

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Mensa, Pfäffikon - 19.05.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	6	111	S 3SA -2	C4	-100	5	6	11	106 W 3SA +1	T6	-630	0	11	2	111 N 3SA -1	C3	-50	0
1	4	107	S 3SA -2	C9	-100	5	6	2	101 O 4C =	PA	-620	15	11	5	104 S 2P =	T10	110	10
1	12	110	W 1SA =	TB	-90	20	6	8	113 O 4C =	PA	-620	15	11	3	113 N 3SA +1	P6	430	25
1	1	101	S 3SA -1	C3	-50	45	6	3	103 W 2SA +3	T6	-210	30	11	12	105 N 3SA +1	P8	430	25
1	11	108	S 3K -1	C3	-50	45	6	13	110 W 3K =	P7	-110	40	11	6	106 S 3SA +3	T8	490	70
1	8	102	S 2SA -1	PK	-50	45	6	10	104 S 3P -2	CA	-100	55	11	4	102 N 3SA +3	CD	490	70
1	5	109	S 3K -1	PK	-50	45	6	9	102 S 3P -2	CA	-100	55	11	1	109 N 3SA +3	P6	490	70
1	13	112	N 2SA +1	P2	150	80	6	1	112 W 3SA -1	P6	100	85	11	13	107 N 3SA +3	C4	490	70
1	10	106	S 2SA +1	C5	150	80	6	12	108 W 3T -1	P6	100	85	11	11	103 N 3SA +3	P6	490	70
1	9	104	S 2SA +1	C3	150	80	6	7	111 O 4C -1	T9	100	85	11	10	101 S 3SA +3	K3	490	70
1	7	113	S 3SA =	C5	400	100	6	6	109 O 4C -1	T9	100	85	11	9	112 N 3SA +3	P2	490	70
2	11	108	N 4P -2	TA	-200	5	7	9	101 S 4C -2	T9	-200	0	12	11	103 S 5C -1	PA	-100	0
2	9	104	N 2K -2	C9	-200	5	7	2	113 S 4P -1	K3	-100	10	12	13	107 W 4P -1	KA	50	15
2	1	101	O 2T +2	P2	-130	20	7	3	102 S 2P =	C9	110	20	12	10	101 W 4P -1	KA	50	15
2	7	113	N 3P -1	TA	-100	30	7	12	107 S 3P =	T9	140	45	12	6	106 W 4P -2	KA	100	60
2	4	107	O 1SA =	P2	-90	40	7	11	105 S 2P +1	K3	140	45	12	5	104 W 3P -2	KA	100	60
2	8	102	O 3K -4	P2	0	50	7	10	103 S 2P +1	C5	140	45	12	4	102 W 4P -2	KA	100	60
2	13	112	O 2SA -1	P6	50	65	7	7	110 S 2P +1	K10	140	45	12	3	113 W 5P -2	KA	100	60
2	5	109	O 3SA -1	P6	50	65	7	4	104 S 2P +2	T9	170	80	12	2	111 W 4P -2	KA	100	60
2	10	106	S 2P =	T4	110	80	7	1	111 S 2P +2	T9	170	80	12	1	109 W 4P -2	KA	100	60
2	12	110	N 2SA +1	C10	150	95	7	8	112 S 2P +2	K5	170	80	12	12	105 W 4P -2	KA	100	60
2	6	111	O 2SA -3	P8	150	95	7	13	109 S 4P =	C9	620	100	12	9	112 N 5C X +1	PA	1050	100
3	12	109	N 4C -2	P7	-100	0	8	4	104 N 4C -1	P6	-50	5	13	5	103 S 4P X -3	CK	-800	0
3	2	102	N 3SA -1	P10	-50	10	8	10	103 N 3C -1	T3	-50	5	13	7	107 S 2P +1	TK	140	35
3	7	112	N 2C =	P8	110	20	8	12	107 W 2K -1	PK	50	20	13	6	105 S 2P +1	CK	140	35
3	1	113	N 3C +2	P10	200	30	8	3	102 S 2P =	K5	110	40	13	3	112 S 3P =	TB	140	35
3	5	108	O 2P -4	TA	400	40	8	2	113 N 2C =	T3	110	40	13	1	108 S 2P +1	TK	140	35
3	13	111	N 4C =	KA	420	60	8	1	111 N 2C =	TA	110	40	13	13	106 S 2P +1	TK	140	35
3	11	107	N 4C =	P7	420	60	8	13	109 N 1SA +1	T3	120	60	13	11	102 S 2P +1	TK	140	35
3	8	101	N 4C =	P10	420	60	8	11	105 N 3C =	TA	140	85	13	12	104 S 3P +1	TK	170	75
3	10	105	N 4C +1	P8	450	90	8	9	101 N 2C +1	P2	140	85	13	10	113 S 2P +2	CK	170	75
3	9	103	N 4C +1	P10	450	90	8	8	112 N 3C =	K4	140	85	13	4	101 W 3T -2	P7	200	95
3	6	110	N 4C +1	P10	450	90	8	7	110 N 2C +1	T3	140	85	13	2	110 W 4T X -1	P10	200	95
4	11	107	O 5K =	PA	-600	0	9	3	101 S 4C -2	K3	-100	0	14	4	101 W 6SA +1	PD	-1020	10
4	7	112	S 4P X -2	K5	-500	10	9	4	103 S 1SA -1	P2	-50	10	14	1	108 W 6SA +1	T2	-1020	10
4	2	102	O 4K =	PA	-130	25	9	8	111 S 2C =	K4	110	20	14	13	106 W 6SA +1	PD	-1020	10
4	5	108	O 2T +2	PA	-130	25	9	5	105 S 2C +1	K3	140	55	14	11	102 O 6K +1	T5	-940	35
4	13	111	O 2T +1	C4	-110	40	9	2	112 N 2C +1	T3	140	55	14	10	113 O 6K +1	K9	-940	35
4	8	101	S 3P -1	K5	-100	50	9	13	108 N 2C +1	K2	140	55	14	6	105 O 3SA +4	C2	-520	60
4	1	113	O 4T -1	PA	100	60	9	12	106 S 3C =	K3	140	55	14	3	112 O 3SA +4	T9	-520	60
4	6	110	S 3P =	K4	140	70	9	10	102 S 3C =	KB	140	55	14	2	110 O 3SA +4	T3	-520	60
4	10	105	S 3P +1	K5	170	80	9	9	113 S 3C =	K3	140	55	14	12	104 W 4SA +1	PD	-460	80
4	12	109	W 3SA -3	P3	300	95	9	1	110 N 3C +1	PD	170	90	14	7	107 W 3SA +1	PD	-430	90
4	9	103	W 3SA -3	P3	300	95	9	11	104 S 4C =	TD	420	100	14	5	103 W 7SA -2	P10	100	100
5	3	103	W 4C =	PK	-420	0	10	5	105 O 4P +1	KA	-650	25	15	3	111 S 3SA -2	C9	-200	0
5	13	110	S 2P -2	C4	-200	15	10	3	101 O 4P +1	K4	-650	25	15	5	102 O 4C -4	TA	200	10
5	11	106	S 2P -2	K6	-200	15	10	13	108 O 4P +1	C6	-650	25	15	8	108 S 3SA =	C9	600	35
5	2	101	W 2C +1	PK	-140	35	10	11	104 O 4P +1	T6	-650	25	15	6	104 S 3SA =	C9	600	35
5	7	111	O 2C +1	K9	-140	35	10	10	102 O 4P +1	C6	-650	25	15	4	113 S 3SA =	C8	600	35
5	1	112	O 1SA +1	P2	-120	50	10	8	111 O 4P +1	C9	-650	25	15	2	109 S 3SA =	C9	600	35
5	12	108	N 2SA -1	K7	-100	60	10	4	103 O 4P =	KA	-620	65	15	13	105 S 3SA +1	C3	630	65
5	10	104	O 2K -1	CA	50	75	10	2	112 O 4P =	C6	-620	65	15	12	103 N 3SA +1	CD	630	65
5	9	102	W 2K -1	CA	50	75	10	9	113 O 3P +1	CB	-170	80	15	7	106 S 3SA +2	C5	660	85
5	8	113	O 3K -2	CA	100	90	10	1	110 O 4P -1	T9	100	95	15	1	107 S 3SA +2	C9	660	85
5	6	109	N 2SA +2	TA	180	100	10	12	106 O 4P -1	C6	100	95	15	11	101 S 3SA +3	C3	690	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	1	107	W 3SA =	C7	-600	0	21	11	111 S 4C -1	K8	-100	5	26	11	109 S 6C -3	K2	-300	0
16	11	101	W 2P +2	CB	-170	10	21	5	112 S 4C -1	K9	-100	5	26	9	105 S 4C -1	KD	-100	20
16	3	111	W 2P +1	C5	-140	25	21	6	101 O 2P -1	TB	50	25	26	5	110 S 4C -1	K10	-100	20
16	13	105	W 2P +1	C5	-140	25	21	4	110 O 3P -1	CA	50	25	26	4	108 S 4C -1	KD	-100	20
16	8	108	W 2P =	CB	-110	60	21	2	106 O 3P -3	TB	150	40	26	13	113 N 4C =	T7	620	65
16	7	106	W 2P =	C6	-110	60	21	3	108 N 3C +1	PA	170	50	26	12	111 N 4C =	P4	620	65
16	5	102	W 2P =	T2	-110	60	21	8	105 O 4P X -2	CA	300	65	26	10	107 S 4C =	KD	620	65
16	4	113	W 2P =	C5	-110	60	21	7	103 O 3P X -2	CA	300	65	26	8	103 S 4C =	KD	620	65
16	2	109	W 2P =	CB	-110	60	21	10	109 S 4C =	PB	620	85	26	7	101 S 4C =	KD	620	65
16	6	104	W 1SA =	CB	-90	95	21	1	104 S 4C =	KD	620	85	26	6	112 S 4C =	K10	620	65
16	12	103	W 1SA =	CB	-90	95	21	9	107 S 4C +1	TA	650	100	26	3	106 S 3SA +1	KD	630	100
17	8	107	O 3SA +2	K7	-460	15	22	3	108 N 2SA -3	TA	-150	0						
17	7	105	W 3SA +2	C6	-460	15	22	5	112 O 3K +1	T9	-130	15						
17	5	101	W 3SA +2	C6	-460	15	22	2	106 O 2K +2	T4	-130	15						
17	2	108	O 3SA +2	C8	-460	15	22	10	109 O 1SA +1	T4	-120	35						
17	6	103	O 3SA +1	K7	-430	50	22	9	107 O 1SA +1	T2	-120	35						
17	1	106	W 3SA +1	C6	-430	50	22	11	111 O 2K +1	T2	-110	60						
17	12	102	O 3SA +1	K8	-430	50	22	6	101 O 3K =	T4	-110	60						
17	3	110	O 2SA +2	K2	-180	70	22	4	110 W 3K =	T5	-110	60						
17	4	112	O 3T +2	KD	-150	80	22	7	103 S 1SA -1	C4	-50	80						
17	13	104	W 2P +1	TA	-140	90	22	1	104 S 1SA =	T6	90	90						
17	9	109	W 2P =	TA	-110	100	22	8	105 O 3T -4	P2	400	100						
18	9	109	S 2SA -2	P5	-200	5	23	6	113 O 3T X =	C9	-670	0						
18	7	105	S 3SA -2	C10	-200	5	23	10	108 O 2T +2	C9	-130	10						
18	8	107	S 2SA -1	C10	-100	40	23	7	102 O 2T +1	C9	-110	25						
18	6	103	N 5K -1	P4	-100	40	23	5	111 O 2T +1	C9	-110	25						
18	5	101	S 1SA -1	C10	-100	40	23	8	104 O 2T =	C9	-90	45						
18	4	112	N 3SA -1	K10	-100	40	23	2	105 O 2T =	C9	-90	45						
18	3	110	N 2SA -1	C2	-100	40	23	12	112 O 3T -1	C5	100	70						
18	12	102	O 1C -1	KA	50	70	23	4	109 O 3T -1	C9	100	70						
18	2	108	N 4K =	P4	130	85	23	3	107 O 2T -1	C9	100	70						
18	13	104	N 2K +2	C9	130	85	23	11	110 O 3T X -1	C3	200	90						
18	1	106	N 1SA +2	C6	150	100	23	9	106 W 2K -3	P5	300	100						
19	9	108	N 1SA -1	PB	-50	5	24	5	111 N 5K -1	T8	-50	0						
19	3	109	N 2K -1	C2	-50	5	24	12	112 N 3K +2	C3	150	25						
19	10	110	N 1SA =	P4	90	45	24	10	108 N 3K +2	CK	150	25						
19	8	106	N 1SA =	P4	90	45	24	4	109 N 3K +2	CK	150	25						
19	6	102	N 1SA =	PB	90	45	24	2	105 N 2K +3	CK	150	25						
19	4	111	N 2K =	PA	90	45	24	8	104 N 5K =	T7	400	60						
19	1	105	N 1SA =	P4	90	45	24	6	113 N 5K =	CK	400	60						
19	13	103	N 1SA =	P4	90	45	24	3	107 N 5K =	PD	400	60						
19	5	113	S 2K +1	P4	110	80	24	11	110 N 3SA +1	CK	430	90						
19	2	107	N 1SA +1	TB	120	90	24	9	106 N 3SA +1	T5	430	90						
19	7	104	W 3T -2	KA	200	100	24	7	102 N 3SA +1	T3	430	90						
20	13	103	W 3SA +1	T3	-630	0	25	13	113 O 4C +1	T2	-650	0						
20	5	113	O 4K =	P7	-130	10	25	3	106 S 3K X -2	TA	-300	10						
20	10	110	O 2K +1	CB	-110	20	25	7	101 O 2SA +2	K10	-180	20						
20	7	104	O 2K =	C5	-90	30	25	8	103 O 2SA +1	K10	-150	30						
20	9	108	W 3SA -1	T5	100	55	25	4	108 W 3T +1	KK	-130	40						
20	8	106	W 3SA -1	P10	100	55	25	10	107 W 2T +1	K2	-110	50						
20	4	111	W 3SA -1	P2	100	55	25	12	111 S 1SA -2	T7	-100	70						
20	1	105	O 3K -1	CB	100	55	25	9	105 S 2K -2	TA	-100	70						
20	3	109	O 3T -2	K8	200	85	25	5	110 S 2K -2	T4	-100	70						
20	2	107	O 3SA -2	TA	200	85	25	6	112 W 2T =	K2	-90	90						
20	6	102	W 3SA -4	T3	400	100	25	11	109 W 4C -2	P2	200	100						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.