

# Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 01.10.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	11	108	N 2SA +2	C3	180	0	5	7	111 W 3SA +2	P5	-460	50	10	2	112 O 3C +1	P7	-170	18
1	9	104	S 3SA =	P6	400	27	5	6	109 O 3SA +2	CA	-460	50	10	3	101 O 3C =	KA	-140	27
1	6	111	N 3SA =	P3	400	27	5	5	107 W 3SA +2	P10	-460	50	10	11	104 N 4K -1	PA	-100	36
1	5	109	N 3SA =	P2	400	27	5	4	105 W 3SA +2	P9	-460	50	10	4	103 O 3C -1	P2	100	59
1	4	107	S 3SA =	PB	400	27	5	1	112 W 4P -2	P10	100	100	10	13	108 O 3C -1	T5	100	59
1	3	105	S 3SA =	PB	400	27	6	10	104 W 6SA =	P3	-1440	0	10	12	106 O 4C -1	KA	100	59
1	1	101	S 3SA +1	P4	430	77	6	12	108 O 4C +2	TK	-680	18	10	9	113 W 3C -1	C9	100	59
1	13	112	N 3SA +1	C3	430	77	6	7	111 O 4C +2	T8	-680	18	10	1	110 N 2P +2	CA	170	82
1	12	110	N 3SA +1	C3	430	77	6	5	107 O 4C +2	TK	-680	18	10	8	111 O 4C -2	T5	200	95
1	10	106	N 3SA +1	C3	430	77	6	1	112 O 4C +1	TK	-650	41	10	6	107 O 4C -2	P2	200	95
1	7	113	N 3SA +1	C3	430	77	6	8	113 O 4C +1	TK	-650	41	11	11	103 S 5T -2	C7	-100	0
1	2	103	S 3SA +1	PB	430	77	6	13	110 O 4C =	TK	-620	55	11	5	104 S 4T -1	KA	-50	14
2	7	113	S 3SA =	KA	600	5	6	4	105 O 3C =	TK	-140	64	11	1	109 S 4T -1	KA	-50	14
2	2	103	S 3SA =	KD	600	5	6	3	103 W 3SA -1	T4	100	77	11	6	106 W 3K -2	TK	100	45
2	1	101	S 4P =	KD	620	27	6	6	109 O 4P -1	TK	100	77	11	3	113 O 3C -2	TA	100	45
2	11	108	S 4P =	KD	620	27	6	11	106 W 3SA -2	T4	200	91	11	10	101 W 3K -2	TK	100	45
2	5	109	S 4P =	KD	620	27	6	2	101 W 3SA -3	T4	300	100	11	9	112 W 4K -2	CB	100	45
2	12	110	S 4P +1	KD	650	55	7	4	104 W 6C =	KA	-1430	9	11	7	108 O 3C -2	TA	100	45
2	10	106	N 4P +1	KA	650	55	7	1	111 O 6C =	KA	-1430	9	11	8	110 S 2P +1	KA	140	73
2	4	107	S 4P +1	KD	650	55	7	9	101 O 6C =	C4	-1430	9	11	2	111 W 4K -3	CB	150	82
2	13	112	S 4C +2	P8	680	82	7	6	108 O 5C +2	P5	-710	27	11	13	107 O 4C -5	TA	250	91
2	9	104	S 4C +2	P8	680	82	7	2	113 O 4C +2	P10	-680	64	11	12	105 O 4C X -4	TA	800	100
2	3	105	S 4P +2	C3	680	82	7	13	109 O 5C +1	P4	-680	64	12	5	104 N 6SA -1	C7	-100	5
2	6	111	W 5K X -4	C6	800	100	7	12	107 O 4C +2	P10	-680	64	12	11	103 N 6K -1	C5	-100	5
3	5	108	W 3SA +2	K5	-660	0	7	10	103 O 4C +2	P4	-680	64	12	2	111 N 3SA +2	P5	660	27
3	9	103	W 3SA +1	P10	-630	9	7	8	112 O 5C +1	KA	-680	64	12	1	109 N 3SA +2	T3	660	27
3	13	111	W 3SA =	K5	-600	36	7	7	110 O 4C +2	P10	-680	64	12	8	110 N 5SA =	K9	660	27
3	12	109	W 3SA =	K2	-600	36	7	5	106 O 4C +2	P4	-680	64	12	6	106 N 3SA +3	T3	690	68
3	11	107	W 3SA =	K5	-600	36	7	11	105 O 4C =	KA	-620	100	12	13	107 N 3SA +3	T3	690	68
3	8	101	W 3SA =	K4	-600	36	8	10	103 N 5T X -3	PK	-500	0	12	12	105 N 3SA +3	T3	690	68
3	3	104	W 3SA =	K5	-600	36	8	4	104 O 4P =	TK	-420	18	12	10	101 N 3SA +3	T3	690	68
3	1	113	W 3SA -1	T7	100	77	8	13	109 O 4P =	TK	-420	18	12	9	112 N 3SA +3	T3	690	68
3	7	112	W 5T -1	C2	100	77	8	8	112 O 4P =	TK	-420	18	12	7	108 N 3SA +3	T3	690	68
3	6	110	W 3SA -1	K2	100	77	8	12	107 N 5T -3	K8	-150	41	12	3	113 S 6SA =	T2	1440	100
3	4	106	W 3SA -1	K5	100	77	8	6	108 N 6T -3	CD	-150	41	13	13	106 N 4P -1	K6	-100	0
3	10	105	O 3SA -2	K5	200	100	8	11	105 W 3K =	TA	-110	55	13	7	107 N 2P +1	C7	140	9
4	6	110	S 4P -2	C7	-200	0	8	1	111 O 5P -1	TK	50	73	13	12	104 N 2P +2	K6	170	23
4	11	107	O 2C +1	TD	-140	9	8	7	110 O 4P -1	C10	50	73	13	8	109 N 2P +2	K6	170	23
4	13	111	O 2C =	K8	-110	23	8	5	106 O 3P -1	TK	50	73	13	5	103 N 2P +4	K6	230	36
4	3	104	O 2C =	TD	-110	23	8	2	113 W 5K -2	PA	100	91	13	4	101 N 2P +5	K6	260	50
4	1	113	O 3C -1	TD	100	59	8	9	101 W 5K X -2	PA	300	100	13	1	108 N 3P +4	C2	260	50
4	12	109	O 2C -1	TD	100	59	9	6	107 O 4P +1	TA	-650	0	13	6	105 N 4P =	KB	620	73
4	9	103	O 3C -1	TD	100	59	9	5	105 W 3P +2	T3	-200	32	13	3	112 N 4P =	C3	620	73
4	7	112	O 3C -1	P2	100	59	9	3	101 O 3P +2	K2	-200	32	13	10	113 N 4P =	C3	620	73
4	5	108	O 2C -1	TD	100	59	9	12	106 W 3P +2	TK	-200	32	13	2	110 N 4P +1	TA	650	95
4	4	106	O 3C -1	PK	100	59	9	11	104 W 3P +2	TK	-200	32	13	9	111 N 4P +1	TA	650	95
4	10	105	S 2P =	C7	110	91	9	8	111 W 3P +2	TK	-200	32	14	8	109 O 3SA +2	P4	-460	0
4	8	101	S 2P +1	CB	140	100	9	7	109 O 3P +2	TA	-200	32	14	9	111 W 5K +1	P2	-420	9
5	13	110	W 3SA +3	P3	-490	0	9	2	112 W 2P =	K8	-110	64	14	7	107 W 5K =	P2	-400	45
5	3	103	O 3SA +2	T7	-460	50	9	4	103 S 4T -2	CB	-100	73	14	6	105 O 5K =	PA	-400	45
5	2	101	W 3SA +2	P5	-460	50	9	13	108 S 3T -1	PA	-50	86	14	5	103 W 5K =	P2	-400	45
5	12	108	W 3SA +2	P3	-460	50	9	9	113 S 3T -1	PA	-50	86	14	4	101 O 3SA =	TB	-400	45
5	11	106	W 3SA +2	P5	-460	50	9	1	110 S 2T =	CB	90	100	14	3	112 O 5K =	PA	-400	45
5	10	104	W 3SA +2	P10	-460	50	10	5	105 S 5K -3	C6	-300	0	14	1	108 O 5K =	PA	-400	45
5	8	113	W 3SA +2	K10	-460	50	10	7	109 N 3P -2	K4	-200	9	14	12	104 W 5K =	P2	-400	45

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 01.10.2015**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
14	10	113	S 2P X -2	KA	-300	82	19	11	112 N 2SA =	CD	120	32	23	9	106 S 4C +1	TD	650	95
14	13	106	O 3K +3	T6	-170	91	19	3	109 S 3K +1	PA	130	45	24	12	112 S 2C -1	KK	-50	9
14	2	110	O 3K +2	PA	-150	100	19	7	104 W 2C -2	K10	200	59	24	3	107 S 3C -1	K4	-50	9
15	6	104	N 4C -1	T9	-100	0	19	13	103 W 3C -2	K10	200	59	24	2	105 S 3C -1	K4	-50	9
15	7	106	N 3C =	T9	140	9	19	9	108 W 3C -3	K10	300	73	24	13	101 O 4K -1	CD	50	27
15	13	105	N 3C +1	T3	170	18	19	12	101 N 3SA =	CD	400	82	24	10	108 O 4K -2	CD	100	36
15	2	109	N 3C +2	T9	200	36	19	4	111 W 3C X -2	K9	500	91	24	4	109 S 2C =	KK	110	45
15	1	107	N 3C +2	T9	200	36	19	1	105 W 4C X -4	K10	1100	100	24	11	110 S 2C +1	K4	140	64
15	12	103	N 3C +2	T9	200	36	20	2	107 O 3C -1	TA	100	0	24	9	106 S 3C =	K4	140	64
15	11	101	N 4C =	T9	620	55	20	11	112 N 4T +1	CA	150	9	24	8	104 S 3C =	K4	140	64
15	4	113	N 4C +1	P10	650	77	20	7	104 S 3P +1	KB	170	27	24	6	113 S 3C +1	K4	170	86
15	3	111	N 4C +1	T9	650	77	20	5	113 S 3P +1	K3	170	27	24	1	103 S 3C +1	TK	170	86
15	10	112	N 4C +1	T9	650	77	20	12	101 S 2P +2	KB	170	27	24	5	111 S 3C +2	TK	200	100
15	9	110	S 4C +1	TA	650	77	20	9	108 S 2P +3	K6	200	55	25	7	101 W 3SA +2	K3	-660	5
15	8	108	N 4C +2	T9	680	100	20	1	105 S 2P +3	K7	200	55	25	2	104 W 3SA +2	P7	-660	5
16	7	106	W 2C +1	PK	-140	5	20	13	103 S 2P +3	C2	200	55	25	12	111 W 3SA +1	PA	-630	18
16	4	113	W 2C +1	PK	-140	5	20	3	109 S 4P =	K3	620	73	25	4	108 W 3SA =	P6	-600	27
16	1	107	N 4P X -1	CB	-100	18	20	10	110 S 4P +1	K3	650	91	25	11	109 O 4K +2	PA	-170	36
16	8	108	N 4P -1	C3	-50	36	20	8	106 S 4P +1	K3	650	91	25	10	107 N 4P X -1	KA	-100	45
16	13	105	N 5P -1	C3	-50	36	20	4	111 S 4P +1	C2	650	91	25	13	113 N 3P -1	KA	-50	59
16	11	101	N 4P -1	C3	-50	36	21	12	113 S 5K X -4	TA	-1100	0	25	6	112 N 3P -1	KA	-50	59
16	2	109	N 3P =	C3	140	59	21	2	106 N 3C X -3	K10	-800	9	25	9	105 N 3P +1	KA	170	82
16	9	110	S 3P =	C6	140	59	21	10	109 N 3C X -2	K10	-500	36	25	5	110 N 3P +1	KK	170	82
16	12	103	N 3P +1	C3	170	73	21	9	107 S 3K X -2	PA	-500	36	25	3	106 N 3P +1	KA	170	82
16	3	111	N 4P =	CB	420	86	21	8	105 N 4C X -2	K10	-500	36	25	8	103 N 4P X =	KA	590	100
16	10	112	N 4P =	CB	420	86	21	7	103 N 3C X -2	P3	-500	36	26	11	109 W 2SA +2	C10	-180	5
16	6	104	W 5C X -2	PK	500	100	21	3	108 N 3C X -2	K10	-500	36	26	5	110 W 2SA +2	CB	-180	5
17	7	105	O 3K +2	CD	-150	18	21	11	111 N 4C -3	K10	-300	64	26	13	113 W 2SA =	P3	-120	50
17	3	110	O 3K +2	CD	-150	18	21	5	112 N 4C -2	TB	-200	73	26	10	107 W 2SA =	T3	-120	50
17	1	106	O 3K +2	C2	-150	18	21	6	101 O 4P -1	KA	50	82	26	9	105 W 2SA =	CB	-120	50
17	13	104	O 3K +2	CD	-150	18	21	4	110 O 4P -2	KA	100	95	26	8	103 W 2SA =	CB	-120	50
17	10	111	O 4K +1	C2	-150	18	21	1	104 O 4P -2	KA	100	95	26	7	101 W 2SA =	T3	-120	50
17	9	109	O 4K =	C2	-130	59	22	11	111 O 4C +1	K3	-650	14	26	6	112 W 2SA =	T3	-120	50
17	6	103	O 3K +1	C2	-130	59	22	3	108 O 4C +1	T5	-650	14	26	4	108 W 2SA =	T3	-120	50
17	5	101	O 3K +1	C3	-130	59	22	2	106 O 5C =	KA	-650	14	26	2	104 W 2SA =	T3	-120	50
17	11	113	O 3K +1	CD	-130	59	22	1	104 O 5C =	KA	-650	14	26	12	111 W 2K =	CB	-90	91
17	8	107	N 3C -2	KA	-100	82	22	9	107 O 4C =	C5	-620	45	26	3	106 W 2SA -1	T3	100	100
17	2	108	O 3SA -1	C2	50	91	22	4	110 O 4C =	KA	-620	45						
17	4	112	W 4P -3	CA	150	100	22	12	113 O 4C =	KA	-620	45						
18	8	107	W 3P +1	CA	-170	0	22	7	103 O 3C +2	PA	-200	68						
18	1	106	W 3P =	CA	-140	9	22	5	112 O 3C +2	T7	-200	68						
18	2	108	O 3C -1	T10	50	23	22	10	109 O 3C +1	KA	-170	86						
18	10	111	W 4P -1	CA	50	23	22	6	101 O 3C +1	KA	-170	86						
18	3	110	W 4P -2	CA	100	45	22	8	105 S 5K -2	TA	-100	100						
18	13	104	O 4C X -1	KA	100	45	23	13	101 S 4C -1	C4	-100	0						
18	11	113	O 4C -2	T10	100	45	23	10	108 S 3C +1	T3	170	14						
18	7	105	N 4T =	P3	130	68	23	1	103 S 2C +2	P3	170	14						
18	4	112	N 4T =	PK	130	68	23	12	112 S 4C =	TD	620	55						
18	6	103	W 3P -3	CA	150	82	23	8	104 S 4C =	P3	620	55						
18	9	109	W 4P X -2	CA	300	91	23	6	113 S 4C =	KA	620	55						
18	5	101	S 3SA +1	KD	630	100	23	5	111 S 4C =	T3	620	55						
19	10	110	N 3SA -1	P10	-50	5	23	4	109 S 4C =	TD	620	55						
19	5	113	N 2SA -1	C3	-50	5	23	3	107 S 4C =	P2	620	55						
19	2	107	W 1C -1	P3	100	18	23	2	105 S 4C =	P3	620	55						
19	8	106	N 2SA =	C3	120	32	23	11	110 S 4C +1	KA	650	95						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.