

NS-Resultate Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 26.05.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	N 2P +1	T6	140	100	10	3	101 W 3T +1	KK	-130	20	17	5	101 O 3SA +3	P6	-490	10
2	1	101	W 4C +1	P6	-450	10	11	3	113 O 3C -1	KA	50	45	18	5	101 N 1P +2	C2	140	80
3	1	113	N 2C -2	K8	-100	70	12	3	113 N 3SA =	TB	600	65	19	5	113 O 3SA +1	P2	-630	55
4	1	113	W 3K -2	T4	200	85	13	3	112 N 4K +1	C10	150	25	20	5	113 N 2P +2	K9	170	60
5	1	112	O 3P -3	KA	150	25	14	3	112 S 5T -2	PK	-100	80	21	5	112 W 3C X -1	P5	100	40
6	1	112	S 2C +2	P3	170	85	15	3	111 N 4C +1	P3	650	80	22	5	112 W 4C =	C4	-620	25
7	1	111	W 2SA -2	PA	200	80	16	3	111 W 6P -1	TA	100	100	23	5	111 O 3SA =	C3	-600	9
8	1	111	O 3K +1	C9	-130	55	17	3	110 W 5K =	C7	-400	80	24	5	111 W 4C +3	T6	-510	64
9	1	110	N 2P =	K8	110	100	18	3	110 S 1SA -1	T3	-100	40	25	5	110 W 1SA -2	P2	200	80
10	1	110	S 3K -1	TK	-100	55	19	3	109 O 5SA -1	C8	100	90	26	5	110 W 2K +4	T3	-170	30
11	1	109	S 2K =	TK	90	70	20	3	109 N 4P +1	K5	650	100	1	6	111 O 4T -2	C4	100	85
12	1	109	S 3SA =	T7	600	65	21	3	108 W 2C -2	P5	100	40	2	6	111 W 4C =	P3	-420	35
13	1	108	N 3SA +2	C8	660	95	22	3	108 W 4C =	PA	-620	25	3	6	110 O 3P =	CK	-140	20
14	1	108	W 5C =	K4	-450	10	23	3	107 N 3C -4	P6	-400	32	4	6	110 N 2C -2	P7	-200	15
15	1	107	N 3SA +2	K3	660	100	24	3	107 W 4C +3	T6	-510	64	5	6	109 N 4C +1	P10	650	85
16	1	107	O 4C +1	KD	-650	35	25	3	106 W 1SA =	C3	-90	15	6	6	109 S 4P =	KA	420	100
17	1	106	W 5K +1	P3	-420	50	26	3	106 W 4K =	P10	-130	80	7	6	108 W 3K -1	PA	100	25
18	1	106	N 2P =	TB	110	60	1	4	107 N 3P -1	KA	-50	40	8	6	108 S 2P -3	CA	-150	30
19	1	105	O 3SA +1	P2	-630	55	2	4	107 O 3SA -2	K2	100	100	11	6	106 W 4C -4	P4	200	100
20	1	105	N 4P -1	K8	-100	20	3	4	106 N 4C -4	K5	-200	0	12	6	106 N 3SA +1	C7	630	80
21	1	104	S 2SA =	CB	120	70	4	4	106 N 1SA -1	P7	-100	50	13	6	105 N 3K +2	C8	150	25
22	1	104	W 4C =	C9	-620	25	7	4	104 O 3K -2	P9	200	80	14	6	105 W 5C -1	K4	50	90
23	1	103	W 3P -2	TA	200	100	8	4	104 W 3SA -2	T10	100	100	15	6	104 N 3SA +1	K6	630	55
24	1	103	W 4C +3	PD	-510	64	9	4	103 W 3K +1	K5	-130	30	16	6	104 N 4T -2	CA	-100	90
3	2	102	W 3K =	P2	-110	45	10	4	103 S 3K -1	P8	-100	55	17	6	103 W 5K +1	C7	-420	50
4	2	102	O 2T +2	CB	-130	30	11	4	102 W 2C =	K6	-110	0	18	6	103 N 3P -1	K4	-100	40
5	2	101	N 4C +2	T5	680	100	12	4	102 S 3K +1	PA	130	10	19	6	102 O 3SA +1	P7	-630	55
6	2	101	S 2C +1	P3	140	55	13	4	101 N 3SA +2	C9	660	95	20	6	102 N 4P =	K9	620	85
7	2	113	W 4K -2	PA	200	80	14	4	101 W 5C -2	K4	100	100	21	6	101 O 3SA -4	P10	200	90
8	2	113	O 3SA =	P6	-400	15	15	4	113 N 4C +1	K6	650	80	22	6	101 W 5T -4	C9	400	100
9	2	112	N 3P -2	CA	-100	60	16	4	113 W 5P =	TA	-650	35	23	6	113 N 2C -3	P3	-300	50
10	2	112	W 2SA -3	K4	300	100	17	4	112 O 3SA -1	C5	50	100	24	6	113 W 6C +1	K8	-1010	9
11	2	111	N 3P -1	C5	-50	20	18	4	112 N 2P +1	C7	140	80	25	6	112 W 1SA -2	C3	200	80
12	2	111	N 3K +2	TB	150	25	19	4	111 O 3SA +2	P8	-660	15	26	6	112 W 5K -1	K2	100	100
13	2	110	N 5K =	C10	600	60	20	4	111 N 2P +2	K8	170	60	1	7	113 W 3C -2	PK	100	85
14	2	110	W 2C +3	K4	-200	45	21	4	110 W 2C -2	P5	100	40	2	7	113 W 4C +1	TA	-450	10
15	2	109	N 3SA -1	K8	-100	15	22	4	110 W 1SA =	K4	-90	80	3	7	112 O 2P -2	TA	200	100
16	2	109	W 4P +1	TA	-650	35	23	4	109 N 2C -1	P6	-100	91	4	7	112 O 4T -2	CB	200	85
17	2	108	W 5K +1	CD	-420	50	24	4	109 O 3SA +4	PB	-520	27	5	7	111 N 4C =	PA	620	55
18	2	108	S 3K -1	T7	-100	40	25	4	108 N 2P =	C10	110	60	6	7	111 S 2C =	PD	110	15
19	2	107	O 3SA +1	P10	-630	55	26	4	108 W 4K +1	P10	-150	50	7	7	110 W 3SA -2	PA	200	80
20	2	107	N 2P +1	T4	140	40	1	5	109 W 2C -1	PK	50	65	8	7	110 O 3K +1	PA	-130	55
21	2	106	S 3SA =	T3	600	100	2	5	109 O 3C +1	K2	-170	60	9	7	109 O 1SA =	P4	-90	80
22	2	106	S 3P -1	KK	-50	90	3	5	108 W 2K =	T8	-90	80	10	7	109 W 2C +1	K4	-140	10
23	2	105	N 3C X -2	P6	-500	18	4	5	108 N 2C +1	P7	140	70	13	7	107 N 3K +1	C10	130	0
24	2	105	W 6C +1	PD	-1010	9	5	5	107 N 4C +1	PA	650	85	14	7	107 O 5K =	TA	-400	30
25	2	104	N 2K -4	C10	-200	0	6	5	107 S 2C +1	KA	140	55	15	7	106 N 4C -1	TD	-100	15
26	2	104	N 3C -3	KB	-300	20	9	5	105 O 2SA +1	C2	-150	20	16	7	106 O 4C +1	TD	-650	35
1	3	105	S 3P -1	KA	-50	40	10	5	105 W 2SA -1	K4	100	75	17	7	105 O 6SA =	CA	-990	0
2	3	105	O 4C +1	K2	-450	10	11	5	104 N 2P -1	T5	-50	20	18	7	105 W 3C =	KK	-140	15
5	3	103	S 4C =	C4	620	55	12	5	104 N 3SA +2	TB	660	90	19	7	104 O 3SA +2	P5	-660	15
6	3	103	S 3C =	P3	140	55	13	5	103 N 3K +2	C8	150	25	20	7	104 N 4P -1	K9	-100	20
7	3	102	O 4C -1	K2	100	25	14	5	103 W 3C +2	K4	-200	45	21	7	103 W 2C =	P5	-110	0
8	3	102	O 3K +1	PA	-130	55	15	5	102 S 3SA -1	T5	-100	15	22	7	103 W 4C =	PA	-620	25
9	3	101	O 2SA =	T10	-120	45	16	5	102 W 4P +1	TA	-650	35	23	7	102 N 3C X -3	P6	-800	0

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
24	7	102	W 6C +1	PD -1010	9	5	10	104	N 4C =	TD 620	55	12	12	105	N 3K +2	C7 150	25
25	7	101	W 1T =	C3 -70	30	6	10	104	S 2C +2	T9 170	85	13	12	104	N 5K =	C10 600	60
26	7	101	W 3K +2	P10 -150	50	7	10	103	S 2P =	TA 110	50	14	12	104	W 3C +1	TB -170	60
1	8	102	O 4T =	P8 -130	10	8	10	103	W 3SA +1	P6 -430	0	15	12	103	N 3SA +1	K6 630	55
2	8	102	O 4C =	P4 -420	35	9	10	102	O 3SA +1	P9 -630	0	16	12	103	N 5T -3	CA -150	80
3	8	101	S 2C =	KA 110	90	10	10	102	W 3T -2	K4 200	90	17	12	102	W 5K +1	CD -420	50
4	8	101	N 2SA -2	T7 -200	15	11	10	101	S 2K =	TK 90	70	18	12	102	O 3C =	TA -140	15
5	8	113	N 4C =	TD 620	55	12	10	101	S 2SA +4	T4 240	50	19	12	101	O 3SA =	P5 -600	80
6	8	113	S 2C =	PD 110	15	13	10	113	N 4P +1	C10 650	80	20	12	101	N 4P -1	T4 -100	20
7	8	112	O 2SA -1	C10 100	25	14	10	113	W 4C =	K4 -420	20	23	12	112	W 2P =	TK -110	82
8	8	112	W 3SA =	T3 -400	15	15	10	112	N 4C +1	K6 650	80	24	12	112	W 4C +3	T8 -510	64
9	8	111	O 2SA =	P9 -120	45	16	10	112	W 5P =	TA -650	35	25	12	111	W 1SA -2	C3 200	80
10	8	111	W 2C =	K4 -110	35	19	10	110	O 3SA +2	P5 -660	15	26	12	111	W 5K =	TA -600	10
11	8	110	S 1SA =	TK 90	70	20	10	110	N 4P -2	K9 -200	0						
12	8	110	S 3SA +3	T4 690	100	21	10	109	S 2P +1	T3 140	80						
15	8	108	N 4C =	TD 620	40	22	10	109	W 3C =	K10 -140	70						
16	8	108	W 4P +1	TA -650	35	23	10	108	N 3C -3	P3 -300	50						
17	8	107	W 5K +2	P4 -440	20	24	10	108	W 5C +2	PD -510	64						
18	8	107	N 2P +2	K4 170	100	25	10	107	O 3C -3	TK 300	100						
19	8	106	W 3SA +2	P5 -660	15	26	10	107	W 3K +1	TB -130	80						
20	8	106	N 4P =	K9 620	85	1	11	108	N 3P -1	K3 -50	40						
21	8	105	W 3C -1	P5 50	10	2	11	108	O 4P -1	K5 50	80						
22	8	105	W 4C =	K9 -620	25	3	11	107	W 2K +1	CB -110	45						
23	8	104	N 3C -4	P6 -400	32	4	11	107	N 2C -1	P7 -100	50						
24	8	104	W 4C +3	P4 -510	64	5	11	106	O 2P -1	KA 50	0						
25	8	103	W 1SA =	K2 -90	15	6	11	106	W 1K =	CA -70	0						
26	8	103	W 4K +1	C2 -150	50	7	11	105	O 4C X -1	KK 200	80						
1	9	104	O 3T -1	PB 50	65	8	11	105	W 1SA +1	P6 -120	80						
2	9	104	O 4C -1	K2 50	80	9	11	104	W 2K =	T7 -90	80						
3	9	103	W 2K +1	P4 -110	45	10	11	104	S 3K -2	P8 -200	0						
4	9	103	N 2C X -2	P7 -500	0	11	11	103	S 2K -1	TK -50	20						
5	9	102	O 3P -2	KA 100	10	12	11	103	N 3K =	TB 110	0						
6	9	102	S 2C +1	KA 140	55	13	11	102	N 2K +3	C10 150	25						
7	9	101	W 1K +2	C2 -110	0	14	11	102	W 4C +2	TB -480	0						
8	9	101	O 3K +1	P6 -130	55	15	11	101	N 3SA -1	K6 -100	15						
9	9	113	O 3SA =	T10 -600	10	16	11	101	W 4P +1	TA -650	35						
10	9	113	W 2C =	K4 -110	35	17	11	113	W 5K +1	CD -420	50						
11	9	112	O 2C -1	KA 50	45	18	11	113	S 3K -2	TK -200	0						
12	9	112	S 2K +4	C2 170	40	21	11	111	O 3SA -2	CA 100	40						
13	9	111	N 5K =	C10 600	60	22	11	111	W 4C =	PA -620	25						
14	9	111	O 3K +2	TA -150	70	23	11	110	N 2C -2	P3 -200	68						
17	9	109	W 3K +3	CD -170	90	24	11	110	W 4C +3	P4 -510	64						
18	9	109	N 2P +1	K4 140	80	25	11	109	W 1SA -1	CD 100	45						
19	9	108	O 3SA -3	P5 300	100	26	11	109	W 3K +1	TA -130	80						
20	9	108	N 2P +2	C10 170	60	1	12	110	W 2K +2	CA -130	10						
21	9	107	O 3T -2	CA 100	40	2	12	110	W 3C +2	TA -200	50						
22	9	107	W 2C +2	K4 -170	60	3	12	109	W 3K =	T3 -110	45						
23	9	106	N 2C X -1	P6 -200	68	4	12	109	N 2C -1	P7 -100	50						
24	9	106	W 4C +2	C4 -480	100	5	12	108	S 1K +4	C2 150	25						
25	9	105	W 1SA -1	C3 100	45	6	12	108	N 2SA =	T2 120	30						
26	9	105	W 3SA +3	T3 -690	0	7	12	107	W 2K -1	PA 100	25						
1	10	106	O 3K +1	P5 -130	10	8	12	107	O 2K +1	PA -110	90						
2	10	106	W 4C -1	P6 50	80	9	12	106	W 2K =	PA -90	80						
3	10	105	O 2SA +1	TA -150	10	10	12	106	O 3P -1	CK 100	75						
4	10	105	W 3SA -3	C5 300	100	11	12	105	O 2SA -2	KA 100	90						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
1	1	101	N 2P +1	T6	-140	0	12	11	103	N 3K =	TB	-110	100	25	9	105	W 1SA -1	C3	-100	55
2	1	101	W 4C +1	P6	450	90	13	5	103	N 3K +2	C8	-150	75	26	9	105	W 3SA +3	T3	690	100
3	8	101	S 2C =	KA	-110	10	14	5	103	W 3C +2	K4	200	55	1	10	106	O 3K +1	P5	130	90
4	8	101	N 2SA -2	T7	200	85	15	12	103	N 3SA +1	K6	-630	45	2	10	106	W 4C -1	P6	-50	20
5	2	101	N 4C +2	T5	-680	0	16	12	103	N 5T -3	CA	150	20	3	4	106	N 4C -4	K5	200	100
6	2	101	S 2C +1	P3	-140	45	17	6	103	W 5K +1	C7	420	50	4	4	106	N 1SA -1	P7	100	50
7	9	101	W 1K +2	C2	110	100	18	6	103	N 3P -1	K4	100	60	5	11	106	O 2P -1	KA	-50	100
8	9	101	O 3K +1	P6	130	45	21	7	103	W 2C =	P5	110	100	6	11	106	W 1K =	CA	70	100
9	3	101	O 2SA =	T10	120	55	22	7	103	W 4C =	PA	620	75	9	12	106	W 2K =	PA	90	20
10	3	101	W 3T +1	KK	130	80	23	1	103	W 3P -2	TA	-200	0	10	12	106	O 3P -1	CK	-100	25
11	10	101	S 2K =	TK	-90	30	24	1	103	W 4C +3	PD	510	36	11	6	106	W 4C -4	P4	-200	0
12	10	101	S 2SA +4	T4	-240	50	25	8	103	W 1SA =	K2	90	85	12	6	106	N 3SA +1	C7	-630	20
13	4	101	N 3SA +2	C9	-660	5	26	8	103	W 4K +1	C2	150	50	15	7	106	N 4C -1	TD	100	85
14	4	101	W 5C -2	K4	-100	0	1	9	104	O 3T -1	PB	-50	35	16	7	106	O 4C +1	TD	650	65
15	11	101	N 3SA -1	K6	100	85	2	9	104	O 4C -1	K2	-50	20	17	1	106	W 5K +1	P3	420	50
16	11	101	W 4P +1	TA	650	65	5	10	104	N 4C =	TD	-620	45	18	1	106	N 2P =	TB	-110	40
17	5	101	O 3SA +3	P6	490	90	6	10	104	S 2C +2	T9	-170	15	19	8	106	W 3SA +2	P5	660	85
18	5	101	N 1P +2	C2	-140	20	7	4	104	O 3K -2	P9	-200	20	20	8	106	N 4P =	K9	-620	15
19	12	101	O 3SA =	P5	600	20	8	4	104	W 3SA -2	T10	-100	0	21	2	106	S 3SA =	T3	-600	0
20	12	101	N 4P -1	T4	100	80	9	11	104	W 2K =	T7	90	20	22	2	106	S 3P -1	KK	50	10
21	6	101	O 3SA -4	P10	-200	10	10	11	104	S 3K -2	P8	200	100	23	9	106	N 2C X -1	P6	200	32
22	6	101	W 5T -4	C9	-400	0	11	5	104	N 2P -1	T5	50	80	24	9	106	W 4C +2	C4	480	0
25	7	101	W 1T =	C3	70	70	12	5	104	N 3SA +2	TB	-660	10	25	3	106	W 1SA =	C3	90	85
26	7	101	W 3K +2	P10	150	50	13	12	104	N 5K =	C10	-600	40	26	3	106	W 4K =	P10	130	20
1	8	102	O 4T =	P8	130	90	14	12	104	W 3C +1	TB	170	40	1	4	107	N 3P -1	KA	50	60
2	8	102	O 4C =	P4	420	65	15	6	104	N 3SA +1	K6	-630	45	2	4	107	O 3SA -2	K2	-100	0
3	2	102	W 3K =	P2	110	55	16	6	104	N 4T -2	CA	100	10	3	11	107	W 2K +1	CB	110	55
4	2	102	O 2T +2	CB	130	70	19	7	104	O 3SA +2	P5	660	85	4	11	107	N 2C -1	P7	100	50
5	9	102	O 3P -2	KA	-100	90	20	7	104	N 4P -1	K9	100	80	5	5	107	N 4C +1	PA	-650	15
6	9	102	S 2C +1	KA	-140	45	21	1	104	S 2SA =	CB	-120	30	6	5	107	S 2C +1	KA	-140	45
7	3	102	O 4C -1	K2	-100	75	22	1	104	W 4C =	C9	620	75	7	12	107	W 2K -1	PA	-100	75
8	3	102	O 3K +1	PA	130	45	23	8	104	N 3C -4	P6	400	68	8	12	107	O 2K +1	PA	110	10
9	10	102	O 3SA +1	P9	630	100	24	8	104	W 4C +3	P4	510	36	13	7	107	N 3K +1	C10	-130	100
10	10	102	W 3T -2	K4	-200	10	25	2	104	N 2K -4	C10	200	100	14	7	107	O 5K =	TA	400	70
11	4	102	W 2C =	K6	110	100	26	2	104	N 3C -3	KB	300	80	15	1	107	N 3SA +2	K3	-660	0
12	4	102	S 3K +1	PA	-130	90	1	3	105	S 3P -1	KA	50	60	16	1	107	O 4C +1	KD	650	65
13	11	102	N 2K +3	C10	-150	75	2	3	105	O 4C +1	K2	450	90	17	8	107	W 5K +2	P4	440	80
14	11	102	W 4C +2	TB	480	100	3	10	105	O 2SA +1	TA	150	90	18	8	107	N 2P +2	K4	-170	0
15	5	102	S 3SA -1	T5	100	85	4	10	105	W 3SA -3	C5	-300	0	19	2	107	O 3SA +1	P10	630	45
16	5	102	W 4P +1	TA	650	65	7	11	105	O 4C X -1	KK	-200	20	20	2	107	N 2P +1	T4	-140	60
17	12	102	W 5K +1	CD	420	50	8	11	105	W 1SA +1	P6	120	20	21	9	107	O 3T -2	CA	-100	60
18	12	102	O 3C =	TA	140	85	9	5	105	O 2SA +1	C2	150	80	22	9	107	W 2C +2	K4	170	40
19	6	102	O 3SA +1	P7	630	45	10	5	105	W 2SA -1	K4	-100	25	23	3	107	N 3C -4	P6	400	68
20	6	102	N 4P =	K9	-620	15	11	12	105	O 2SA -2	KA	-100	10	24	3	107	W 4C +3	T6	510	36
23	7	102	N 3C X -3	P6	800	100	12	12	105	N 3K +2	C7	-150	75	25	10	107	O 3C -3	TK	-300	0
24	7	102	W 6C +1	PD	1010	91	13	6	105	N 3K +2	C8	-150	75	26	10	107	W 3K +1	TB	130	20
3	9	103	W 2K +1	P4	110	55	14	6	105	W 5C -1	K4	-50	10	1	11	108	N 3P -1	K3	50	60
4	9	103	N 2C X -2	P7	500	100	17	7	105	O 6SA =	CA	990	100	2	11	108	O 4P -1	K5	-50	20
5	3	103	S 4C =	C4	-620	45	18	7	105	W 3C =	KK	140	85	3	5	108	W 2K =	T8	90	20
6	3	103	S 3C =	P3	-140	45	19	1	105	O 3SA +1	P2	630	45	4	5	108	N 2C +1	P7	-140	30
7	10	103	S 2P =	TA	-110	50	20	1	105	N 4P -1	K8	100	80	5	12	108	S 1K +4	C2	-150	75
8	10	103	W 3SA +1	P6	430	100	21	8	105	W 3C -1	P5	-50	90	6	12	108	N 2SA =	T2	-120	70
9	4	103	W 3K +1	K5	130	70	22	8	105	W 4C =	K9	620	75	7	6	108	W 3K -1	PA	-100	75
10	4	103	S 3K -1	P8	100	45	23	2	105	N 3C X -2	P6	500	82	8	6	108	S 2P -3	CA	150	70
11	11	103	S 2K -1	TK	50	80	24	2	105	W 6C +1	PD	1010	91	13	1	108	N 3SA +2	C8	-660	5

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

OW-Resultate Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 26.05.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
14	1	108	W 5C =	K4	450	90	25	5	110	W 1SA -2	P2	-200	20	10	9	113	W 2C =	K4	110	65
15	8	108	N 4C =	TD	-620	60	26	5	110	W 2K +4	T3	170	70	11	3	113	O 3C -1	KA	-50	55
16	8	108	W 4P +1	TA	650	65	1	6	111	O 4T -2	C4	-100	15	12	3	113	N 3SA =	TB	-600	35
17	2	108	W 5K +1	CD	420	50	2	6	111	W 4C =	P3	420	65	13	10	113	N 4P +1	C10	-650	20
18	2	108	S 3K -1	T7	100	60	5	7	111	N 4C =	PA	-620	45	14	10	113	W 4C =	K4	420	80
19	9	108	O 3SA -3	P5	-300	0	6	7	111	S 2C =	PD	-110	85	15	4	113	N 4C +1	K6	-650	20
20	9	108	N 2P +2	C10	-170	40	7	1	111	W 2SA -2	PA	-200	20	16	4	113	W 5P =	TA	650	65
21	3	108	W 2C -2	P5	-100	60	8	1	111	O 3K +1	C9	130	45	17	11	113	W 5K +1	CD	420	50
22	3	108	W 4C =	PA	620	75	9	8	111	O 2SA =	P9	120	55	18	11	113	S 3K -2	TK	200	100
23	10	108	N 3C -3	P3	300	50	10	8	111	W 2C =	K4	110	65	19	5	113	O 3SA +1	P2	630	45
24	10	108	W 5C +2	PD	510	36	11	2	111	N 3P -1	C5	50	80	20	5	113	N 2P +2	K9	-170	40
25	4	108	N 2P =	C10	-110	40	12	2	111	N 3K +2	TB	-150	75	23	6	113	N 2C -3	P3	300	50
26	4	108	W 4K +1	P10	150	50	13	9	111	N 5K =	C10	-600	40	24	6	113	W 6C +1	K8	1010	91
1	5	109	W 2C -1	PK	-50	35	14	9	111	O 3K +2	TA	150	30							
2	5	109	O 3C +1	K2	170	40	15	3	111	N 4C +1	P3	-650	20							
3	12	109	W 3K =	T3	110	55	16	3	111	W 6P -1	TA	-100	0							
4	12	109	N 2C -1	P7	100	50	19	4	111	O 3SA +2	P8	660	85							
5	6	109	N 4C +1	P10	-650	15	20	4	111	N 2P +2	K8	-170	40							
6	6	109	S 4P =	KA	-420	0	21	11	111	O 3SA -2	CA	-100	60							
9	7	109	O 1SA =	P4	90	20	22	11	111	W 4C =	PA	620	75							
10	7	109	W 2C +1	K4	140	90	23	5	111	O 3SA =	C3	600	91							
11	1	109	S 2K =	TK	-90	30	24	5	111	W 4C +3	T6	510	36							
12	1	109	S 3SA =	T7	-600	35	25	12	111	W 1SA -2	C3	-200	20							
15	2	109	N 3SA -1	K8	100	85	26	12	111	W 5K =	TA	600	90							
16	2	109	W 4P +1	TA	650	65	3	7	112	O 2P -2	TA	-200	0							
17	9	109	W 3K +3	CD	170	10	4	7	112	O 4T -2	CB	-200	15							
18	9	109	N 2P +1	K4	-140	20	5	1	112	O 3P -3	KA	-150	75							
19	3	109	O 5SA -1	C8	-100	10	6	1	112	S 2C +2	P3	-170	15							
20	3	109	N 4P +1	K5	-650	0	7	8	112	O 2SA -1	C10	-100	75							
21	10	109	S 2P +1	T3	-140	20	8	8	112	W 3SA =	T3	400	85							
22	10	109	W 3C =	K10	140	30	9	2	112	N 3P -2	CA	100	40							
23	4	109	N 2C -1	P6	100	9	10	2	112	W 2SA -3	K4	-300	0							
24	4	109	O 3SA +4	PB	520	73	11	9	112	O 2C -1	KA	-50	55							
25	11	109	W 1SA -1	CD	-100	55	12	9	112	S 2K +4	C2	-170	60							
26	11	109	W 3K +1	TA	130	20	13	3	112	N 4K +1	C10	-150	75							
1	12	110	W 2K +2	CA	130	90	14	3	112	S 5T -2	PK	100	20							
2	12	110	W 3C +2	TA	200	50	15	10	112	N 4C +1	K6	-650	20							
3	6	110	O 3P =	CK	140	80	16	10	112	W 5P =	TA	650	65							
4	6	110	N 2C -2	P7	200	85	17	4	112	O 3SA -1	C5	-50	0							
7	7	110	W 3SA -2	PA	-200	20	18	4	112	N 2P +1	C7	-140	20							
8	7	110	O 3K +1	PA	130	45	21	5	112	W 3C X -1	P5	-100	60							
9	1	110	N 2P =	K8	-110	0	22	5	112	W 4C =	C4	620	75							
10	1	110	S 3K -1	TK	100	45	23	12	112	W 2P =	TK	110	18							
11	8	110	S 1SA =	TK	-90	30	24	12	112	W 4C +3	T8	510	36							
12	8	110	S 3SA +3	T4	-690	0	25	6	112	W 1SA -2	C3	-200	20							
13	2	110	N 5K =	C10	-600	40	26	6	112	W 5K -1	K2	-100	0							
14	2	110	W 2C +3	K4	200	55	1	7	113	W 3C -2	PK	-100	15							
17	3	110	W 5K =	C7	400	20	2	7	113	W 4C +1	TA	450	90							
18	3	110	S 1SA -1	T3	100	60	3	1	113	N 2C -2	K8	100	30							
19	10	110	O 3SA +2	P5	660	85	4	1	113	W 3K -2	T4	-200	15							
20	10	110	N 4P -2	K9	200	100	5	8	113	N 4C =	TD	-620	45							
21	4	110	W 2C -2	P5	-100	60	6	8	113	S 2C =	PD	-110	85							
22	4	110	W 1SA =	K4	90	20	7	2	113	W 4K -2	PA	-200	20							
23	11	110	N 2C -2	P3	200	32	8	2	113	O 3SA =	P6	400	85							
24	11	110	W 4C +3	P4	510	36	9	9	113	O 3SA =	T10	600	90							

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.