

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 16.06.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	N 3SA -2	KD	-100	0	6	7	110 N 3SA -2	K9	-100	0	11	6	106 N 4P +1	C8	450	45
1	14	113	N 3SA -1	P8	-50	30	6	12	107 N 3SA -1	K9	-50	10	11	5	104 N 4P +1	C8	450	45
1	10	105	N 3SA -1	P7	-50	30	6	2	101 N 2SA +2	C9	180	25	11	4	102 N 4P +1	T4	450	45
1	8	114	N 2SA -1	K3	-50	30	6	14	111 N 1SA +3	P4	180	25	11	3	114 N 4P +1	T4	450	45
1	6	110	N 1SA -1	K3	-50	30	6	3	103 N 3SA =	K3	400	60	11	2	112 N 4P +1	T4	450	45
1	5	108	N 3SA -1	P4	-50	30	6	13	109 N 3SA =	K9	400	60	11	1	110 N 4P +1	TB	450	45
1	11	107	N 2SA =	P7	120	70	6	10	102 N 5T =	KA	400	60	11	14	108 N 4P +1	TB	450	45
1	9	103	N 2SA =	P4	120	70	6	9	114 N 3SA =	K9	400	60	11	13	105 N 4P +1	TB	450	45
1	7	112	N 2SA =	P7	120	70	6	8	112 N 3SA =	K9	400	60	11	11	101 N 4P +1	C8	450	45
1	13	111	W 3C -3	KA	150	90	6	1	113 N 3SA +2	KA	460	95	11	10	113 N 4P +1	K2	450	45
1	12	109	N 3SA =	P7	400	100	6	11	105 N 3SA +2	K3	460	95	11	12	103 N 4P +2	TB	480	100
2	1	101	S 3SA -2	P8	-200	10	7	3	102 S 1SA =	P7	90	5	12	2	112 S 4T X -3	KK	-800	0
2	12	109	S 3SA -2	P3	-200	10	7	2	114 S 1SA =	T3	90	5	12	3	114 W 4K =	T10	-130	15
2	9	103	N 4C -2	PA	-200	10	7	1	112 S 2SA =	CB	120	25	12	10	113 W 4K =	T10	-130	15
2	14	113	S 5K -1	P5	-100	50	7	14	110 S 1SA +1	P7	120	25	12	14	108 W 5K -1	T10	50	35
2	13	111	N 4C -1	PA	-100	50	7	8	111 S 1C +2	T4	140	40	12	12	103 W 4K -1	P6	50	35
2	7	112	N 4C -1	PA	-100	50	7	9	113 S 1SA +2	PA	150	50	12	5	104 W 5K -2	P6	100	50
2	6	110	S 5K -1	P6	-100	50	7	4	104 S 1C +3	K3	170	70	12	13	105 N 3P =	K8	140	60
2	5	108	N 4C -1	PA	-100	50	7	13	108 N 3C +1	P5	170	70	12	1	110 N 4P =	CD	620	70
2	11	107	S 3K +1	P4	130	80	7	12	106 S 1C +3	P7	170	70	12	6	106 N 4P +1	TA	650	85
2	8	114	N 3C =	PA	140	90	7	10	101 S 1SA +3	P7	180	90	12	4	102 N 4P +1	TA	650	85
2	10	105	N 4C =	PA	620	100	7	11	103 N 4C =	P10	620	100	12	11	101 N 4P X =	CD	790	100
3	1	114	O 3C X +1	KK	-930	0	8	4	104 N 4C -2	P3	-100	10	13	4	101 N 3K +1	P2	130	5
3	14	112	N 5T -3	CA	-150	10	8	13	108 N 4C -2	PA	-100	10	13	2	111 N 2K +2	P3	130	5
3	11	106	N 4T -2	CA	-100	30	8	12	106 N 4C -2	KA	-100	10	13	3	113 S 3C +1	PA	170	20
3	8	113	N 5T -2	CA	-100	30	8	10	101 N 3C -1	K2	-50	30	13	14	106 S 3C +3	K3	230	30
3	7	111	N 4T -2	CA	-100	30	8	2	114 N 2C =	KA	110	55	13	6	105 N 4C =	P3	620	65
3	2	102	N 3T -1	CA	-50	70	8	1	112 N 2C =	KA	110	55	13	5	103 S 4C =	T7	620	65
3	12	108	N 3T -1	CA	-50	70	8	14	110 N 2C =	T3	110	55	13	1	109 S 4C =	PA	620	65
3	10	104	N 3T -1	CA	-50	70	8	9	113 N 2C =	PA	110	55	13	13	104 S 4C =	T2	620	65
3	9	101	N 3T -1	CA	-50	70	8	3	102 N 2C +1	T2	140	90	13	12	102 S 4C =	PA	620	65
3	6	109	N 3T -1	CA	-50	70	8	11	103 N 2C +1	T10	140	90	13	11	114 S 4C =	CB	620	65
3	13	110	N 2T =	CA	90	100	8	8	111 N 3C =	KA	140	90	13	7	107 S 4C +2	T7	680	100
4	8	113	N 2C -3	P4	-300	0	9	11	102 W 5K X +2	PB	-1150	0	14	2	111 O 3SA +2	T9	-460	0
4	1	114	N 2C -2	P3	-200	10	9	1	111 W 3SA +4	PB	-720	15	14	5	103 O 3SA +1	T2	-430	10
4	14	112	N 2P -1	P4	-100	20	9	14	109 W 3SA +4	PB	-720	15	14	7	107 W 4C =	K5	-420	35
4	13	110	O 1SA =	K3	-90	30	9	4	103 O 5T =	CA	-600	40	14	4	101 W 4C =	T3	-420	35
4	2	102	W 3T -1	K9	100	45	9	2	113 O 5T =	CA	-600	40	14	14	106 W 4C =	K2	-420	35
4	7	111	O 3SA -1	C10	100	45	9	9	112 O 5T =	CA	-600	40	14	11	114 W 4C =	PD	-420	35
4	12	108	W 3P -2	K8	200	60	9	10	114 N 4P X -2	TA	-300	60	14	3	113 W 3C =	K5	-140	60
4	11	106	W 3K -3	C10	300	80	9	3	101 O 4T +1	CA	-150	70	14	13	104 O 4K =	T4	-130	70
4	10	104	O 3SA -3	K2	300	80	9	12	104 N 4P -1	TA	-50	80	14	6	105 W 4C -1	K5	50	80
4	9	101	W 4P -3	CA	300	80	9	13	107 O 6T -1	CA	100	90	14	1	109 W 4C -2	K5	100	95
4	6	109	O 3SA -4	C4	400	100	9	5	105 W 4P -5	C4	500	100	14	12	102 W 4C -2	K5	100	95
5	9	114	N 5K X -3	C5	-800	0	10	12	104 S 4K -1	PK	-100	10	15	12	101 O 3C =	K6	-140	0
5	11	105	N 3K -3	C6	-300	15	10	10	114 S 4K -1	PK	-100	10	15	1	107 O 2C =	T5	-110	10
5	7	110	S 3SA -3	P3	-300	15	10	9	112 S 4K -1	PK	-100	10	15	3	112 N 3K -1	C2	-100	20
5	3	103	N 3SA -2	C6	-200	35	10	3	101 O 3P -1	C10	100	40	15	7	106 O 2C -1	K6	50	60
5	12	107	N 3SA -2	C6	-200	35	10	2	113 O 3P -1	KD	100	40	15	6	104 O 2C -1	P10	50	60
5	2	101	S 2SA -1	CA	-100	55	10	14	109 O 3P -1	KD	100	40	15	5	102 O 2C -1	P10	50	60
5	1	113	N 4K -1	C6	-100	55	10	13	107 S 3K =	PK	110	60	15	4	114 O 3C -1	T5	50	60
5	14	111	N 3K =	C6	110	75	10	5	105 N 2SA +1	P5	150	70	15	2	110 O 2C -1	P10	50	60
5	8	112	N 3K =	C6	110	75	10	11	102 O 3P -2	C10	200	80	15	14	105 O 2C -1	T4	50	60
5	10	102	N 3K +1	C9	130	90	10	4	103 N 3SA +1	P4	630	90	15	13	103 O 2C -1	P10	50	60
5	13	109	O 4C X -2	TA	300	100	10	1	111 N 3SA +2	PA	660	100	15	8	108 O 3C -2	K6	100	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 16.06.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	7	106	S 4C X -1	PK	-100	10	21	3	108 O 1SA +1	KD	-120	0	26	11	109 S 2SA -1	C6	-100	5
16	4	114	S 4C X -1	PK	-100	10	21	5	113 S 2P -1	KA	-100	10	26	4	108 S 3SA -1	C6	-100	5
16	3	112	N 5K -2	P5	-100	10	21	6	101 W 2SA -2	TD	100	20	26	5	110 S 2SA =	C4	120	20
16	2	110	N 4K +2	TK	170	30	21	10	109 S 2C =	P2	110	55	26	7	101 N 3K +1	T3	130	30
16	8	108	W 4P -3	KA	300	40	21	8	105 S 2C =	KA	110	55	26	6	112 S 2SA +3	C6	210	40
16	1	107	N 5K =	P8	400	60	21	7	103 N 2C =	P8	110	55	26	12	111 S 3SA =	P7	600	50
16	14	105	N 5K =	P8	400	60	21	4	110 S 2C =	P2	110	55	26	3	106 S 3SA +1	P7	630	60
16	13	103	N 5K =	P8	400	60	21	2	106 N 2C =	P8	110	55	26	13	113 S 3SA +2	C6	660	85
16	6	104	N 5K +1	P8	420	85	21	1	104 S 2C =	T3	110	55	26	10	107 S 3SA +2	C6	660	85
16	12	101	N 5K +1	P8	420	85	21	11	111 N 2C +1	TA	140	90	26	9	105 S 3SA +2	C6	660	85
16	5	102	N 3SA +2	T2	460	100	21	9	107 N 2C +2	TB	170	100	26	8	103 S 3SA +2	C6	660	85
17	9	109	W 3K +1	TK	-130	0	22	5	113 S 3SA -2	C6	-100	5	27	14	114 S 2SA -2	K5	-100	0
17	5	101	N 4C -2	K4	-100	10	22	2	106 S 3SA -2	T2	-100	5	27	12	110 N 4P -1	CK	-50	15
17	14	104	N 4C -1	TA	-50	20	22	3	108 N 2SA +2	K8	180	20	27	11	108 S 2SA -1	C8	-50	15
17	7	105	N 2C =	K4	110	40	22	11	111 S 3SA =	C9	400	60	27	5	109 S 1T +2	PK	110	30
17	3	111	N 2C =	K10	110	40	22	10	109 S 3SA =	C9	400	60	27	13	112 S 2SA =	K5	120	45
17	13	102	N 2C =	K10	110	40	22	9	107 N 3SA =	K8	400	60	27	10	106 S 2SA =	K5	120	45
17	6	103	S 2SA =	K3	120	60	22	8	105 S 3SA =	T2	400	60	27	9	104 S 2P +1	C8	140	65
17	8	107	N 3C =	TA	140	80	22	7	103 N 3SA =	K4	400	60	27	6	111 S 2P +1	K6	140	65
17	4	113	N 2C +1	K4	140	80	22	6	101 S 3SA =	C9	400	60	27	8	102 S 2SA +1	K6	150	85
17	2	108	N 3C =	TA	140	80	22	1	104 N 3SA =	KA	400	60	27	7	113 S 2SA +1	K5	150	85
17	1	106	S 2SA +1	P8	150	100	22	4	110 S 3SA +1	T2	430	100	27	4	107 S 3SA =	K5	400	100
18	3	111	W 3SA +2	P5	-460	0	23	12	112 S 6K -1	TA	-100	10	28	11	108 N 4C X -2	P10	-500	0
18	2	108	W 4C +1	TB	-450	10	23	9	106 N 5P -1	KA	-100	10	28	12	110 N 2C +1	P10	140	10
18	5	101	W 4SA =	TB	-430	25	23	2	105 N 4P -1	T3	-100	10	28	10	106 N 3C +1	P10	170	35
18	13	102	W 3SA +1	P2	-430	25	23	6	114 S 4K +1	T4	150	30	28	7	113 N 3C +1	T6	170	35
18	9	109	W 4C =	P4	-420	45	23	5	111 W 5T -3	CA	300	40	28	6	111 N 3C +1	P10	170	35
18	14	104	W 4C =	P4	-420	45	23	11	110 W 6T X -2	CA	500	50	28	4	107 N 3C +1	P10	170	35
18	4	113	W 3SA =	P4	-400	60	23	10	108 S 5K =	TA	600	60	28	8	102 N 3C +2	P10	200	60
18	8	107	O 4C -1	T7	50	85	23	7	102 S 5K +1	TA	620	80	28	14	114 N 4C =	P9	620	80
18	7	105	W 4C -1	K7	50	85	23	4	109 S 5K +1	TA	620	80	28	13	112 N 4C =	T10	620	80
18	6	103	W 4C -1	K7	50	85	23	3	107 S 5K +1	TA	620	80	28	9	104 N 4C =	P10	620	80
18	1	106	W 4C -1	TB	50	85	23	8	104 W 5C X -4	PK	1100	100	28	5	109 N 4C +1	P10	650	100
19	6	102	O 4P =	TA	-620	0	24	10	108 O 4P =	CA	-420	0						
19	2	107	O 3P +1	KB	-170	15	24	3	107 S 4C -4	KK	-200	10						
19	14	103	O 3P +1	C7	-170	15	24	9	106 O 3K +1	CA	-130	40						
19	9	108	O 3P =	C7	-140	30	24	8	104 O 3K +1	CA	-130	40						
19	7	104	W 2K =	C6	-90	45	24	7	102 O 3K +1	CA	-130	40						
19	1	105	W 2K =	C6	-90	45	24	6	114 O 3K +1	TK	-130	40						
19	4	112	N 3T -1	PA	-50	60	24	2	105 O 3K +1	CA	-130	40						
19	5	114	O 3P -1	KB	100	75	24	5	111 S 3C -2	KK	-100	70						
19	3	109	O 3P -1	KB	100	75	24	12	112 S 2C -1	KK	-50	90						
19	10	110	W 2SA -2	T9	200	95	24	11	110 S 2C -1	KK	-50	90						
19	8	106	W 2SA -2	T9	200	95	24	4	109 S 2C -1	KK	-50	90						
20	6	102	N 4P -3	K4	-300	0	25	11	109 S 3T +3	C9	170	0						
20	9	108	N 2P -2	K5	-200	25	25	5	110 S 1SA +3	KB	180	10						
20	8	106	S 3P -2	KA	-200	25	25	6	112 N 2C +3	K7	200	20						
20	7	104	N 3P -2	K5	-200	25	25	10	107 S 5T +1	P6	420	35						
20	4	112	S 4P -2	KA	-200	25	25	9	105 N 4C =	K7	420	35						
20	3	109	W 2K +2	CK	-130	50	25	4	108 N 3SA +1	K7	430	50						
20	10	110	N 2P -1	K5	-100	65	25	8	103 N 4C +1	K7	450	65						
20	2	107	S 2P -1	KA	-100	65	25	3	106 N 4C +1	P6	450	65						
20	1	105	W 2K =	TK	-90	85	25	7	101 N 3SA +2	K7	460	80						
20	14	103	W 2K =	T2	-90	85	25	13	113 S 4C +2	K10	480	95						
20	5	114	S 1P =	KA	80	100	25	12	111 S 4C +2	P4	480	95						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.