

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Wine Drive - 24.09.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	205	309	S 3SA -2	P2	-100	0	3	211	307 O 4P =	CK	-620	22	5	7	111 N 4C =	P2	620	65
1	11	108	S 2SA -1	P2	-50	22	3	210	305 O 4P =	K8	-620	22	5	6	109 N 4C =	P4	620	65
1	9	104	S 2SA -1	P2	-50	22	3	10	105 O 3SA =	C5	-600	41	5	5	107 N 4C =	P4	620	65
1	5	109	S 2SA -1	K7	-50	22	3	4	106 O 3SA =	C6	-600	41	5	203	303 N 4C =	TA	620	65
1	4	107	S 2SA -1	P2	-50	22	3	202	302 W 1SA +1	TD	-120	48	5	201	312 N 4C =	P2	620	65
1	3	105	S 2K -1	C5	-50	22	3	2	102 O 4P -1	K8	100	70	5	210	304 N 4C =	P2	620	65
1	201	301	S 3SA -1	P2	-50	22	3	13	111 O 1SA -1	T6	100	70	5	209	302 N 4C =	TA	620	65
1	209	304	S 2SA -1	P2	-50	22	3	12	109 W 4C -1	TD	100	70	5	207	311 N 4C =	P2	620	65
1	207	313	S 2SA -1	P2	-50	22	3	11	107 W 2C -1	TD	100	70	5	206	309 N 4C =	K3	620	65
1	206	311	S 3SA -1	P2	-50	22	3	5	108 O 4P -1	K8	100	70	5	205	307 N 4C +1	P4	650	100
1	13	112	W 1SA -1	KA	50	48	3	209	303 O 4P -1	K8	100	70	6	1	112 S 5T X -4	C2	-800	0
1	12	110	W 1SA -1	KA	50	48	3	207	312 O 4P -1	K8	100	70	6	11	106 N 3K -4	C9	-200	4
1	213	312	W 1SA -1	P5	50	48	3	206	310 O 4P -1	K8	100	70	6	12	108 N 4K -3	T3	-150	9
1	7	113	W 1SA -2	KA	100	59	3	204	306 O 4P -1	P10	100	70	6	13	110 W 3C =	P7	-140	24
1	6	111	W 1SA -2	P2	100	59	3	1	113 O 4P -2	CK	200	96	6	10	104 W 2C +1	KA	-140	24
1	1	101	S 2SA =	P2	120	74	3	6	110 O 4P -2	K8	200	96	6	203	303 W 2C +1	KA	-140	24
1	10	106	S 1SA +1	C5	120	74	3	208	301 O 4P -2	K8	200	96	6	201	312 W 2C +1	TA	-140	24
1	211	308	S 2SA =	P2	120	74	4	10	105 W 3SA +1	TA	-630	2	6	213	310 W 3C =	TA	-140	24
1	210	306	S 2SA =	P2	120	74	4	201	313 W 3SA +1	CB	-630	2	6	212	308 W 3C =	CB	-140	24
1	204	307	S 2SA =	P2	120	74	4	2	102 N 3T X -2	K6	-500	9	6	3	103 W 2C =	TA	-110	50
1	8	102	S 2SA +1	P2	150	93	4	211	307 W 2SA +3	T8	-210	13	6	9	102 W 2C =	P7	-110	50
1	212	310	S 2SA +1	C5	150	93	4	12	109 N 3T -2	C3	-200	17	6	210	304 W 2C =	P7	-110	50
1	208	302	S 2SA +1	P2	150	93	4	1	113 W 2SA +2	T7	-180	24	6	207	311 W 2C =	P7	-110	50
1	203	305	S 2SA +1	P2	150	93	4	4	106 W 2SA +2	K2	-180	24	6	206	309 W 2C =	CB	-110	50
2	8	102	N 3C X -4	KA	-1100	0	4	210	305 W 2SA +1	CB	-150	30	6	205	307 W 2C =	KA	-110	50
2	211	308	O 3SA +3	PB	-490	4	4	9	103 W 2SA =	C4	-120	43	6	6	109 S 3T -1	KD	-50	65
2	208	302	O 3SA +2	P4	-460	9	4	7	112 W 2SA =	T8	-120	43	6	2	101 W 3C -1	P8	100	83
2	1	101	O 3SA +1	P5	-430	33	4	213	311 W 2SA =	T10	-120	43	6	8	113 O 2K -1	CA	100	83
2	12	110	O 3SA +1	K9	-430	33	4	212	309 W 2SA =	T7	-120	43	6	5	107 W 2C -1	KA	100	83
2	9	104	O 3SA +1	KK	-430	33	4	207	312 W 2SA =	T8	-120	43	6	202	301 W 2C -1	P7	100	83
2	7	113	W 3SA +1	C5	-430	33	4	205	308 W 3K =	CB	-110	57	6	211	306 W 3C -1	CB	100	83
2	3	105	W 3SA +1	T3	-430	33	4	13	111 W 2K =	CB	-90	67	6	209	302 W 2C -1	P7	100	83
2	210	306	W 3SA +1	C8	-430	33	4	11	107 W 2K =	P2	-90	67	6	208	313 W 3C -1	P7	100	83
2	209	304	O 3SA +1	K7	-430	33	4	6	110 W 2K =	CB	-90	67	6	7	111 W 4C -3	TA	300	100
2	207	313	W 3SA +1	T3	-430	33	4	206	310 W 2K =	CB	-90	67	7	212	307 O 4T X =	CA	-710	0
2	205	309	W 3SA +1	CD	-430	33	4	8	101 W 2SA -1	TA	100	85	7	3	102 O 4T +1	KA	-150	4
2	204	307	W 3SA +1	C5	-430	33	4	202	302 W 3K -1	C4	100	85	7	4	104 O 4T =	CA	-130	20
2	4	107	O 3SA =	K7	-400	57	4	209	303 W 3SA -1	T8	100	85	7	11	105 O 4T =	CA	-130	20
2	13	112	N 2P -3	KA	-300	61	4	208	301 W 3K -1	CB	100	85	7	10	103 O 3T +1	CA	-130	20
2	11	108	W 1SA +4	T3	-210	65	4	5	108 W 3SA -2	TA	200	98	7	203	302 O 4T =	CA	-130	20
2	6	111	W 2SA +2	CD	-180	74	4	204	306 O 3C -2	T9	200	98	7	202	313 O 4T =	CA	-130	20
2	5	109	W 2SA +2	C4	-180	74	5	13	110 N 4C -1	P5	-100	4	7	201	311 O 4T =	CA	-130	20
2	201	301	W 2SA +2	TB	-180	74	5	202	301 N 4C -1	P4	-100	4	7	2	113 S 5K -1	T9	-100	37
2	10	106	O 3T +1	KK	-130	89	5	208	313 N 4C -1	K3	-100	4	7	7	110 S 5K -1	T6	-100	37
2	212	310	O 3T +1	C7	-130	89	5	213	310 O 3P -2	C7	100	13	7	8	112 O 5T -1	CA	100	57
2	206	311	O 3T +1	PB	-130	89	5	9	102 N 3C =	K3	140	24	7	204	304 O 5T -1	CA	100	57
2	203	305	O 3T +1	KK	-130	89	5	8	113 N 3C =	P5	140	24	7	213	309 W 3SA -1	K10	100	57
2	213	312	W 3SA -1	TB	50	100	5	212	308 N 3C =	P2	140	24	7	210	303 O 5T -1	CA	100	57
3	8	101	W 4P +1	TD	-650	2	5	211	306 N 3C =	P4	140	24	7	209	301 O 5T -1	CA	100	57
3	205	308	O 4P +1	K8	-650	2	5	3	103 N 4C =	P5	620	65	7	208	312 O 5T -1	CA	100	57
3	9	103	O 4P =	C5	-620	22	5	2	101 N 4C =	P2	620	65	7	206	308 O 5T -1	CK	100	57
3	7	112	O 4P =	CK	-620	22	5	1	112 N 4C =	P2	620	65	7	211	305 S 4K =	T9	130	74
3	201	313	O 4P =	K6	-620	22	5	12	108 N 4C =	K3	620	65	7	13	109 N 4K +2	TA	170	78
3	213	311	O 4P =	C5	-620	22	5	11	106 N 4C =	P5	620	65	7	9	101 O 6T -2	CA	200	85
3	212	309	O 4P =	CK	-620	22	5	10	104 N 4C =	TA	620	65	7	207	310 N 3C +2	TA	200	85

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Wine Drive - 24.09.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
7	12	107	S 5K =	T9	600	91	10	204	303 N 4C -1	PD	-100	17	12	213	307 W 5T -5	P2	250	48
7	1	111	N 4C =	TA	620	98	10	205	305 S 2SA +1	TA	150	22	12	4	102 S 4P =	TD	620	67
7	6	108	N 4C =	TA	620	98	10	4	103 S 3SA =	TA	600	48	12	2	111 S 4P =	CA	620	67
8	210	303	S 6C -2	KD	-100	0	10	2	112 S 3SA =	TA	600	48	12	11	103 S 4P =	TD	620	67
8	12	107	N 5K -1	PD	-50	4	10	13	108 S 3SA =	T8	600	48	12	206	306 S 4P =	TD	620	67
8	10	103	N 3K =	PK	110	11	10	12	106 S 3SA =	TA	600	48	12	202	311 S 4P =	TD	620	67
8	213	309	S 1C +1	T3	110	11	10	10	102 S 3SA =	T4	600	48	12	211	303 S 4P =	TD	620	67
8	202	313	S 2C +1	K4	140	17	10	8	111 S 3SA =	C8	600	48	12	209	312 S 4P =	T5	620	67
8	4	104	S 4C =	TB	420	30	10	211	304 N 3SA =	PD	600	48	12	208	310 S 4P =	TD	620	67
8	3	102	S 4C =	P3	420	30	10	210	302 S 3SA =	TA	600	48	12	5	104 S 4P +1	TD	650	93
8	8	112	S 4C =	TB	420	30	10	209	313 S 3SA =	P6	600	48	12	1	109 S 4P +1	T3	650	93
8	208	312	S 4C =	P3	420	30	10	208	311 S 3SA =	T4	600	48	12	13	107 S 4P +1	T5	650	93
8	206	308	S 4C =	KD	420	30	10	207	309 S 3SA =	T4	600	48	12	204	302 S 4P +1	CA	650	93
8	2	113	N 3SA +1	P10	430	54	10	5	105 N 3SA +1	K2	630	85	13	6	105 W 4P +1	CA	-650	0
8	9	101	N 3SA +1	T4	430	54	10	1	110 S 3SA +1	TA	630	85	13	209	311 W 5T =	CA	-600	4
8	7	110	N 3SA +1	T6	430	54	10	11	104 S 3SA +1	TA	630	85	13	212	304 S 4C -2	PA	-200	9
8	203	302	S 3SA +1	P3	430	54	10	7	109 S 3SA +1	TA	630	85	13	11	102 W 2P +2	T2	-170	17
8	211	305	N 3SA +1	T4	430	54	10	203	301 S 3SA +1	TA	630	85	13	207	307 W 3P +1	CA	-170	17
8	209	301	N 3SA +1	T2	430	54	10	202	312 S 3SA +1	C2	630	85	13	205	303 W 2P +2	CA	-170	17
8	1	111	S 4C +1	T10	450	80	10	9	113 N 4C +1	T8	650	100	13	7	107 W 3T +2	CA	-150	35
8	13	109	S 4C +1	T3	450	80	11	210	301 W 2K +1	CA	-110	0	13	5	103 W 3T +2	CA	-150	35
8	11	105	S 4C +1	TB	450	80	11	209	312 S 1SA -2	K5	-100	4	13	4	101 W 3T +2	CA	-150	35
8	6	108	S 4C +1	P4	450	80	11	3	113 W 2K =	CA	-90	15	13	3	112 W 3T +2	CA	-150	35
8	212	307	S 4C +1	T3	450	80	11	12	105 O 1SA =	P6	-90	15	13	211	302 O 4T +1	CD	-150	35
8	207	310	S 4C +1	TB	450	80	11	206	306 W 2K =	CA	-90	15	13	206	305 W 2P +1	CA	-140	50
8	204	304	N 3SA +2	T9	460	96	11	202	311 W 2K =	CA	-90	15	13	213	306 W 2P +1	CA	-140	50
8	201	311	N 3SA +4	T5	520	100	11	2	111 N 3C -1	K9	-50	33	13	10	113 W 4T =	CA	-130	59
9	205	305	S 3SA -2	C2	-100	0	11	13	107 N 3C -1	K9	-50	33	13	201	308 W 2T +2	CA	-130	59
9	3	101	N 3SA -1	T2	-50	4	11	11	103 N 3C -1	K9	-50	33	13	13	106 S 4C -1	PA	-100	67
9	7	109	Pass		0	11	11	9	112 S 1SA -1	KD	-50	33	13	204	301 S 3C -1	PA	-100	67
9	213	308	Pass		0	11	11	8	110 W 3K -1	CA	50	46	13	202	310 W 3P -1	CA	100	76
9	11	104	N 2K +1	PB	110	17	11	213	307 W 3K -1	CA	50	46	13	210	313 W 4P -1	CA	100	76
9	212	306	N 2SA =	PB	120	24	11	208	310 W 4K -2	CA	100	52	13	2	110 S 3C =	P10	140	89
9	209	313	N 2SA =	PB	120	24	11	6	106 N 2C =	K6	110	65	13	1	108 S 2C +1	PA	140	89
9	2	112	N 1SA +2	T2	150	33	11	4	102 N 2C =	K9	110	65	13	12	104 S 3C =	PA	140	89
9	202	312	S 2SA +1	P5	150	33	11	10	101 N 2C =	K9	110	65	13	203	312 S 3C =	PA	140	89
9	1	110	N 2SA +2	T2	180	46	11	203	313 S 2C =	K3	110	65	13	9	111 O 3SA -2	CD	200	100
9	13	108	N 1SA +3	C5	180	46	11	212	305 N 2C =	K9	110	65	14	12	104 S 3SA -3	K4	-150	2
9	201	310	S 2SA +2	CA	180	46	11	5	104 N 3C =	K9	140	89	14	213	306 S 3SA -3	K4	-150	2
9	207	309	N 2SA +2	C3	180	46	11	1	109 S 2C +1	KD	140	89	14	9	111 N 6P -2	TB	-100	13
9	4	103	O 1C -2	KK	200	57	11	205	304 N 3C =	K9	140	89	14	207	307 S 3SA -2	K4	-100	13
9	203	301	S 1SA +4	P5	210	65	11	204	302 N 3C =	TA	140	89	14	201	308 S 4C -2	T5	-100	13
9	210	302	S 1SA +4	P7	210	65	11	201	309 N 2C +1	K5	140	89	14	204	301 S 4C -1	K5	-50	26
9	208	311	N 2SA +3	C3	210	65	11	211	303 N 2C +1	K7	140	89	14	202	310 S 2SA -1	KD	-50	26
9	8	111	N 3SA =	T2	400	74	12	12	105 S 4P -1	TD	-100	2	14	211	302 S 3SA -1	T10	-50	26
9	12	106	N 3SA +1	T2	430	85	12	8	110 S 4P -1	P7	-100	2	14	4	101 N 2P =	T2	110	35
9	10	102	S 3SA +1	P5	430	85	12	3	113 S 2P +2	TD	170	17	14	3	112 N 2P +1	K9	140	39
9	9	113	N 3SA +1	T2	430	85	12	10	101 S 3P +1	T3	170	17	14	210	313 N 2P +2	T2	170	43
9	211	304	S 3SA +1	P5	430	85	12	9	112 S 2P +2	TD	170	17	14	10	113 S 2SA +2	K4	180	48
9	5	105	S 3SA +2	P5	460	98	12	205	304 S 2P +2	TD	170	17	14	6	105 N 3P +2	K5	200	52
9	204	303	N 3SA +2	T2	460	98	12	201	309 S 2P +2	T4	170	17	14	13	106 S 2SA +3	T10	210	61
10	3	101	N 4C -2	T8	-200	7	12	203	313 S 3P +2	TD	200	35	14	212	304 S 2SA +3	K4	210	61
10	201	310	S 3SA -2	T5	-200	7	12	212	305 S 3P +2	T5	200	35	14	209	311 N 2SA +3	K4	210	61
10	213	308	N 4C -2	PD	-200	7	12	210	301 S 2P +3	T3	200	35	14	11	102 N 3SA =	T4	400	70
10	212	306	S 4P -2	TA	-200	7	12	6	106 S 2P +4	T3	230	43	14	7	107 S 4C =	T10	420	85

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
14	5	103	N 4P =	K5	420	85	17	213	304 O 4C =	K9	-420	2	19	203	309 N 2C +1	T9	140	33
14	2	110	N 4P =	T3	420	85	17	7	105 N 5K -2	CK	-100	17	19	3	109 N 2C +2	K6	170	39
14	1	108	N 4P =	K3	420	85	17	5	101 N 5K X -1	CK	-100	17	19	9	108 N 2C +3	P4	200	46
14	206	305	N 4P =	K9	420	85	17	12	102 N 5K -2	CK	-100	17	19	1	105 N 2C +3	P5	200	46
14	205	303	N 4P =	T2	420	85	17	207	305 N 3SA -2	CK	-100	17	19	201	305 N 3SA =	K5	400	52
14	203	312	S 3SA +1	K4	430	100	17	204	312 N 3SA -2	CK	-100	17	19	10	110 S 4C =	T2	420	61
15	205	302	S 4SA -2	K9	-200	0	17	3	110 N 4K -1	CK	-50	43	19	12	101 N 4C =	K6	420	61
15	4	113	S 3SA -1	K4	-100	9	17	208	307 N 3SA -1	CK	-50	43	19	202	307 N 4C =	K2	420	61
15	12	103	S 3SA -1	K9	-100	9	17	203	310 N 4K -1	CK	-50	43	19	207	304 N 3SA +1	P4	430	70
15	204	313	S 6P -1	K7	-100	9	17	202	308 N 4K -1	CK	-50	43	19	6	102 N 4C +1	C2	450	87
15	213	305	S 2P +3	K7	200	17	17	201	306 N 4K -1	CK	-50	43	19	5	113 N 4C +1	T9	450	87
15	7	106	N 4P =	KK	620	28	17	212	302 N 5K -1	P4	-50	43	19	13	103 S 4C +1	C2	450	87
15	3	111	S 4P =	K9	620	28	17	211	313 N 4K -1	CK	-50	43	19	210	310 N 4C +1	P2	450	87
15	203	311	N 4P =	KK	620	28	17	209	309 O 4P -2	KA	100	61	19	208	306 S 4C +1	P10	450	87
15	202	309	S 4P =	K9	620	28	17	9	109 N 2K +1	CB	110	70	19	204	311 N 4C +1	K4	450	87
15	8	108	S 4P +1	C3	650	59	17	6	103 N 3K =	CK	110	70	19	212	301 S 4C +1	P9	450	87
15	5	102	S 4P +1	K9	650	59	17	13	104 N 2K +1	TA	110	70	20	2	107 O 4P =	KK	-620	2
15	2	109	S 4P +1	C3	650	59	17	8	107 N 3K +1	P4	130	87	20	1	105 O 4P =	KK	-620	2
15	1	107	S 4P +1	K7	650	59	17	2	108 N 2K +2	CK	130	87	20	209	308 S 3K -2	PA	-200	9
15	13	105	S 4P +1	K9	650	59	17	1	106 N 4K =	CK	130	87	20	207	304 W 2SA +2	K5	-180	15
15	11	101	S 4P +1	K3	650	59	17	11	113 N 3K +1	CK	130	87	20	202	307 W 2SA +2	C6	-180	15
15	10	112	S 4P +1	K9	650	59	17	206	303 N 4K =	CK	130	87	20	206	302 O 3P +1	KK	-170	22
15	208	308	S 4P +1	C3	650	59	17	205	301 N 5K X =	TA	550	100	20	8	106 O 2P +1	C10	-140	28
15	211	301	S 4P +1	K2	650	59	18	7	105 O 2C =	K6	-110	0	20	203	309 O 1P +2	KK	-140	28
15	210	312	S 4P +1	K9	650	59	18	9	109 S 2P -1	C4	-100	7	20	9	108 W 1SA =	K5	-90	41
15	207	306	S 4P +2	K9	680	89	18	3	110 N 1SA -1	K5	-100	7	20	208	306 W 1K +1	C6	-90	41
15	206	304	S 4P +2	K9	680	89	18	12	102 W 1SA =	PK	-90	15	20	205	313 W 1SA =	K5	-90	41
15	201	307	N 4P +2	KK	680	89	18	211	313 W 1SA =	C9	-90	15	20	212	301 W 1SA =	T6	-90	41
15	212	303	N 4P +2	KK	680	89	18	4	112 O 1C =	KK	-80	22	20	4	111 W 1C =	K5	-80	52
15	6	104	S 4P +3	TK	710	100	18	202	308 N 1SA =	K5	90	26	20	7	104 W 1T =	K5	-70	57
16	211	301	O 4C =	PA	-620	0	18	209	309 W 2C -2	K9	100	37	20	10	110 W 2SA -1	K3	100	70
16	5	102	O 3T +2	PA	-150	7	18	204	312 W 1SA -2	CD	100	37	20	5	113 O 4P -1	KK	100	70
16	13	105	O 4T +1	PA	-150	7	18	201	306 W 1SA -2	CD	100	37	20	3	109 W 1SA -1	T7	100	70
16	4	113	O 4T =	PA	-130	15	18	213	304 O 1SA -2	K3	100	37	20	12	101 W 2SA -1	T6	100	70
16	202	309	W 4T =	PK	-130	15	18	207	305 S 2P =	T5	110	48	20	201	305 W 2SA -1	T5	100	70
16	3	111	N 4P -1	TA	-50	26	18	6	103 N 1SA +1	K5	120	54	20	13	103 W 2C -2	K5	200	89
16	208	308	N 4P -1	TA	-50	26	18	203	310 S 1SA +1	T9	120	54	20	210	310 W 2SA -2	T8	200	89
16	207	306	N 3P -1	TK	-50	26	18	8	107 N 2SA +1	K5	150	74	20	204	311 W 2C -2	K5	200	89
16	10	112	N 2P =	TA	110	37	18	2	108 N 1SA +2	K5	150	74	20	213	303 O 4P -2	KB	200	89
16	205	302	N 2P =	TA	110	37	18	1	106 N 1SA +2	C2	150	74	20	6	102 W 2SA -3	T6	300	100
16	6	104	N 3P =	KA	140	59	18	13	104 W 3C -3	K9	150	74	21	11	111 N 1SA -2	T3	-200	4
16	12	103	N 3P =	TA	140	59	18	206	303 N 2SA +1	C2	150	74	21	10	109 N 2K -2	P2	-200	4
16	11	101	N 3P =	TA	140	59	18	205	301 N 1SA +2	K5	150	74	21	2	106 N 2K -2	P2	-200	4
16	206	304	N 3P =	CA	140	59	18	212	302 N 1SA +2	K6	150	74	21	13	102 O 2C +1	KA	-140	13
16	203	311	N 3P =	TA	140	59	18	11	113 N 1SA +3	K5	180	91	21	8	105 O 3T =	KA	-110	26
16	213	305	N 3P =	TA	140	59	18	5	101 O 1SA -4	P6	200	98	21	6	101 O 3T =	KA	-110	26
16	212	303	N 3P =	TA	140	59	18	208	307 O 2C -4	KK	200	98	21	209	307 O 2T +1	KA	-110	26
16	210	312	N 3P =	TA	140	59	19	8	106 S 4C -2	TA	-100	0	21	205	312 O 2C =	KA	-110	26
16	2	109	N 3P +1	TA	170	78	19	7	104 N 4P -1	P4	-50	11	21	202	306 O 3T =	KA	-110	26
16	7	106	W 4K -3	T2	300	83	19	4	111 N 4C -1	K2	-50	11	21	7	103 N 2K -1	T5	-100	46
16	8	108	N 4P =	CA	420	91	19	2	107 S 4C -1	P9	-50	11	21	5	112 N 2K -1	P8	-100	46
16	204	313	N 4P =	TA	420	91	19	209	308 N 4C -1	T7	-50	11	21	203	308 N 3K -1	P8	-100	46
16	201	307	N 4P =	TA	420	91	19	205	313 N 2T +1	K2	110	24	21	201	304 N 2K -1	P5	-100	46
16	1	107	N 4P X =	TA	590	100	19	213	303 N 2T +1	C2	110	24	21	206	301 O 3T -1	P6	50	59
17	4	112	O 4P =	KA	-420	2	19	206	302 N 3C =	K2	140	33	21	213	302 O 2C -1	P9	50	59

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Donnerstag - Wine Drive - 24.09.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
21	9	107	N 2K =	P8	90	67	23	208	304 S 2P =	CA	110	93	26	206	312 O 4C =	K4	-620	17
21	210	309	N 2K =	P8	90	67	23	203	307 N 2P =	C10	110	93	26	204	308 O 4C =	T5	-620	17
21	204	310	O 4T X -1	P6	100	74	24	206	313 W 4C =	KA	-420	0	26	202	304 O 3SA =	P3	-600	30
21	4	110	N 2K +1	P8	110	85	24	202	305 W 2C +2	KA	-170	4	26	205	310 O 3C +2	T9	-200	35
21	1	104	N 2K +1	TA	110	85	24	211	310 O 4T +1	K4	-150	9	26	5	110 O 3C +1	P3	-170	48
21	208	305	N 2K +1	TA	110	85	24	10	108 W 3C =	KA	-140	20	26	211	309 O 2C +2	K6	-170	48
21	207	303	N 2K +1	P8	110	85	24	9	106 W 2C +1	T8	-140	20	26	210	307 O 3C +1	C9	-170	48
21	211	311	S 2SA =	T3	120	96	24	3	107 W 3C =	KA	-140	20	26	209	305 O 3C +1	P3	-170	48
21	3	108	N 2K +2	P8	130	100	24	2	105 W 3C =	T8	-140	20	26	208	303 W 2C +2	K2	-170	48
22	211	311	S 3C -3	KD	-150	2	24	7	102 O 4T =	K6	-130	41	26	12	111 O 2SA +1	P3	-150	61
22	207	303	S 4K -3	PB	-150	2	24	212	312 O 4T =	CB	-130	41	26	207	301 O 3C =	T9	-140	65
22	10	109	W 2P =	K6	-110	9	24	209	306 O 3T +1	KB	-130	41	26	11	109 O 2T +2	P9	-130	70
22	210	309	S 4K X -1	PB	-100	17	24	207	302 O 4T =	KB	-130	41	26	213	313 Pass		0	74
22	206	301	N 2SA -2	KA	-100	17	24	204	309 O 4T =	KB	-130	41	26	13	113 O 4C -1	P9	100	87
22	202	306	S 4K -2	PB	-100	17	24	203	307 O 4T =	KB	-130	41	26	9	105 O 4C -1	K4	100	87
22	8	105	S 4K -1	PB	-50	39	24	4	109 N 4K -2	TK	-100	59	26	7	101 O 4C -1	P3	100	87
22	5	112	N 3K -1	PA	-50	39	24	210	308 N 4K -2	TK	-100	59	26	3	106 O 4C -1	P3	100	87
22	3	108	S 3K -1	T2	-50	39	24	205	311 O 1SA =	K10	-90	65	26	203	306 O 4C -1	K4	100	87
22	13	102	S 3K -1	PB	-50	39	24	201	303 N 4K -1	CA	-50	70	26	10	107 O 2SA -2	P3	200	100
22	209	307	S 3K -1	PB	-50	39	24	12	112 O 4T -1	KB	50	78						
22	204	310	S 4K -1	P6	-50	39	24	11	110 O 4T -1	KB	50	78						
22	201	304	S 3K -1	PB	-50	39	24	6	113 O 5T -1	KB	50	78						
22	4	110	W 3P -1	KB	100	61	24	8	104 N 2K =	TK	90	87						
22	2	106	W 4P -1	KB	100	61	24	5	111 N 3K =	C7	110	96						
22	1	104	W 3P -1	K2	100	61	24	1	103 N 3K =	TK	110	96						
22	11	111	S 3K =	PB	110	72	24	208	304 N 3K =	TK	110	96						
22	7	103	S 3K =	PB	110	72	25	5	110 O 5SA =	C6	-660	2						
22	6	101	S 4K =	PB	130	83	25	211	309 O 3SA +2	C6	-660	2						
22	208	305	S 4K =	TD	130	83	25	9	105 O 3SA +1	TB	-630	24						
22	203	308	S 3K +1	TD	130	83	25	8	103 W 3SA +1C10	-630	24							
22	205	312	W 3P -2	KB	200	93	25	7	101 W 3SA +1C10	-630	24							
22	213	302	W 3P -2	K6	200	93	25	6	112 W 3SA +1C10	-630	24							
22	9	107	W 3P -3	K2	300	100	25	2	104 O 3SA +1	T4	-630	24						
23	9	106	S 3SA -2	CA	-200	2	25	210	307 W 3SA +1C10	-630	24							
23	209	306	N 3P -2	C10	-200	2	25	207	301 W 3SA +1C10	-630	24							
23	11	110	W 3C +1	PK	-170	9	25	206	312 O 3SA +1	P10	-630	24						
23	4	109	W 3C =	P3	-140	15	25	204	308 W 4P =	C10	-620	43						
23	2	105	W 3C =	P3	-140	15	25	205	310 O 5K =	CA	-600	52						
23	1	103	W 2C =	K9	-110	28	25	203	306 W 3SA =	C10	-600	52						
23	210	308	W 2C =	TD	-110	28	25	202	304 O 3SA =	C6	-600	52						
23	207	302	W 2C =	TD	-110	28	25	13	113 W 2P +1	C10	-140	63						
23	206	313	W 2C =	TD	-110	28	25	3	106 W 2P +1	C10	-140	63						
23	12	112	S 2P -1	CA	-100	43	25	11	109 O 4K =	CA	-130	70						
23	205	311	N 3P -1	C10	-100	43	25	209	305 O 3K =	P10	-110	74						
23	204	309	N 2P -1	C10	-100	43	25	213	313 Pass		0	78						
23	7	102	W 3C -1	TD	100	67	25	12	111 O 5K -1	CA	100	89						
23	6	113	W 3C -1	P3	100	67	25	10	107 O 3SA -1	C6	100	89						
23	5	111	W 3C -1	TD	100	67	25	4	108 W 4P -1	C10	100	89						
23	3	107	W 3C -1	PK	100	67	25	212	311 W 4P -1	C10	100	89						
23	212	312	W 3C -1	P3	100	67	25	208	303 O 5K -2	P10	200	100						
23	211	310	W 3C -1	K9	100	67	26	4	108 O 4C X =	P9	-790	0						
23	202	305	W 4C -1	PK	100	67	26	8	103 O 3SA +2	K4	-660	4						
23	201	303	W 3C -1	TD	100	67	26	6	112 O 4C =	C3	-620	17						
23	10	108	N 2P =	C10	110	93	26	2	104 O 4C =	K4	-620	17						
23	8	104	S 2P =	CA	110	93	26	212	311 O 4C =	T6	-620	17						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.