

NS-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 21.05.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
1	1	101	W 4C X -1 KA	100	75	8	3	103	W 3SA -1 C8	50	62	3	5	109	N 4P -2 T9	-100	0
2	1	101	S 3SA +1 K2	630	56	9	3	103	W 4P +2 TK	-680	31	4	5	108	O 2P +2 TA	-170	12
3	1	101	S 3SA +1 T5	430	25	10	3	102	S 4C +3 T10	710	62	5	5	108	S 3C = K6	140	25
4	1	111	W 3P = TD	-140	44	11	3	102	S 3SA +1 T5	430	94	6	5	108	N 4P +2 T7	480	6
5	1	111	S 3C +1 PA	170	44	12	3	102	W 4P = T9	-420	19	13	5	105	S 5T = CA	600	81
6	1	111	N 5P +1 K5	480	6	13	3	101	S 4T +1 CA	150	12	14	5	105	N 2C = TD	110	38
7	1	110	O 3T = C5	-110	31	14	3	101	N 2C +1 P2	140	75	15	5	105	W 3C +1 K2	-170	38
8	1	110	W 1SA = CD	-90	31	15	3	101	W 3C = K2	-140	56	16	5	104	W 4P +1 CD	-650	6
9	1	110	O 3SA +3 T4	-690	12	16	3	111	W 4P = CD	-620	44	17	5	104	N 3SA -1 T3	-50	44
10	1	109	N 3SA +4 T2	720	94	17	3	111	S 4C -2 T6	-100	6	18	5	104	N 3SA +3 K5	690	19
11	1	109	S 3SA = T5	400	56	18	3	111	N 6C +1 K5	1460	81	19	5	103	O 2C -2 K8	200	100
12	1	109	W 3P = T9	-140	56	19	3	110	N 1SA +2 C4	150	69	20	5	103	N 3SA +4 P6	720	25
13	1	108	S 3T +4 KB	190	44	20	3	110	N 6SA = T5	1440	69	21	5	103	O 3SA +1 T3	-430	25
14	1	108	N 3C = TD	140	75	21	3	110	W 3SA = T4	-400	69	22	5	102	O 4C +1 K5	-650	19
15	1	108	N 5P -2 C4	-200	12	22	3	109	O 4C = P4	-620	75	23	5	102	O 3SA -1 C10	100	75
16	1	107	W 4P -1 CD	100	100	23	3	109	O 3SA = C10	-600	6	24	5	102	S 3T -3 C2	-150	12
17	1	107	S 3C = T9	140	94	24	3	109	S 3SA +2 C2	460	94	25	5	101	W 2P -1 KD	100	69
18	1	107	S 6C +1 K9	1460	81	25	3	108	W 2P -1 KD	100	69	26	5	101	O 3C = P8	-140	19
19	1	106	S 2P +1 CB	140	31	26	3	108	O 2C -2 P8	200	88	27	5	101	N 2P +1 CA	140	88
20	1	106	N 6SA = PA	1440	69	27	3	108	N 3P -1 TB	-50	25	28	5	111	O 2SA +2 CA	-180	50
21	1	106	O 3SA +2 P4	-460	0	28	3	107	W 2K +2 C6	-130	75	29	5	111	N 2P -1 KK	-100	62
22	1	105	O 4C +1 K5	-650	19	29	3	107	N 2P -1 K5	-100	62	30	5	111	W 4C -3 PA	150	50
23	1	105	O 2SA +1 C10	-150	44	30	3	107	S 5K +1 TA	420	75	31	5	110	W 2C +1 P5	-140	0
24	1	105	S 3SA -1 C2	-50	31	31	3	106	S 3P +1 T9	170	75	32	5	110	S 3P -1 C3	-50	19
25	1	104	N 1SA -1 K2	-50	25	32	3	106	S 2P +1 KB	140	94	33	5	110	O 1SA +2 PA	-150	12
26	1	104	S 5T = C6	600	100	33	3	106	O 1SA -2 P3	100	94	1	6	111	W 4C X -1 TA	100	75
27	1	104	N 4P -2 K2	-100	0	1	4	107	N 4T -1 CK	-50	38	2	6	111	S 3SA +1 P10	630	56
4	2	102	S 3T = K4	110	94	2	4	107	N 3SA +1 K8	630	56	3	6	111	N 3SA +2 C2	460	56
5	2	102	S 4C = T7	620	81	3	4	107	S 3SA +3 T5	490	88	4	6	110	O 2P +1 TA	-140	44
6	2	102	N 6P = K5	980	94	10	4	104	S 4C +2 K10	680	38	5	6	110	S 4C -1 K6	-100	0
7	2	101	S 3P -2 T6	-200	12	11	4	104	S 3SA = C10	400	56	6	6	110	N 3SA +4 K5	520	75
8	2	101	O 2C = K9	-110	6	12	4	104	W 4P -1 KK	50	88	7	6	109	O 4C = P3	-620	0
9	2	101	W 4P = TK	-620	75	13	4	103	S 5T = CA	600	81	8	6	109	W 3SA -3 CD	150	100
10	2	111	S 6C -1 PD	-100	0	14	4	103	N 2C +1 P4	140	75	9	6	109	W 4P +2 TK	-680	31
11	2	111	S 3SA -1 C10	-50	6	15	4	103	W 4C X -1 K2	100	100	16	6	106	O 3P +1 CD	-170	75
12	2	111	W 3P = T9	-140	56	16	4	102	W 4P = K4	-620	44	17	6	106	S 3C -1 PD	-50	44
13	2	110	S 4T +3 PD	190	44	17	4	102	S 3C = PD	140	94	18	6	106	N 6SA = K5	1440	62
14	2	110	W 1SA X : C4	-180	0	18	4	102	S 4C +3 K3	710	44	19	6	105	S 2P +1 P3	140	31
15	2	110	W 4C -1 K2	50	81	19	4	101	N 1SA +2 C4	150	69	20	6	105	N 6SA = PA	1440	69
16	2	109	W 4P = CD	-620	44	20	4	101	N 6SA = P6	1440	69	21	6	105	O 3SA +1 T8	-430	25
17	2	109	S 4C -2 PD	-100	6	21	4	101	O 3SA -1 T3	50	100	22	6	104	O 4C = TA	-620	75
18	2	109	S 3SA +3 K9	690	19	22	4	111	O 4C = K5	-620	75	23	6	104	O 2P -1 K6	100	75
19	2	108	N 1SA +1 C4	120	6	23	4	111	O 4T -2 C3	200	100	24	6	104	S 2SA +2 C2	180	50
20	2	108	S 3SA +3 CB	690	12	24	4	111	N 3SA +1 C3	430	69	25	6	103	N 1SA = C7	90	44
21	2	108	O 3SA = T3	-400	69	25	4	110	N 1SA -2 K7	-100	0	26	6	103	O 2C -1 P8	100	69
22	2	107	O 4C = K5	-620	75	26	4	110	W 3P +2 TK	-200	0	27	6	103	N 2P = K5	110	56
23	2	107	O 1SA +3 C3	-180	25	27	4	110	N 2P +1 TB	140	88	28	6	102	W 5K = PK	-400	25
24	2	107	S 3SA -1 C2	-50	31	28	4	109	W 3K +1 C6	-130	75	29	6	102	N 2P = K5	110	100
25	2	106	O 1SA = P8	-90	12	29	4	109	O 1SA = P6	-90	88	30	6	102	S 5K -1 P2	-50	25
26	2	106	W 2P +1 TK	-140	19	30	4	109	S 5K -1 C3	-50	25	31	6	101	N 4P = CA	620	100
27	2	106	N 2P = K4	110	56	31	4	108	N 3P = T9	140	38	32	6	101	N 1SA = C7	90	38
28	2	105	W 3K +1 PK	-130	75	32	4	108	S 2P = CB	110	50	33	6	101	O 1SA +2 P3	-150	12
29	2	105	N 3P -2 KK	-200	12	33	4	108	O 1SA = K5	-90	56	1	7	102	W 4C X -1 KA	100	75
30	2	105	S 4K X +2 C5	710	100	1	5	109	W 4C X = KA	-590	0	2	7	102	S 3SA +1 C3	630	56
7	3	103	O 3T = C5	-110	31	2	5	109	S 3SA +1 C2	630	56	3	7	102	N 3SA +2 C2	460	56

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
4	7	101	S 3T =	K4	110	94	5	9	105 S 3C +1	PA	170	44	6	11	109 N 4P +3	P3	510	44
5	7	101	S 4C =	PA	620	81	6	9	105 N 6P =	T7	980	94	7	11	108 O 4T -1	PA	100	56
6	7	101	N 4P +3	T7	510	44	7	9	104 W 4C -2	PB	200	88	8	11	108 W 3SA -1	CD	50	62
7	7	111	W 4C X -1	PB	200	88	8	9	104 S 1SA =	C7	90	88	9	11	108 W 4P +3	CD	-710	0
8	7	111	W 1SA =	C8	-90	31	9	9	104 O 3SA =	C10	-600	88	10	11	107 S 4C +3	K10	710	62
9	7	111	W 3SA +1	C6	-630	62	10	9	103 S 4C +1	PD	650	19	11	11	107 S 3SA -1	T5	-50	6
10	7	110	S 4C +1	PD	650	19	11	9	103 S 3SA +1	T5	430	94	12	11	107 W 4P -2	T9	100	100
11	7	110	S 2SA +1	C10	150	25	12	9	103 W 3P =	T9	-140	56	13	11	106 S 5T =	CA	600	81
12	7	110	W 4P +1	T9	-450	0	13	9	102 S 6T -1	CA	-100	0	14	11	106 N 2C +1	P2	140	75
19	7	107	N 1SA +2	C4	150	69	14	9	102 N 4C -1	P4	-50	12	15	11	106 N 3P -2	C4	-200	12
20	7	107	S 6C -1	K8	-100	0	15	9	102 W 3C =	K2	-140	56	16	11	105 W 4P =	T3	-620	44
21	7	107	W 3SA =	P3	-400	69	16	9	101 W 3P =	P8	-140	88	17	11	105 S 2C =	T6	110	75
22	7	106	O 4C =	K5	-620	75	17	9	101 S 3SA -1	T6	-50	44	18	11	105 S 4C +2	K3	680	0
23	7	106	O 3SA =	C10	-600	6	18	9	101 S 7C =	K2	2210	100	19	11	104 N 1SA +2	C4	150	69
24	7	106	N 3SA +2	C5	460	94	25	9	109 W 2P -2	TD	200	94	20	11	104 N 6SA =	PA	1440	69
25	7	105	W 2P -2	KD	200	94	26	9	109 O 2C =	P8	-110	38	21	11	104 O 3SA +1	T5	-430	25
26	7	105	W 4P -1	TK	100	69	27	9	109 N 3P -1	K2	-50	25	22	11	103 O 4C +1	K5	-650	19
27	7	105	N 2P -1	K2	-50	25	28	9	108 W 3SA +1	PK	-430	0	23	11	103 O 2SA +1	C10	-150	44
28	7	104	W 3SA -3	PK	150	100	29	9	108 N 3P -2	K5	-200	12	24	11	103		-200	0
29	7	104	W 3K =	PA	-110	38	30	9	108 S 5K -1	P9	-50	25	31	11	111 N 3P =	T9	140	38
30	7	104	S 5K -2	C3	-100	0	31	9	107 N 3P =	CA	140	38	32	11	111 N 1SA -1	C2	-50	19
31	7	103	N 4P -1	T9	-100	12	32	9	107 N 2T +2	CA	130	75	33	11	111 O 1SA -1	K5	50	75
32	7	103	N 2SA =	C7	120	62	33	9	107 W 1SA +1	C3	-120	38						
33	7	103	O 1SA +2	P3	-150	12	1	10	108 N 5T -2	CK	-100	25						
1	8	104	W 4C X -1	TA	100	75	2	10	108 S 3SA +2	C2	660	100						
2	8	104	S 3SA +1	C3	630	56	3	10	108 N 3SA +2	T9	460	56						
3	8	104	N 3SA +2	P8	460	56	4	10	107 S 2T -1	K4	-100	75						
4	8	103	O 2P +1	TA	-140	44	5	10	107 S 4C =	PA	620	81						
5	8	103	S 4C =	PA	620	81	6	10	107 N 4P +3	K6	510	44						
6	8	103	N 4P +3	C7	510	44	7	10	106 O 3SA -2	C5	200	88						
7	8	102	O 4T -1	C6	100	56	8	10	106 O 1P +1	CK	-110	6						
8	8	102	W 4C -1	T9	50	62	9	10	106 W 4P +1	TK	-650	50						
9	8	102	W 3P +3	TK	-230	100	10	10	105 N 3SA +4	T4	720	94						
10	8	101	S 4C +3	TD	710	62	11	10	105 S 3SA =	C10	400	56						
11	8	101	S 3SA =	T5	400	56	12	10	105 W 4P =	T9	-420	19						
12	8	101	W 3P =	T9	-140	56	13	10	104 S 4T +2	KB	170	25						
13	8	111	S 5T =	CA	600	81	14	10	104 O 1SA -1	C4	50	25						
14	8	111	N 2C +1	P2	140	75	15	10	104 N 3P -2	C4	-200	12						
15	8	111	W 3C -1	K2	50	81	16	10	103 O 4P +1	CD	-650	6						
22	8	108	O 4C +1	C2	-650	19	17	10	103 N 3SA -1	K2	-50	44						
23	8	108	O 3T -1	C10	100	75	18	10	103 S 4C +3	P4	710	44						
24	8	108	S 3SA +1	TK	430	69	19	10	102 N 1SA +1	C4	120	6						
25	8	107	N 1SA =	TA	90	44	20	10	102 N 6SA =	PA	1440	69						
26	8	107	N 3SA -1	CK	-100	50	21	10	102 O 3SA =	T3	-400	69						
27	8	107	N 2P +1	T7	140	88	28	10	110 W 5K +1	PK	-420	12						
28	8	106	N 2P X -1	TA	-200	38	29	10	110 N 3P -2	K5	-200	12						
29	8	106	N 2P -1	K5	-100	62	30	10	110 S 5K =	C5	400	62						
30	8	106	S 5K X =	C5	550	88	31	10	109 N 3P +1	T8	170	75						
31	8	105	N 3P +1	TA	170	75	32	10	109 O 2C +1	KA	-140	0						
32	8	105	S 2P +1	C3	140	94	33	10	109 O 1SA -2	P3	100	94						
33	8	105	O 1SA =	P3	-90	56	1	11	110 W 4C =	KA	-420	12						
1	9	106	W 4C X -1	TA	100	75	2	11	110 S 3SA =	K2	600	6						
2	9	106	S 3SA =	C3	600	6	3	11	110 N 3SA =	T9	400	12						
3	9	106	O 2P X -4	TA	1100	100	4	11	109 S 3T -2	K4	-200	0						
4	9	105	O 3P =	TA	-140	44	5	11	109 O 3T -1	KD	50	12						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
1	1	101	W 4C X -1 KA	-100	25	5	8	103	S 4C = PA	-620	19	6	9	105	N 6P = T7	-980	6
2	1	101	S 3SA +1 K2	-630	44	6	8	103	N 4P +3 C7	-510	56	10	10	105	N 3SA +4 T4	-720	6
3	1	101	S 3SA +1 T5	-430	75	7	3	103	O 3T = C5	110	69	11	10	105	S 3SA = C10	-400	44
4	7	101	S 3T = K4	-110	6	8	3	103	W 3SA -1 C8	-50	38	12	10	105	W 4P = T9	420	81
5	7	101	S 4C = PA	-620	19	9	3	103	W 4P +2 TK	680	69	13	5	105	S 5T = CA	-600	19
6	7	101	N 4P +3 T7	-510	56	10	9	103	S 4C +1 PD	-650	81	14	5	105	N 2C = TD	-110	62
7	2	101	S 3P -2 T6	200	88	11	9	103	S 3SA +1 T5	-430	6	15	5	105	W 3C +1 K2	170	62
8	2	101	O 2C = K9	110	94	12	9	103	W 3P = T9	140	44	16	11	105	W 4P = T3	620	56
9	2	101	W 4P = TK	620	25	13	4	103	S 5T = CA	-600	19	17	11	105	S 2C = T6	-110	25
10	8	101	S 4C +3 TD	-710	38	14	4	103	N 2C +1 P4	-140	25	18	11	105	S 4C +2 K3	-680	100
11	8	101	S 3SA = T5	-400	44	15	4	103	W 4C X -1 K2	-100	0	19	6	105	S 2P +1 P3	-140	69
12	8	101	W 3P = T9	140	44	16	10	103	O 4P +1 CD	650	94	20	6	105	N 6SA = PA	-1440	31
13	3	101	S 4T +1 CA	-150	88	17	10	103	N 3SA -1 K2	50	56	21	6	105	O 3SA +1 T8	430	75
14	3	101	N 2C +1 P2	-140	25	18	10	103	S 4C +3 P4	-710	56	22	1	105	O 4C +1 K5	650	81
15	3	101	W 3C = K2	140	44	19	5	103	O 2C -2 K8	-200	0	23	1	105	O 2SA +1 C10	150	56
16	9	101	W 3P = P8	140	12	20	5	103	N 3SA +4 P6	-720	75	24	1	105	S 3SA -1 C2	50	69
17	9	101	S 3SA -1 T6	50	56	21	5	103	O 3SA +1 T3	430	75	25	7	105	W 2P -2 KD	-200	6
18	9	101	S 7C = K2	-2210	0	22	11	103	O 4C +1 K5	650	81	26	7	105	W 4P -1 TK	-100	31
19	4	101	N 1SA +2 C4	-150	31	23	11	103	O 2SA +1 C10	150	56	27	7	105	N 2P -1 K2	50	75
20	4	101	N 6SA = P6	-1440	31	24	11	103		200	100	28	2	105	W 3K +1 PK	130	25
21	4	101	O 3SA -1 T3	-50	0	25	6	103	N 1SA = C7	-90	56	29	2	105	N 3P -2 KK	200	88
25	5	101	W 2P -1 KD	-100	31	26	6	103	O 2C -1 P8	-100	31	30	2	105	S 4K X +2 C5	-710	0
26	5	101	O 3C = P8	140	81	27	6	103	N 2P = K5	-110	44	31	8	105	N 3P +1 TA	-170	25
27	5	101	N 2P +1 CA	-140	12	31	7	103	N 4P -1 T9	100	88	32	8	105	S 2P +1 C3	-140	6
31	6	101	N 4P = CA	-620	0	32	7	103	N 2SA = C7	-120	38	33	8	105	O 1SA = P3	90	44
32	6	101	N 1SA = C7	-90	62	33	7	103	O 1SA +2 P3	150	88						
33	6	101	O 1SA +2 P3	150	88												
1	7	102	W 4C X -1 KA	-100	25	1	8	104	W 4C X -1 TA	-100	25	1	9	106	W 4C X -1 TA	-100	25
2	7	102	S 3SA +1 C3	-630	44	2	8	104	S 3SA +1 C3	-630	44	2	9	106	S 3SA = C3	-600	94
3	7	102	N 3SA +2 C2	-460	44	3	8	104	N 3SA +2 P8	-460	44	3	9	106	O 2P X -4 TA	-1100	0
4	2	102	S 3T = K4	-110	6	7	9	104	W 4C -2 PB	-200	12	7	10	106	O 3SA -2 C5	-200	12
5	2	102	S 4C = T7	-620	19	8	9	104	S 1SA = C7	-90	12	8	10	106	O 1P +1 CK	110	94
6	2	102	N 6P = K5	-980	6	9	9	104	O 3SA = C10	600	12	9	10	106	W 4P +1 TK	650	50
7	8	102	O 4T -1 C6	-100	44	10	4	104	S 4C +2 K10	-680	62	13	11	106	S 5T = CA	-600	19
8	8	102	W 4C -1 T9	-50	38	11	4	104	S 3SA = C10	-400	44	14	11	106	N 2C +1 P2	-140	25
9	8	102	W 3P +3 TK	230	0	12	4	104	W 4P -1 KK	-50	12	15	11	106	N 3P -2 C4	200	88
10	3	102	S 4C +3 T10	-710	38	13	10	104	S 4T +2 KB	-170	75	16	6	106	O 3P +1 CD	170	25
11	3	102	S 3SA +1 T5	-430	6	14	10	104	O 1SA -1 C4	-50	75	17	6	106	S 3C -1 PD	50	56
12	3	102	W 4P = T9	420	81	15	10	104	N 3P -2 C4	200	88	18	6	106	N 6SA = K5	-1440	38
13	9	102	S 6T -1 CA	100	100	16	5	104	W 4P +1 CD	650	94	19	1	106	S 2P +1 CB	-140	69
14	9	102	N 4C -1 P4	50	88	17	5	104	N 3SA -1 T3	50	56	20	1	106	N 6SA = PA	-1440	31
15	9	102	W 3C = K2	140	44	18	5	104	N 3SA +3 K5	-690	81	21	1	106	O 3SA +2 P4	460	100
16	4	102	W 4P = K4	620	56	19	11	104	N 1SA +2 C4	-150	31	22	7	106	O 4C = K5	620	25
17	4	102	S 3C = PD	-140	6	20	11	104	N 6SA = PA	-1440	31	23	7	106	O 3SA = C10	600	94
18	4	102	S 4C +3 K3	-710	56	21	11	104	O 3SA +1 T5	430	75	24	7	106	N 3SA +2 C5	-460	6
19	10	102	N 1SA +1 C4	-120	94	22	6	104	O 4C = TA	620	25	25	2	106	O 1SA = P8	90	88
20	10	102	N 6SA = PA	-1440	31	23	6	104	O 2P -1 K6	-100	25	26	2	106	W 2P +1 TK	140	81
21	10	102	O 3SA = T3	400	31	24	6	104	S 2SA +2 C2	-180	50	27	2	106	N 2P = K4	-110	44
22	5	102	O 4C +1 K5	650	81	25	1	104	N 1SA -1 K2	50	75	28	8	106	N 2P X -1 TA	200	62
23	5	102	O 3SA -1 C10	-100	25	26	1	104	S 5T = C6	-600	0	29	8	106	N 2P -1 K5	100	38
24	5	102	S 3T -3 C2	150	88	27	1	104	N 4P -2 K2	100	100	30	8	106	S 5K X = C5	-550	12
28	6	102	W 5K = PK	400	75	28	7	104	W 3SA -3 PK	-150	0	31	3	106	S 3P +1 T9	-170	25
29	6	102	N 2P = K5	-110	0	29	7	104	W 3K = PA	110	62	32	3	106	S 2P +1 KB	-140	6
30	6	102	S 5K -1 P2	50	75	30	7	104	S 5K -2 C3	100	100	33	3	106	O 1SA -2 P3	-100	6
4	8	103	O 2P +1 TA	140	56	4	9	105	O 3P = TA	140	56						
						5	9	105	S 3C +1 PA	-170	56	1	4	107	N 4T -1 CK	50	62
												2	4	107	N 3SA +1 K8	-630	44
												3	4	107	S 3SA +3 T5	-490	12

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

OW-Resultate Mitchell-Turnier Donnerstag - Mensa, Pfäffikon - 21.05.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
4	10	107	S 2T -1	K4	100	25	5	11	109	O 3T -1	KD	-50	88	6	1	111	N 5P +1	K5	-480	94
5	10	107	S 4C =	PA	-620	19	6	11	109	N 4P +3	P3	-510	56	7	7	111	W 4C X -1	PB	-200	12
6	10	107	N 4P +3	K6	-510	56	7	6	109	O 4C =	P3	620	100	8	7	111	W 1SA =	C8	90	69
10	11	107	S 4C +3	K10	-710	38	8	6	109	W 3SA -3	CD	-150	0	9	7	111	W 3SA +1	C6	630	38
11	11	107	S 3SA -1	T5	50	94	9	6	109	W 4P +2	TK	680	69	10	2	111	S 6C -1	PD	100	100
12	11	107	W 4P -2	T9	-100	0	10	1	109	N 3SA +4	T2	-720	6	11	2	111	S 3SA -1	C10	50	94
16	1	107	W 4P -1	CD	-100	0	11	1	109	S 3SA =	T5	-400	44	12	2	111	W 3P =	T9	140	44
17	1	107	S 3C =	T9	-140	6	12	1	109	W 3P =	T9	140	44	13	8	111	S 5T =	CA	-600	19
18	1	107	S 6C +1	K9	-1460	19	16	2	109	W 4P =	CD	620	56	14	8	111	N 2C +1	P2	-140	25
19	7	107	N 1SA +2	C4	-150	31	17	2	109	S 4C -2	PD	100	94	15	8	111	W 3C -1	K2	-50	19
20	7	107	S 6C -1	K8	100	100	18	2	109	S 3SA +3	K9	-690	81	16	3	111	W 4P =	CD	620	56
21	7	107	W 3SA =	P3	400	31	22	3	109	O 4C =	P4	620	25	17	3	111	S 4C -2	T6	100	94
22	2	107	O 4C =	K5	620	25	23	3	109	O 3SA =	C10	600	94	18	3	111	N 6C +1	K5	-1460	19
23	2	107	O 1SA +3	C3	180	75	24	3	109	S 3SA +2	C2	-460	6	22	4	111	O 4C =	K5	620	25
24	2	107	S 3SA -1	C2	50	69	25	9	109	W 2P -2	TD	-200	6	23	4	111	O 4T -2	C3	-200	0
25	8	107	N 1SA =	TA	-90	56	26	9	109	O 2C =	P8	110	62	24	4	111	N 3SA +1	C3	-430	31
26	8	107	N 3SA -1	CK	100	50	27	9	109	N 3P -1	K2	50	75	28	5	111	O 2SA +2	CA	180	50
27	8	107	N 2P +1	T7	-140	12	28	4	109	W 3K +1	C6	130	25	29	5	111	N 2P -1	KK	100	38
28	3	107	W 2K +2	C6	130	25	29	4	109	O 1SA =	P6	90	12	30	5	111	W 4C -3	PA	-150	50
29	3	107	N 2P -1	K5	100	38	30	4	109	S 5K -1	C3	50	75	31	11	111	N 3P =	T9	-140	62
30	3	107	S 5K +1	TA	-420	25	31	10	109	N 3P +1	T8	-170	25	32	11	111	N 1SA -1	C2	50	81
31	9	107	N 3P =	CA	-140	62	32	10	109	O 2C +1	KA	140	100	33	11	111	O 1SA -1	K5	-50	25
32	9	107	N 2T +2	CA	-130	25	33	10	109	O 1SA -2	P3	-100	6							
33	9	107	W 1SA +1	C3	120	62														
1	10	108	N 5T -2	CK	100	75	1	11	110	W 4C =	KA	420	88							
2	10	108	S 3SA +2	C2	-660	0	2	11	110	S 3SA =	K2	-600	94							
3	10	108	N 3SA +2	T9	-460	44	3	11	110	N 3SA =	T9	-400	88							
4	5	108	O 2P +2	TA	170	88	4	6	110	O 2P +1	TA	140	56							
5	5	108	S 3C =	K6	-140	75	5	6	110	S 4C -1	K6	100	100							
6	5	108	N 4P +2	T7	-480	94	6	6	110	N 3SA +4	K5	-520	25							
7	11	108	O 4T -1	PA	-100	44	7	1	110	O 3T =	C5	110	69							
8	11	108	W 3SA -1	CD	-50	38	8	1	110	W 1SA =	CD	90	69							
9	11	108	W 4P +3	CD	710	100	9	1	110	O 3SA +3	T4	690	88							
13	1	108	S 3T +4	KB	-190	56	10	7	110	S 4C +1	PD	-650	81							
14	1	108	N 3C =	TD	-140	25	11	7	110	S 2SA +1	C10	-150	75							
15	1	108	N 5P -2	C4	200	88	12	7	110	W 4P +1	T9	450	100							
19	2	108	N 1SA +1	C4	-120	94	13	2	110	S 4T +3	PD	-190	56							
20	2	108	S 3SA +3	CB	-690	88	14	2	110	W 1SA X :	C4	180	100							
21	2	108	O 3SA =	T3	400	31	15	2	110	W 4C -1	K2	-50	19							
22	8	108	O 4C +1	C2	650	81	19	3	110	N 1SA +2	C4	-150	31							
23	8	108	O 3T -1	C10	-100	25	20	3	110	N 6SA =	T5	-1440	31							
24	8	108	S 3SA +1	TK	-430	31	21	3	110	W 3SA =	T4	400	31							
25	3	108	W 2P -1	KD	-100	31	25	4	110	N 1SA -2	K7	100	100							
26	3	108	O 2C -2	P8	-200	12	26	4	110	W 3P +2	TK	200	100							
27	3	108	N 3P -1	TB	50	75	27	4	110	N 2P +1	TB	-140	12							
28	9	108	W 3SA +1	PK	430	100	28	10	110	W 5K +1	PK	420	88							
29	9	108	N 3P -2	K5	200	88	29	10	110	N 3P -2	K5	200	88							
30	9	108	S 5K -1	P9	50	75	30	10	110	S 5K =	C5	-400	38							
31	4	108	N 3P =	T9	-140	62	31	5	110	W 2C +1	P5	140	100							
32	4	108	S 2P =	CB	-110	50	32	5	110	S 3P -1	C3	50	81							
33	4	108	O 1SA =	K5	90	44	33	5	110	O 1SA +2	PA	150	88							
1	5	109	W 4C X =	KA	590	100	1	6	111	W 4C X -1	TA	-100	25							
2	5	109	S 3SA +1	C2	-630	44	2	6	111	S 3SA +1	P10	-630	44							
3	5	109	N 4P -2	T9	100	100	3	6	111	N 3SA +2	C2	-460	44							
4	11	109	S 3T -2	K4	200	100	4	1	111	W 3P =	TD	140	56							
							5	1	111	S 3C +1	PA	-170	56							

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.