

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 05.05.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	7	113	S 4P -3	CA	-150	0	6	2	101 O 1P -1	CK	100	56	12	11	103 O 4P =	KA	-420	0
1	8	102	N 1SA -2	T4	-100	11	6	1	112 W 1SA -1	T3	100	56	12	9	112 N 3C -4	T6	-400	11
1	1	101	N 1SA -1	T3	-50	28	6	9	102 N 2C =	KA	110	78	12	6	106 O 3P +1	KA	-170	39
1	4	107	N 1SA -1	T4	-50	28	6	10	104 S 1SA +3	T10	180	89	12	5	104 O 3P +1	KA	-170	39
1	12	110	N 2P =	T3	110	67	6	11	106 O 2P -2	CK	200	100	12	3	113 O 3P +1	KA	-170	39
1	10	106	S 2P =	CA	110	67	7	3	102 S 4C -2	K7	-200	0	12	2	111 O 3P +1	K6	-170	39
1	9	104	N 2P =	T4	110	67	7	12	107 O 3K +1	T4	-130	11	12	4	102 O 3P =	KA	-140	78
1	6	111	N 2P =	TD	110	67	7	9	101 O 3K =	T4	-110	28	12	1	109 O 2P +1	K2	-140	78
1	5	109	S 2P =	CA	110	67	7	8	112 O 3K =	CA	-110	28	12	12	105 O 3P =	KA	-140	78
1	11	108	N 2P +1	TD	140	100	7	1	111 W 4T -1	C5	100	44	12	10	101 S 3T -1	PA	-100	100
2	4	107	S 2P +3	CK	200	0	7	4	104 S 3C +1	K7	170	67	13	3	112 N 2P -2	C5	-200	17
2	7	113	S 3SA =	K7	600	11	7	11	105 S 3C +1	K7	170	67	13	1	108 S 2SA -2	P4	-200	17
2	5	109	S 4P =	T4	620	22	7	10	103 S 3C +1	PA	170	67	13	12	104 N 3C -2	K4	-200	17
2	1	101	S 4P +1	P6	650	61	7	7	110 S 4C =	P6	620	89	13	10	113 S 2SA -2	K7	-200	17
2	11	108	S 4P +1	K10	650	61	7	2	113 S 4C +1	PA	650	100	13	7	107 O 3K +1	TA	-130	44
2	10	106	S 4P +1	K7	650	61	8	1	111 W 1SA +1	C2	-120	0	13	6	105 O 3K =	P9	-110	61
2	9	104	N 4P +1	K7	650	61	8	4	104 O 2K +1	P10	-110	39	13	4	101 O 3K =	P9	-110	61
2	8	102	S 4P +1	CK	650	61	8	3	102 W 2P =	CA	-110	39	13	5	103 N 2P -1	K4	-100	89
2	6	111	S 4P +1	K9	650	61	8	2	113 O 2K +1	T5	-110	39	13	2	110 N 2P -1	K4	-100	89
2	12	110	S 4SA +1	CK	660	100	8	12	107 O 3K =	TA	-110	39	13	11	102 S 3T -1	CA	-100	89
3	2	102	O 4C +3	KD	-710	33	8	10	103 O 3K =	C2	-110	39	14	11	102 O 2P +3	CB	-200	6
3	1	113	O 4C +3	T6	-710	33	8	8	112 O 3K =	C2	-110	39	14	10	113 O 2P +3	T3	-200	6
3	12	109	O 4C +3	T5	-710	33	8	9	101 S 3C -2	PA	-100	83	14	7	107 O 2P +2	T9	-170	39
3	10	105	O 4C +3	T5	-710	33	8	7	110 S 3C -2	PA	-100	83	14	4	101 O 2P +2	CB	-170	39
3	8	101	O 4C +3	T5	-710	33	8	11	105 N 2C -1	P6	-50	100	14	1	108 O 3P +1	T9	-170	39
3	7	112	O 4C +3	T6	-710	33	9	3	101 N 2K -2	TA	-100	0	14	12	104 O 2P +2	T7	-170	39
3	6	110	O 4C +3	K7	-710	33	9	9	113 O 1SA =	P4	-90	11	14	6	105 W 3P =	T2	-140	78
3	11	107	O 4C +2	P10	-680	78	9	4	103 S 2P -1	CB	-50	22	14	3	112 O 2P +1	K10	-140	78
3	9	103	W 2C +5	K3	-260	89	9	12	106 S 1P =	C6	80	33	14	2	110 O 2P +1	CB	-140	78
3	5	108	W 3C +3	PK	-230	100	9	2	112 N 2K =	C2	90	50	14	5	103 O 3SA -1	CB	50	100
4	8	101	W 4P X =	C10	-790	6	9	8	111 N 2K =	C2	90	50	15	5	102 S 6C -2	K6	-200	6
4	5	108	W 4P X =	K5	-790	6	9	1	110 O 2T -1	K4	100	67	15	4	113 S 6C -2	K6	-200	6
4	1	113	W 4P =	K9	-620	39	9	11	104 S 1SA +1	P6	120	83	15	12	103 S 4C =	K6	620	22
4	12	109	W 4P =	T6	-620	39	9	10	102 N 1SA +1	TA	120	83	15	7	106 S 4C +1	K6	650	56
4	11	107	W 4P =	K10	-620	39	9	5	105 N 1SA +3	TB	180	100	15	6	104 N 4C +1	K6	650	56
4	7	112	W 4P =	C10	-620	39	10	11	104 S 3SA -2	C9	-200	0	15	3	111 S 4C +1	K6	650	56
4	9	103	W 3P =	K10	-140	67	10	3	101 N 2P +1	K9	140	11	15	2	109 S 4C +1	K6	650	56
4	10	105	W 5P -1	K10	100	83	10	2	112 N 3P +3	K9	230	22	15	1	107 S 4C +1	K6	650	56
4	6	110	W 4P -1	K10	100	83	10	5	105 N 4P +1	K3	650	50	15	8	108 N 3SA +2	K10	660	89
4	2	102	W 5P X -1	T2	200	100	10	4	103 N 4P +1	CA	650	50	15	11	101 O 5K X -6	CA	1400	100
5	3	103	W 1P =	TA	-80	0	10	12	106 N 4P +1	CA	650	50	16	1	107 W 3K X +'	C7	-870	0
5	1	112	Pass		0	33	10	8	111 N 4P +1	CA	650	50	16	3	111 N 4C X -4	KD	-800	11
5	12	108	Pass		0	33	10	1	110 N 4P +2	K9	680	89	16	5	102 N 3C X -3	KD	-500	22
5	11	106	Pass		0	33	10	10	102 N 4P +2	K4	680	89	16	8	108 S 2SA -3	K2	-150	39
5	10	104	Pass		0	33	10	9	113 N 4P +2	K4	680	89	16	4	113 N 3C -3	KD	-150	39
5	8	113	Pass		0	33	11	3	113 N 3SA +1	P7	430	11	16	11	101 W 3K +1	CK	-130	56
5	7	111	W 2P -1	TA	50	67	11	2	111 N 3SA +1	P7	430	11	16	12	103 W 2C =	T3	-110	67
5	9	102	W 2P -2	TA	100	83	11	9	112 N 3SA +1	P7	430	11	16	7	106 S 2SA -2	KA	-100	83
5	6	109	O 1SA -2	K6	100	83	11	5	104 N 4C +1	K8	450	44	16	2	109 N 2C -2	KD	-100	83
5	2	101	W 4P -3	KB	150	100	11	11	103 N 4C +1	K8	450	44	16	6	104 W 2SA -3	C7	300	100
6	7	111	W 1SA =	C8	-90	0	11	10	101 N 4C +1	K8	450	44	17	2	108 O 4P =	K8	-420	0
6	12	108	W 1C =	TA	-80	11	11	6	106 N 3SA +3	P5	490	78	17	9	109 O 4P -1	T7	50	28
6	8	113	N 2C -1	KA	-50	28	11	4	102 N 3SA +3	P7	490	78	17	8	107 O 4P -1	CA	50	28
6	6	109	N 3T -1	KA	-50	28	11	1	109 N 3SA +3	P10	490	78	17	7	105 O 4P -1	CA	50	28
6	3	103	O 2P -1	CK	100	56	11	12	105 O 4P X -3	KA	500	100	17	5	101 O 4P -1	K2	50	28

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OWASpKonErgAus	Sco	Prz		
17	4	112	O 4P -2	T7	100	72	22	2	106 S 3P +2	TA	200	75
17	3	110	O 4P -2	K2	100	72	22	1	104 S 5K =	T9	400	100
17	1	106	O 4P -2	K2	100	72	23	12	112 S 2C -3	TD	-300	0
17	12	102	O 4P -2	C4	100	72	23	5	111 W 2SA +1	TA	-150	10
17	6	103	W 3SA -3	K3	150	100	23	9	106 W 2SA =	K4	-120	35
18	7	105	O 4C =	PA	-420	0	23	8	104 W 2SA =	TA	-120	35
18	8	107	O 5T =	K7	-400	22	23	3	107 W 2SA =	T3	-120	35
18	5	101	O 5T =	PA	-400	22	23	2	105 W 2SA =	K4	-120	35
18	1	106	W 3SA =	KB	-400	22	23	4	109 O 2C =	T5	-110	60
18	3	110	O 2C +1	TB	-140	50	23	10	108 S 1P =	T3	80	70
18	2	108	O 3C =	K8	-140	50	23	11	110 W 2SA -1	TA	100	85
18	12	102	W 3SA -1	PD	50	67	23	6	113 W 2SA -1	K4	100	85
18	9	109	N 2K =	TA	90	78	23	7	102 O 2P -3	C10	300	100
18	6	103	O 5T X -1	K8	100	89	24	10	108 O 3P =	CK	-140	5
18	4	112	W 3SA -3	P3	150	100	24	6	113 O 3P =	K4	-140	5
19	9	108	S 2C -4	P9	-200	6	24	11	110 S 4C -2	P6	-100	25
19	4	111	S 1C -4	P9	-200	6	24	7	102 S 4C -2	P7	-100	25
19	5	113	W 1SA +1	T10	-120	28	24	12	112 S 4C -1	P7	-50	55
19	1	105	W 1SA +1	T8	-120	28	24	9	106 S 4C -1	P6	-50	55
19	10	110	O 2C =	TA	-110	50	24	8	104 S 4C -1	C4	-50	55
19	8	106	W 2C =	K3	-110	50	24	4	109 S 4C -1	T5	-50	55
19	6	102	S 1SA -1	P9	-50	67	24	5	111 O 4P -1	CK	50	90
19	3	109	W 2T -1	C6	100	83	24	3	107 O 4P -1	K4	50	90
19	2	107	W 3C -1	PA	100	83	24	2	105 O 4P -1	TA	50	90
19	7	104	W 2C -2	T10	200	100	25	6	112 O 4P +2	T9	-680	6
20	2	107	S 4P -2	K4	-200	0	25	5	110 O 4P +2	TB	-680	6
20	9	108	S 2P -1	T10	-100	28	25	12	111 O 4P +1	T7	-650	33
20	5	113	S 2P -1	T10	-100	28	25	7	101 O 4P +1	CA	-650	33
20	3	109	N 2SA -1	TD	-100	28	25	3	106 O 4P +1	C4	-650	33
20	1	105	S 2P -1	T10	-100	28	25	9	105 O 3SA +1	TB	-630	56
20	10	110	O 1SA -1	PK	100	56	25	11	109 O 4P =	TB	-620	78
20	6	102	S 2P =	K5	110	67	25	10	107 O 4P =	TB	-620	78
20	4	111	S 3P =	K5	140	78	25	4	108 O 4P =	TB	-620	78
20	8	106	S 2P +2	K4	170	94	25	8	103 O 2P +1	TB	-140	100
20	7	104	S 2P +2	K4	170	94	26	10	107 S 4K -1	P10	-100	6
21	10	109	O 2P +1	KK	-140	20	26	7	101 S 3K -1	P10	-100	6
21	9	107	O 2P +1	KK	-140	20	26	9	105 W 3P -1	CA	100	33
21	7	103	O 2P +1	KK	-140	20	26	5	110 W 3P -1	CA	100	33
21	3	108	O 2P +1	K3	-140	20	26	3	106 W 3P -1	CK	100	33
21	2	106	O 2P +1	KK	-140	20	26	12	111 S 2K +1	TA	110	56
21	11	111	O 2P =	CB	-110	55	26	11	109 S 3K +1	TA	130	67
21	1	104	W 2P =	T4	-110	55	26	8	103 O 2SA -2	K8	200	83
21	8	105	O 4P -1	CB	50	80	26	4	108 W 4P -2	CA	200	83
21	6	101	O 4P -1	CB	50	80	26	6	112 O 2SA -3	K9	300	100
21	5	112	O 4P -1	T4	50	80						
21	4	110	O 4P -2	CB	100	100						
22	9	107	N 5P -4	TA	-200	0						
22	3	108	W 3T +1	KK	-130	10						
22	8	105	N 5K -2	T9	-100	20						
22	11	111	N 4K -1	T7	-50	30						
22	5	112	N 3K =	T9	110	40						
22	7	103	N 3K +1	P3	130	50						
22	10	109	W 5T -2	KK	200	75						
22	6	101	S 3P +2	TA	200	75						
22	4	110	W 5T -2	KK	200	75						

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