4	104	S 2C +1	PD	-140	67	10	12	106	O3SA+2	PB	660	75
5	9	102	N 4C +1	PK	-650	17	8	4	104	S 5T =	C7	-400	17	11	6	106	W3SA-1	PD	-50	50
6	9	102	O5TX-1	KD	-200	50	9	11	104	O 4C +1	KD	650	67	12	6	106	O 3SA =	P4	400	46
7	3	102	S 3C -1	T6	100	88	10	11	104	W 4C =	P3	620	54	13	13	106	N4PX-2	CA	500	62
8	3	102	S 4T +1	K5	-150	50	11	5	104	S 3C +1	PA	-170	4	14	13	106	W3SA+2	C3	460	92
9	10	102	O 4C +1	KD	650	67	12	5	104	O3SA+3	T8	490	83	15	7	106	O3SA+2	P9	460	75
10	10	102	O3SA+2	C10	660	75	13	12	104	N 4P -2	CA	200	38	16	7	106	O 1T -1	P8	-100	42
11	4	102	S 3C =	PA	-140	21	14	12	104	W 3SA =	TD	400	38	17	1	106	N 7C =	P2	-1510	25
12	4	102	O3SA-1	T3	-50	25	15	6	104	W 5T +2	KK	440	50	18	1	106	N 4C =	K2	-620	0
13	11	102	N 4P -2	CA	200	38	16	6	104	O1SA-1	C5	-100	42	19	8	106	S 3C -3	K5	150	54
14	11	102	W3SA-2	TD	-100	8	17	13	104	N 6C +1	K6	-1010	75	20	8	106	W 5T =	P10	600	100
15	5	102	W 3T +4	KK	190	25	18	13	104	N3SA-2	K5	200	71	21	2	106	W 3K +1	CK	130	71
16	5	102	O 1SA =	T4	90	92	19	7	104	W3SA+3	C8	690	96	22	2	106	N 2P +2	CA	-170	38
17	12	102	N 7C =	P9	-1510	25	20	7	104	S 3P -2	T6	200	92	23	9	106	W2PX-1	C6	-200	12
18	12	102	N 3C =	KK	-140	8	21	1	104	W 4K =	PK	130	71	24	9	106	O 3K -1	C3	-50	17
19	6	102	W3SA-1	T5	-100	12	22	1	104	N 2P +1	CA	-140	79	25	3	106	N2PX-1	T6	100	75
20	6	102	W 4T =	P5	130	62	23	8	104	W 2P =	C5	110	88	26	3	106	W 2P -1	KA	-100	46
21	13	102	O 4K =	CK	130	71	24	8	104	O 3K -1	C3	-50	17	1	4	107	W 4C +1	TK	450	92
22	13	102	O 3T -2	PD	-200	4	25	2	104	S 3T -2	P8	100	75	2	4	107	O2SA-1	C9	-50	54
23	7	102	W 2P -1	C5	-100	46	26	2	104	W 2P -1	T8	-100	46	3	11	107	O 4P -1	CD	-100	17
24	7	102	O 2SA =	T5	120	42	1	3	105	W 4K +1	TK	150	71	4	11	107	W 4P +1	C10	650	100
25	1	102	S 2T -1	P8	50	38	2	3	105	N 3C =	KD	-140	8	5	5	107	N 4C =	PK	-620	50
26	1	102	W 2P =	KA	110	83	3	10	105	O 2P +3	T8	200	79	6	5	107	N 4C -1	T7	50	71
1	2	103	S 4T -1	CA	50	17	4	10	105	W 3P +1	C9	170	42	7	12	107	N 3P +4	C3	-260	54
2	2	103	O 2P =	C6	110	92	5	4	105	N 4C +1	PK	-650	17	8	12	107	N 5T +1	P5	-420	0
3	9	103	O 4P =	P9	620	100	6	4	105	S 5K +1	C2	-420	25	9	6	107	W 4C +1	P7	650	67

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

OW-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 18.02.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
10	6	107	W3SA-1	P7	-100	25	13	8	109	N 4P -2	CA	200	38	16	3	111	O 1SA =	T4	90	92
11	13	107	W 2SA =	PD	120	75	14	8	109	O 4P =	T8	420	62	17	10	111	N 6C +1	T8	-1010	75
12	13	107	O 2C -2	K10	-100	4	15	2	109	W 6T +1	KK	940	96	18	10	111	N3SA-1	KK	100	46
13	7	107	O 4C +1	PA	650	83	16	2	109	O 1SA =	K8	90	92	19	4	111	W3SA-1	T7	-100	12
14	7	107	W3SA+2	T4	460	92	17	9	109	N 7C =	P2	-1510	25	20	4	111	W3SA-2	P10	-200	4
15	1	107	W 2T +5	KK	190	25	18	9	109	N 2SA =	K5	-120	21	21	11	111	W 4K -1	PK	-50	21
16	1	107	O1SA-1	K10	-100	42	19	3	109	O 3K +2	T2	150	54	22	11	111	N 2P +1	CA	-140	79
17	8	107	N 7C =	P3	-1510	25	20	3	109	W 6T -1	P9	-100	33	23	5	111	W 2P =	C5	110	88
18	8	107	N3SA-1	K5	100	46	21	10	109	W 3K =	CK	110	38	24	5	111	O3SA+1	T4	430	100
19	2	107	O 3K +2	PB	150	54	22	10	109	O 3T -2	P6	-200	4	25	12	111	S 3T -2	P8	100	75
20	2	107			0	50	23	4	109	S 2C -1	PA	100	67	26	12	111	W 2P =	C2	110	83
21	9	107	S 4P -2	KA	200	100	24	4	109	O1SA+3	T5	180	88	1	13	112	W 3K +2	TK	150	71
22	9	107	N 2P +2	CA	-170	38	25	11	109	S 3T -2	P8	100	75	2	13	112	N 3P =	TD	-140	8
23	3	107	W 4P -2	C5	-200	12	26	11	109	W 2P -1	KA	-100	46	3	7	112	O 4P -1	KA	-100	17
24	3	107	O3SA-2	C3	-100	0	1	12	110	W 4C =	TD	420	83	4	7	112	W 4P =	K3	620	83
25	10	107	S 3T -1	C10	50	38	2	12	110	N 3C -1	KD	100	79	5	1	112	W5PX-3	T7	-500	67
26	10	107	W 2P -1	KA	-100	46	3	6	110	O 2P +3	CD	200	79	6	1	112	S 5K =	T5	-400	42
1	11	108	S 4T -1	CA	50	17	4	6	110	W 4P =	C6	620	83	7	8	112	N 5P +2	C2	-710	12
2	11	108	O 3P -1	C9	-50	54	5	13	110	N 5C =	PK	-650	17	8	8	112	W5PX-1	KA	-100	88
3	5	108	O 4P -1	KA	-100	17	6	13	110	S 5K +1	TD	-420	25	9	2	112	O 5C =	T10	650	67
4	5	108	O 4P =	CA	620	83	7	7	110	N 3P +4	C3	-260	54	10	2	112	W 4C -1	K6	-100	25
5	12	108	S 4T +1	PK	-150	75	8	7	110	S 3T +1	K5	-130	75	11	9	112	S4CX-2	PA	300	88
6	12	108	S 5K +1	TD	-420	25	9	1	110	O 4C =	P4	620	17	12	9	112	O3SA+3	P6	490	83
7	6	108	N 4P +3	C3	-710	12	10	1	110	W 6C -3	P7	-300	0	13	3	112	O 4C +2	PA	680	96
8	6	108	S 5T =	PA	-400	17	11	8	110	S 3C =	PA	-140	21	14	3	112	W3SA+1	T4	430	75
9	13	108	O 4C +1	KD	650	67	12	8	110	O3SA+2	PB	460	58	15	10	112	O6SA-1	K9	-50	4
10	13	108	W3SA-1	P7	-100	25	13	2	110	N 3P -1	CA	100	4	16	10	112	O1SA-1	CB	-100	42
11	7	108	S4CX-5	PA	1100	100	14	2	110	W3SA+2	C9	460	92	17	4	112	S 7SA =	K4	-1520	0
12	7	108	O3SA+3	T3	490	83	15	9	110	W 5T +2	KK	440	50	18	4	112	S 4P -1	KA	100	46
13	1	108	W 5K +1	PD	620	75	16	9	110	O1SA-1	T2	-100	42	19	11	112	O 3K +2	T2	150	54
14	1	108	O 6P -3	T8	-150	0	17	3	110	N 6C +1	T8	-1010	75	20	11	112	O 4T =	KA	130	62
15	8	108	O3SA+2	CD	460	75	18	3	110	N3SA-2	K5	200	71	21	5	112	W 3K +1	PK	130	71
16	8	108	O1SA-1	K10	-100	42	19	10	110	S 2C -4	K5	200	75	22	5	112	N 3P -1	CA	50	100
17	2	108	N 6C +1	CB	-1010	75	20	10	110	W 4T +1	P10	150	75	23	12	112	W 2P =	C5	110	88
18	2	108	N3SA-3	KK	300	88	21	4	110	W 2K +2	CK	130	71	24	12	112	O 2K =	C7	90	33
19	9	108	W3SA+3	C8	690	96	22	4	110	N 3P +1	CA	-170	38	25	6	112	O 3K -1	CK	-100	8
20	9	108	W 3C +1	C8	170	83	23	11	110	W 2P =	C5	110	88	26	6	112	W 2P =	C2	110	83
21	3	108	S 3P =	KA	-140	0	24	11	110	W 2P +1	P4	140	50	1	7	113	N 3P -2	C7	100	38
22	3	108	N 2P +1	P8	-140	79	25	5	110	N3SA-3	K6	150	100	2	7	113	O 2P -1	C9	-50	54
23	10	108	W 2P -1	CA	-100	46	26	5	110	W 3P -2	KA	-200	12	3	1	113	O 2P +1	CD	140	54
24	10	108	O2SA+2	T4	180	88	1	6	111	W 4K =	TK	130	58	4	1	113	W 4P -1	C6	-100	8
25	4	108	S 3T -1	P8	50	38	2	6	111	O 3P -1	C6	-50	54	5	8	113	N 4C =	PK	-620	50
26	4	108	W 2P -2	KA	-200	12	3	13	111	S4KX-3	P6	500	92	6	8	113	S 6K =	TD	-920	4
1	5	109	W 4K -1	PA	-50	0	4	13	111	O 3P +1	KB	170	42	7	2	113	S 4C +1	K8	-650	38
2	5	109	N 2C -1	PD	100	79	5	7	111	N 5C -1	PK	100	83	8	2	113	S1SA+2	K5	-150	50
3	12	109	O 3P =	CD	140	54	6	7	111	S 4K +2	TD	-170	58	9	9	113	N 3P -2	KA	100	0
4	12	109	O2SA+2	T2	180	67	7	1	111	S 4C +3	T6	-710	12	10	9	113	O 5T =	C10	600	42
5	6	109	N 4C =	PK	-620	50	8	1	111	S 4T +1	PA	-150	50	11	3	113	S 4C -2	PA	100	62
6	6	109	N 5C -2	TK	100	88	9	8	111	O 4C +1	KD	650	67	12	3	113	O3SA-1	P4	-50	25
7	13	109	S 4C -1	T6	100	88	10	8	111	W3SA+2	K5	660	75	13	10	113	W 4K +2	PD	170	17
8	13	109	W4PX-1	K9	-100	88	11	2	111	N 2P -2	T3	100	62	14	10	113	W 3SA =	T4	400	38
9	7	109	W 4C =	T8	620	17	12	2	111	O3SA-2	P4	-100	4	15	4	113	W 5T +2	KK	440	50
10	7	109	W 6C -2	K5	-200	8	13	9	111	N 4P -2	CA	200	38	16	4	113	O1SA-2	C5	-200	0
11	1	109	O4PX-1	TK	-100	38	14	9	111	W 3SA =	C3	400	38	17	11	113	N 6C +1	T9	-1010	75
12	1	109	O 3SA =	P4	400	46	15	3	111	W 6T +1	KK	940	96	18	11	113	N 2SA =	K5	-120	21

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

OW-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 18.02.2016

Bd	NS	OW	ASpKonErgAus	Sco	Prz
19	5	113	S2CX-3 T6	500	83
20	5	113	W 4C -2 P5	-200	4
21	12	113	W 2K +1 CK	110	38
22	12	113	N 3P +1 CA	-170	38
23	6	113	W 2P -1 C5	-100	46
24	6	113	W 2P +2 C4	170	67
25	13	113	N 3P -1 CA	50	38
26	13	113	S 3SA = P8	-600	0