

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 20.01.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz
1	8	115	W 3SA +2 T3	-460	0	6	13	108	W 3P +1 TA	-170	25	11	4	102	O 4C = T4	-420	39
1	1	101	O 3SA +1 K2	-430	28	6	12	106	W 3P +1 TA	-170	25	11	1	111	O 4C = T4	-420	39
1	15	114	W 3SA +1 C3	-430	28	6	1	114	S 5T -3 PA	-150	40	11	14	107	O 4C = KB	-420	39
1	12	108	W 3SA +1 C3	-430	28	6	2	101	W 2P +1 K10	-140	65	11	12	103	O 4C = TB	-420	39
1	11	106	O 3SA +1 K2	-430	28	6	15	112	W 2P +1 K5	-140	65	11	11	101	O 4C = PA	-420	39
1	14	112	W 3SA = C3	-400	67	6	14	110	W 3P = K10	-140	65	11	13	105	O 2C +2 KB	-170	78
1	9	102	O 3SA = P9	-400	67	6	10	102	W 3P = K10	-140	65	11	15	109	O 3C = T6	-140	89
1	7	113	W 3SA = C3	-400	67	6	11	104	W 4P -1 K8	100	95	11	2	113	O 4C -1 K4	50	100
1	13	110	W 2SA +3 C6	-210	89	6	8	113	W 4P -1 TD	100	95	12	5	104	N 2P -4 T6	-400	0
1	10	104	W 3SA -1 C9	50	100	7	11	103	O 6SA +1 K4	-1470	0	12	12	103	N 2SA -2 P2	-200	11
2	8	115	W 3P +2 T2	-200	0	7	14	109	O 6C +1 KB	-1460	10	12	4	102	W 3T = PA	-110	22
2	1	101	W 3P +1 K9	-170	39	7	15	111	W 3SA +4 P2	-720	35	12	11	101	W 2T = PA	-90	33
2	15	114	W 3P +1 C9	-170	39	7	13	107	W 3SA +4 K9	-720	35	12	3	115	W 3T -1 PA	50	72
2	12	108	W 2P +2 T2	-170	39	7	12	105	W 3SA +4 K7	-720	35	12	2	113	W 3T -1 PA	50	72
2	11	106	W 2P +2 K9	-170	39	7	9	114	W 3SA +4 K5	-720	35	12	1	111	W 3T -1 K9	50	72
2	10	104	W 3P +1 C9	-170	39	7	1	113	O 4C +3 KB	-710	60	12	15	109	W 3T -1 PA	50	72
2	9	102	W 2P +2 KD	-170	39	7	10	101	W 3SA +3 K6	-690	70	12	14	107	W 3T -1 PA	50	72
2	13	110	W 3P = KD	-140	78	7	4	104	W 5T +1 K6	-620	85	12	13	105	W 2P -1 TA	50	72
2	14	112	N 2C +1 TD	140	89	7	3	102	W 5T +1 C2	-620	85	13	7	107	N 4C -1 K5	-100	28
2	7	113	N 2C +2 P7	170	100	7	2	115	O 6C -2 K8	200	100	13	5	103	N 4C -1 P3	-100	28
3	13	109	S 3SA +1 K5	430	5	8	3	102	O 4P +1 CK	-450	15	13	4	101	N 4C -1 P3	-100	28
3	11	105	S 3SA +1 K6	430	5	8	1	113	O 4P +1 CK	-450	15	13	3	114	N 4C -1 TA	-100	28
3	2	102	S 4P +1 CB	450	30	8	13	107	O 4P +1 TA	-450	15	13	1	110	N 4C -1 P6	-100	28
3	12	107	S 4P +1 T9	450	30	8	12	105	O 5P = CK	-450	15	13	13	104	N 4C -1 P6	-100	28
3	8	114	S 4P +1 CB	450	30	8	4	104	O 4P = TA	-420	50	13	2	112	N 4C = P3	620	83
3	1	115	S 4P +2 CB	480	75	8	11	103	O 4P = TA	-420	50	13	15	108	N 4C = P8	620	83
3	15	113	S 4P +2 C5	480	75	8	9	114	O 4P = C5	-420	50	13	14	106	N 4C = K5	620	83
3	14	111	S 4P +2 CD	480	75	8	15	111	S 5C X -2 PD	-300	70	13	12	102	N 4C = P6	620	83
3	10	103	S 4P +2 CB	480	75	8	14	109	S 3C -3 PD	-150	80	14	13	104	N 3SA -2 CD	-100	0
3	9	101	S 4P +2 CB	480	75	8	2	115	S 5C X -1 PD	-100	95	14	14	106	W 2P -1 CA	50	11
3	7	112	S 4P +2 CB	480	75	8	10	101	S 5C X -1 PD	-100	95	14	12	102	S 3K = C7	110	22
4	12	107	S 3SA -2 T8	-200	0	9	4	103	S 4P -1 C9	-50	10	14	5	103	N 1SA +2 P10	150	33
4	9	101	N 2SA -1 P7	-100	10	9	3	101	S 4P -1 C3	-50	10	14	1	110	N 2SA +3 C4	210	44
4	13	109	S 1SA = TK	90	20	9	15	110	N 4P -1 PD	-50	10	14	7	107	N 3SA = C4	400	61
4	11	105	S 1C +2 KB	140	30	9	13	106	S 3P = C8	140	30	14	4	101	N 3SA = C4	400	61
4	15	113	N 3K +3 P8	170	40	9	2	114	O 4C -2 PA	200	55	14	3	114	N 3SA +1 C4	430	78
4	14	111	S 2SA +2 P10	180	55	9	14	108	O 4C -2 PA	200	55	14	15	108	N 3SA +2 P6	460	89
4	10	103	S 2SA +2 TB	180	55	9	12	104	O 4C -2 PA	200	55	14	2	112	N 3SA +3 C4	490	100
4	2	102	S 3SA = TK	600	70	9	11	102	O 4C -2 PA	200	55	15	14	105	N 4P -2 KD	-200	0
4	1	115	S 3SA +1 TK	630	90	9	10	115	O 5C -3 PA	300	80	15	8	108	N 4P -1 KD	-100	22
4	8	114	S 3SA +1 TK	630	90	9	5	105	S 4P = C9	420	95	15	4	115	N 4P -1 K4	-100	22
4	7	112	S 3SA +1 TB	630	90	9	1	112	S 4P = C3	420	95	15	3	113	N 4P -1 C3	-100	22
5	3	103	S 4C X -1 TA	-200	0	10	11	102	O 4P +1 CA	-650	0	15	2	111	N 2P = KD	110	44
5	11	104	S 4C -1 TA	-100	10	10	14	108	O 4P = KB	-620	15	15	1	109	N 3P = KD	140	61
5	15	112	O 3P -1 CA	50	20	10	10	115	W 4P = TA	-620	15	15	13	103	N 2P +1 KD	140	61
5	13	108	S 3C = PK	140	50	10	2	114	W 3P = TA	-140	30	15	5	102	N 2P +2 P2	170	78
5	12	106	S 3C = TA	140	50	10	5	105	S 1SA -1 C6	-100	50	15	7	106	N 4P = C4	620	89
5	10	102	S 3C = TA	140	50	10	3	101	N 4T -1 P2	-100	50	15	15	107	N 4P +1 C3	650	100
5	9	115	S 3C = TA	140	50	10	12	104	N 5T -1 P2	-100	50	16	8	108	W 2P +2 CK	-170	11
5	8	113	S 2C +1 TA	140	50	10	4	103	O 4P -1 K6	100	80	16	7	106	O 1P +3 KB	-170	11
5	2	101	S 4C = TA	620	90	10	1	112	W 4P -1 TA	100	80	16	2	111	O 1P +3 K2	-170	11
5	1	114	S 4C = PK	620	90	10	13	106	O 4P -1 TA	100	80	16	3	113	O 1P +2 K5	-140	39
5	14	110	S 4C = TA	620	90	10	15	110	S 3T +1 P3	130	100	16	15	107	O 2P +1 KB	-140	39
6	3	103	W 4P = TA	-620	5	11	3	115	O 4C +1 T4	-450	0	16	13	103	W 2C = T10	-110	56
6	9	115	W 4P = K10	-620	5	11	5	104	O 4C = P10	-420	39	16	5	102	N 1C -2 PA	-100	72

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 20.01.2015

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
16	1	109	N 3K -2	PA	-100	72	22	10	109	S 1SA -1	K6	-50	22	27	11	108	N 2C -1	TA	-50	78
16	14	105	W 1T +1	KB	-90	89	22	5	114	S 1SA =	K6	90	33	27	12	110	O 2SA -1	P5	50	94
16	4	115	O 4P -1	CA	100	100	22	11	111	S 1SA +1	K9	120	56	27	10	106	O 2T -1	C6	50	94
17	15	106	S 2K X -3	T7	-500	0	22	9	107	S 1SA +1	T10	120	56	28	9	104	O 4P +2	TB	-480	0
17	14	104	O 4C =	KA	-420	11	22	2	108	S 1SA +1	K6	120	56	28	14	114	W 4P +1	T6	-450	50
17	9	109	O 3SA =	KA	-400	22	22	8	105	S 1SA +2	K6	150	78	28	13	112	W 4P +1	KA	-450	50
17	7	105	O 2C +2	KA	-170	44	22	3	110	S 1SA +3	T10	180	89	28	12	110	W 4P +1	KA	-450	50
17	5	101	O 2C +2	KA	-170	44	22	4	112	S 1SA X +	K6	280	100	28	11	108	W 4P +1	T2	-450	50
17	3	112	O 2C +2	KA	-170	44	23	3	109	S 3SA -3	P7	-300	0	28	10	106	W 4P +1	T6	-450	50
17	2	110	O 2C +1	KA	-140	67	23	7	102	S 3SA -2	P7	-200	17	28	7	115	W 4P +1	T3	-450	50
17	8	107	W 3T =	KA	-110	78	23	5	113	S 2SA -2	P7	-200	17	28	5	111	W 4P +1	T9	-450	50
17	4	114	O 4C -1	KA	50	94	23	11	110	S 2SA -1	T2	-100	44	28	4	109	W 4P +1	T6	-450	50
17	1	108	O 3C -1	KA	50	94	23	4	111	S 3SA -1	T2	-100	44	28	8	102	W 4P =	C7	-420	100
18	15	106	W 3SA +3	P2	-490	0	23	2	107	S 3SA -1	T2	-100	44	29	15	115	W 2P +2	KA	-170	6
18	9	109	W 3SA +1	TB	-430	17	23	9	106	W 2C -1	T8	100	67	29	7	114	W 2P +2	KA	-170	6
18	7	105	W 3SA +1	P2	-430	17	23	10	108	S 3K =	P7	110	78	29	14	113	W 2P +1	KA	-140	50
18	8	107	O 3SA =	P2	-400	56	23	8	104	S 2SA +1	P7	150	89	29	13	111	W 2P +1	KA	-140	50
18	4	114	W 3SA =	P2	-400	56	23	12	112	W 2P -3	T8	300	100	29	12	109	W 2P +1	KA	-140	50
18	3	112	W 3SA =	P2	-400	56	24	12	112	N 2K -1	T5	-50	11	29	11	107	W 2P +1	KA	-140	50
18	2	110	W 3SA =	P2	-400	56	24	11	110	S 4P -1	TA	-50	11	29	8	101	W 2P +1	T8	-140	50
18	14	104	O 3SA =	T6	-400	56	24	5	113	S 4P -1	TA	-50	11	29	5	110	W 2P +1	K10	-140	50
18	5	101	O 5K -1	TA	50	94	24	7	102	S 3P =	TA	140	33	29	10	105	W 2P =	C7	-110	94
18	1	108	W 3SA -1	P10	50	94	24	8	104	S 3P +1	TA	170	50	29	9	103	W 2P =	TB	-110	94
19	3	111	N 3SA -3	PK	-150	0	24	3	109	S 2P +2	TA	170	50	30	11	107	S 2SA +2	T4	180	0
19	5	115	N 3K -1	CD	-50	22	24	10	108	N 3P +2	TK	200	67	30	15	115	N 3P +2	P4	200	11
19	2	109	S 4C -1	P2	-50	22	24	9	106	S 4P =	C3	420	89	30	13	111	S 3SA =	T8	400	22
19	15	105	S 4C -1	P2	-50	22	24	4	111	N 4P =	CB	420	89	30	7	114	S 4P =	T4	420	33
19	10	110	N 2SA =	PK	120	44	24	2	107	N 4P =	C2	420	89	30	14	113	S 3SA +1	P5	430	44
19	7	104	N 2SA +1	PK	150	56	25	12	111	N 3SA -2	K5	-100	0	30	12	109	S 4P +1	P7	450	72
19	9	108	S 2SA +3	PK	210	72	25	13	113	N 4P -1	T9	-50	11	30	10	105	N 4P +1	K6	450	72
19	8	106	N 2SA +3	PK	210	72	25	5	112	N 1P +2	C6	140	28	30	9	103	N 4P +1	T9	450	72
19	1	107	S 4C =	P2	420	89	25	4	110	N 2P +1	KA	140	28	30	8	101	N 4P +1	CA	450	72
19	4	113	S 4C +1	P2	450	100	25	3	108	N 2SA +1	K5	150	44	30	5	110	N 3SA +3	K7	490	100
20	9	108	N 4C -1	T4	-100	17	25	8	103	N 2P +2	T9	170	56							
20	8	106	N 4C -1	T8	-100	17	25	11	109	N 4P =	T9	420	83							
20	7	104	S 4P -1	K5	-100	17	25	10	107	N 4P =	KA	420	83							
20	2	109	N 3C -1	T2	-100	17	25	9	105	N 4P =	KA	420	83							
20	5	115	S 2P +2	T9	170	50	25	7	101	N 4P =	KA	420	83							
20	3	111	S 1P +3	K5	170	50	26	11	109	O 4C +1	K3	-650	28							
20	1	107	S 2P +3	T9	200	67	26	10	107	O 4C +1	C8	-650	28							
20	15	105	N 4C =	T6	620	78	26	8	103	O 4C +1	K3	-650	28							
20	10	110	N 4C +1	T5	650	94	26	7	101	O 4C +1	T3	-650	28							
20	4	113	N 4C +1	K3	650	94	26	4	110	O 4C +1	PK	-650	28							
21	2	108	W 4P =	TK	-420	0	26	3	108	O 4C +1	T3	-650	28							
21	11	111	W 3P +1	K3	-170	17	26	9	105	O 3SA +1	K6	-630	67							
21	7	103	W 3P +1	TK	-170	17	26	13	113	O 4C =	PK	-620	89							
21	10	109	W 3P =	C7	-140	50	26	12	111	O 4C =	PK	-620	89							
21	5	114	W 2P +1	TK	-140	50	26	5	112	O 4C =	P4	-620	89							
21	3	110	W 3P =	TK	-140	50	27	7	115	W 1SA +3	T3	-180	0							
21	1	106	W 3P =	C7	-140	50	27	8	102	W 2SA =	CB	-120	17							
21	4	112	W 2P =	TK	-110	78	27	5	111	O 2SA =	P5	-120	17							
21	8	105	W 3P -1	TK	50	89	27	14	114	S 2P -2	KA	-100	50							
21	9	107	N 3T =	K10	110	100	27	13	112	N 2C -2	KK	-100	50							
22	7	103	O 2K X =	C2	-180	0	27	9	104	N 2C -2	C3	-100	50							
22	1	106	S 1SA -2	P9	-100	11	27	4	109	S 2P -2	T9	-100	50							

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.