

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 26.05.2015**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	12	110	W 2K +2	CA	-130	10	6	11	106 W 1K =	CA	-70	0	11	4	102 W 2C =	K6	-110	0
1	10	106	O 3K +1	P5	-130	10	6	8	113 S 2C =	PD	110	15	11	5	104 N 2P -1	T5	-50	20
1	8	102	O 4T =	P8	-130	10	6	7	111 S 2C =	PD	110	15	11	2	111 N 3P -1	C5	-50	20
1	11	108	N 3P -1	K3	-50	40	6	12	108 N 2SA =	T2	120	30	11	11	103 S 2K -1	TK	-50	20
1	4	107	N 3P -1	KA	-50	40	6	3	103 S 3C =	P3	140	55	11	3	113 O 3C -1	KA	50	45
1	3	105	S 3P -1	KA	-50	40	6	2	101 S 2C +1	P3	140	55	11	9	112 O 2C -1	KA	50	45
1	9	104	O 3T -1	PB	50	65	6	9	102 S 2C +1	KA	140	55	11	1	109 S 2K =	TK	90	70
1	5	109	W 2C -1	PK	50	65	6	5	107 S 2C +1	KA	140	55	11	10	101 S 2K =	TK	90	70
1	7	113	W 3C -2	PK	100	85	6	1	112 S 2C +2	P3	170	85	11	8	110 S 1SA =	TK	90	70
1	6	111	O 4T -2	C4	100	85	6	10	104 S 2C +2	T9	170	85	11	12	105 O 2SA -2	KA	100	90
1	1	101	N 2P +1	T6	140	100	6	6	109 S 4P =	KA	420	100	11	6	106 W 4C -4	P4	200	100
2	1	101	W 4C +1	P6	-450	10	7	9	101 W 1K +2	C2	-110	0	12	11	103 N 3K =	TB	110	0
2	7	113	W 4C +1	TA	-450	10	7	3	102 O 4C -1	K2	100	25	12	4	102 S 3K +1	PA	130	10
2	3	105	O 4C +1	K2	-450	10	7	12	107 W 2K -1	PA	100	25	12	2	111 N 3K +2	TB	150	25
2	8	102	O 4C =	P4	-420	35	7	8	112 O 2SA -1	C10	100	25	12	12	105 N 3K +2	C7	150	25
2	6	111	W 4C =	P3	-420	35	7	6	108 W 3K -1	PA	100	25	12	9	112 S 2K +4	C2	170	40
2	12	110	W 3C +2	TA	-200	50	7	10	103 S 2P =	TA	110	50	12	10	101 S 2SA +4	T4	240	50
2	5	109	O 3C +1	K2	-170	60	7	4	104 O 3K -2	P9	200	80	12	3	113 N 3SA =	TB	600	65
2	11	108	O 4P -1	K5	50	80	7	2	113 W 4K -2	PA	200	80	12	1	109 S 3SA =	T7	600	65
2	10	106	W 4C -1	P6	50	80	7	1	111 W 2SA -2	PA	200	80	12	6	106 N 3SA +1	C7	630	80
2	9	104	O 4C -1	K2	50	80	7	11	105 O 4C X -1	KK	200	80	12	5	104 N 3SA +2	TB	660	90
2	4	107	O 3SA -2	K2	100	100	7	7	110 W 3SA -2	PA	200	80	12	8	110 S 3SA +3	T4	690	100
3	4	106	N 4C -4	K5	-200	0	8	10	103 W 3SA +1	P6	-430	0	13	7	107 N 3K +1	C10	130	0
3	10	105	O 2SA +1	TA	-150	10	8	2	113 O 3SA =	P6	-400	15	13	6	105 N 3K +2	C8	150	25
3	6	110	O 3P =	CK	-140	20	8	8	112 W 3SA =	T3	-400	15	13	5	103 N 3K +2	C8	150	25
3	2	102	W 3K =	P2	-110	45	8	6	108 S 2P -3	CA	-150	30	13	3	112 N 4K +1	C10	150	25
3	12	109	W 3K =	T3	-110	45	8	3	102 O 3K +1	PA	-130	55	13	11	102 N 2K +3	C10	150	25
3	11	107	W 2K +1	CB	-110	45	8	1	111 O 3K +1	C9	-130	55	13	2	110 N 5K =	C10	600	60
3	9	103	W 2K +1	P4	-110	45	8	9	101 O 3K +1	P6	-130	55	13	12	104 N 5K =	C10	600	60
3	1	113	N 2C -2	K8	-100	70	8	7	110 O 3K +1	PA	-130	55	13	9	111 N 5K =	C10	600	60
3	5	108	W 2K =	T8	-90	80	8	11	105 W 1SA +1	P6	-120	80	13	10	113 N 4P +1	C10	650	80
3	8	101	S 2C =	KA	110	90	8	12	107 O 2K +1	PA	-110	90	13	4	101 N 3SA +2	C9	660	95
3	7	112	O 2P -2	TA	200	100	8	4	104 W 3SA -2	T10	100	100	13	1	108 N 3SA +2	C8	660	95
4	9	103	N 2C X -2	P7	-500	0	9	10	102 O 3SA +1	P9	-630	0	14	11	102 W 4C +2	TB	-480	0
4	8	101	N 2SA -2	T7	-200	15	9	9	113 O 3SA =	T10	-600	10	14	1	108 W 5C =	K4	-450	10
4	6	110	N 2C -2	P7	-200	15	9	5	105 O 2SA +1	C2	-150	20	14	10	113 W 4C =	K4	-420	20
4	2	102	O 2T +2	CB	-130	30	9	4	103 W 3K +1	K5	-130	30	14	7	107 O 5K =	TA	-400	30
4	12	109	N 2C -1	P7	-100	50	9	3	101 O 2SA =	T10	-120	45	14	5	103 W 3C +2	K4	-200	45
4	11	107	N 2C -1	P7	-100	50	9	8	111 O 2SA =	P9	-120	45	14	2	110 W 2C +3	K4	-200	45
4	4	106	N 1SA -1	P7	-100	50	9	2	112 N 3P -2	CA	-100	60	14	12	104 W 3C +1	TB	-170	60
4	5	108	N 2C +1	P7	140	70	9	12	106 W 2K =	PA	-90	80	14	9	111 O 3K +2	TA	-150	70
4	1	113	W 3K -2	T4	200	85	9	11	104 W 2K =	T7	-90	80	14	3	112 S 5T -2	PK	-100	80
4	7	112	O 4T -2	CB	200	85	9	7	109 O 1SA =	P4	-90	80	14	6	105 W 5C -1	K4	50	90
4	10	105	W 3SA -3	C5	300	100	9	1	110 N 2P =	K8	110	100	14	4	101 W 5C -2	K4	100	100
5	11	106	O 2P -1	KA	50	0	10	11	104 S 3K -2	P8	-200	0	15	7	106 N 4C -1	TD	-100	15
5	9	102	O 3P -2	KA	100	10	10	7	109 W 2C +1	K4	-140	10	15	5	102 S 3SA -1	T5	-100	15
5	1	112	O 3P -3	KA	150	25	10	3	101 W 3T +1	KK	-130	20	15	2	109 N 3SA -1	K8	-100	15
5	12	108	S 1K +4	C2	150	25	10	9	113 W 2C =	K4	-110	35	15	11	101 N 3SA -1	K6	-100	15
5	3	103	S 4C =	C4	620	55	10	8	111 W 2C =	K4	-110	35	15	8	108 N 4C =	TD	620	40
5	10	104	N 4C =	TD	620	55	10	4	103 S 3K -1	P8	-100	55	15	6	104 N 3SA +1	K6	630	55
5	8	113	N 4C =	TD	620	55	10	1	110 S 3K -1	TK	-100	55	15	12	103 N 3SA +1	K6	630	55
5	7	111	N 4C =	PA	620	55	10	5	105 W 2SA -1	K4	100	75	15	4	113 N 4C +1	K6	650	80
5	6	109	N 4C +1	P10	650	85	10	12	106 O 3P -1	CK	100	75	15	3	111 N 4C +1	P3	650	80
5	5	107	N 4C +1	PA	650	85	10	10	102 W 3T -2	K4	200	90	15	10	112 N 4C +1	K6	650	80
5	2	101	N 4C +2	T5	680	100	10	2	112 W 2SA -3	K4	300	100	15	1	107 N 3SA +2	K3	660	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 26.05.2015**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	8	108	W 4P +1	TA	-650	35	21	7	103 W 2C =	P5	-110	0	25	5	110 W 1SA -2	P2	200	80
16	7	106	O 4C +1	TD	-650	35	21	8	105 W 3C -1	P5	50	10	25	10	107 O 3C -3	TK	300	100
16	5	102	W 4P +1	TA	-650	35	21	11	111 O 3SA -2	CA	100	40	26	9	105 W 3SA +3	T3	-690	0
16	4	113	W 5P =	TA	-650	35	21	9	107 O 3T -2	CA	100	40	26	12	111 W 5K =	TA	-600	10
16	2	109	W 4P +1	TA	-650	35	21	5	112 W 3C X -1	P5	100	40	26	2	104 N 3C -3	KB	-300	20
16	1	107	O 4C +1	KD	-650	35	21	4	110 W 2C -2	P5	100	40	26	5	110 W 2K +4	T3	-170	30
16	11	101	W 4P +1	TA	-650	35	21	3	108 W 2C -2	P5	100	40	26	8	103 W 4K +1	C2	-150	50
16	10	112	W 5P =	TA	-650	35	21	1	104 S 2SA =	CB	120	70	26	7	101 W 3K +2	P10	-150	50
16	12	103	N 5T -3	CA	-150	80	21	10	109 S 2P +1	T3	140	80	26	4	108 W 4K +1	P10	-150	50
16	6	104	N 4T -2	CA	-100	90	21	6	101 O 3SA -4	P10	200	90	26	11	109 W 3K +1	TA	-130	80
16	3	111	W 6P -1	TA	100	100	21	2	106 S 3SA =	T3	600	100	26	10	107 W 3K +1	TB	-130	80
17	7	105	O 6SA =	CA	-990	0	22	11	111 W 4C =	PA	-620	25	26	3	106 W 4K =	P10	-130	80
17	5	101	O 3SA +3	P6	-490	10	22	8	105 W 4C =	K9	-620	25	26	6	112 W 5K -1	K2	100	100
17	8	107	W 5K +2	P4	-440	20	22	7	103 W 4C =	PA	-620	25						
17	6	103	W 5K +1	C7	-420	50	22	5	112 W 4C =	C4	-620	25						
17	2	108	W 5K +1	CD	-420	50	22	3	108 W 4C =	PA	-620	25						
17	1	106	W 5K +1	P3	-420	50	22	1	104 W 4C =	C9	-620	25						
17	12	102	W 5K +1	CD	-420	50	22	9	107 W 2C +2	K4	-170	60						
17	11	113	W 5K +1	CD	-420	50	22	10	109 W 3C =	K10	-140	70						
17	3	110	W 5K =	C7	-400	80	22	4	110 W 1SA =	K4	-90	80						
17	9	109	W 3K +3	CD	-170	90	22	2	106 S 3P -1	KK	-50	90						
17	4	112	O 3SA -1	C5	50	100	22	6	101 W 5T -4	C9	400	100						
18	11	113	S 3K -2	TK	-200	0	23	7	102 N 3C X -3	P6	-800	0						
18	7	105	W 3C =	KK	-140	15	23	5	111 O 3SA =	C3	-600	9						
18	12	102	O 3C =	TA	-140	15	23	2	105 N 3C X -2	P6	-500	18						
18	6	103	N 3P -1	K4	-100	40	23	8	104 N 3C -4	P6	-400	32						
18	3	110	S 1SA -1	T3	-100	40	23	3	107 N 3C -4	P6	-400	32						
18	2	108	S 3K -1	T7	-100	40	23	10	108 N 3C -3	P3	-300	50						
18	1	106	N 2P =	TB	110	60	23	6	113 N 2C -3	P3	-300	50						
18	9	109	N 2P +1	K4	140	80	23	11	110 N 2C -2	P3	-200	68						
18	5	101	N 1P +2	C2	140	80	23	9	106 N 2C X -1	P6	-200	68						
18	4	112	N 2P +1	C7	140	80	23	12	112 W 2P =	TK	-110	82						
18	8	107	N 2P +2	K4	170	100	23	4	109 N 2C -1	P6	-100	91						
19	10	110	O 3SA +2	P5	-660	15	23	1	103 W 3P -2	TA	200	100						
19	8	106	W 3SA +2	P5	-660	15	24	7	102 W 6C +1	PD	-1010	9						
19	7	104	O 3SA +2	P5	-660	15	24	6	113 W 6C +1	K8	-1010	9						
19	4	111	O 3SA +2	P8	-660	15	24	2	105 W 6C +1	PD	-1010	9						
19	6	102	O 3SA +1	P7	-630	55	24	4	109 O 3SA +4	PB	-520	27						
19	5	113	O 3SA +1	P2	-630	55	24	12	112 W 4C +3	T8	-510	64						
19	2	107	O 3SA +1	P10	-630	55	24	11	110 W 4C +3	P4	-510	64						
19	1	105	O 3SA +1	P2	-630	55	24	10	108 W 5C +2	PD	-510	64						
19	12	101	O 3SA =	P5	-600	80	24	8	104 W 4C +3	P4	-510	64						
19	3	109	O 5SA -1	C8	100	90	24	5	111 W 4C +3	T6	-510	64						
19	9	108	O 3SA -3	P5	300	100	24	3	107 W 4C +3	T6	-510	64						
20	10	110	N 4P -2	K9	-200	0	24	1	103 W 4C +3	PD	-510	64						
20	7	104	N 4P -1	K9	-100	20	24	9	106 W 4C +2	C4	-480	100						
20	1	105	N 4P -1	K8	-100	20	25	2	104 N 2K -4	C10	-200	0						
20	12	101	N 4P -1	T4	-100	20	25	8	103 W 1SA =	K2	-90	15						
20	2	107	N 2P +1	T4	140	40	25	3	106 W 1SA =	C3	-90	15						
20	9	108	N 2P +2	C10	170	60	25	7	101 W 1T =	C3	-70	30						
20	5	113	N 2P +2	K9	170	60	25	11	109 W 1SA -1	CD	100	45						
20	4	111	N 2P +2	K8	170	60	25	9	105 W 1SA -1	C3	100	45						
20	8	106	N 4P =	K9	620	85	25	4	108 N 2P =	C10	110	60						
20	6	102	N 4P =	K9	620	85	25	12	111 W 1SA -2	C3	200	80						
20	3	109	N 4P +1	K5	650	100	25	6	112 W 1SA -2	C3	200	80						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.