

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 23.12.2014**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
1	8	104	N 4C -1	P3	-50	6	2	101	S 4T =	CA	130	67	12	7	108	S 5K -2	TK	-200	0	
1	4	107	N 3C -1	P6	-50	6	1	110	S 3T +1	CA	130	67	12	8	110	S 5K -1	TK	-100	11	
1	7	102	W 1K -1	CA	50	22	6	9	104	S 3T +1	CA	130	67	12	10	103	S 1SA +2	TK	150	28
1	10	108	N 2C =	K6	110	33	6	10	106	N 1SA +2	C9	150	89	12	9	101	S 1K +4	TK	150	28
1	1	101	S 2SA =	KA	120	44	6	8	102	S 3SA +1	CA	430	100	12	6	106	N 3SA =	C5	600	61
1	3	105	N 3C =	K6	140	56	7	10	105	N 1T -3	TA	-300	0	12	2	109	S 3SA =	TK	600	61
1	11	110	N 2C +2	K6	170	83	7	4	104	O 3P +1	T9	-170	11	12	1	107	N 3SA =	TK	600	61
1	9	106	N 1C +3	K6	170	83	7	1	109	O 3T =	KD	-110	28	12	11	105	S 3SA =	TK	600	61
1	5	109	S 2C +2	KA	170	83	7	9	103	O 3T =	T10	-110	28	12	5	104	S 3SA +1	T9	630	94
1	2	103	N 2C +2	K6	170	83	7	6	108	O 1SA =	T9	-90	44	12	4	102	S 3SA +1	T10	630	94
2	8	104	W 6C X +	P4	-1310	0	7	3	102	O 3SA -1	T3	100	72	13	7	107	W 4C +1	K4	-650	22
2	4	107	O 6SA +1	T4	-1020	11	7	11	107	W 3SA -1	CA	100	72	13	6	105	O 4C +1	KB	-650	22
2	1	101	O 6C +1	P5	-1010	28	7	7	110	W 3SA -1	C2	100	72	13	4	101	W 4C +1	TK	-650	22
2	3	105	O 6C +1	P5	-1010	28	7	5	106	O 3P -1	C6	100	72	13	2	108	W 4C +1	TK	-650	22
2	10	108	O 6SA =	K4	-990	44	7	8	101	O 3SA -2	C3	200	100	13	11	104	W 4C +1	TK	-650	22
2	7	102	W 6P =	K8	-980	56	8	11	107	W 4C =	P2	-420	0	13	5	103	W 4C =	TK	-620	61
2	11	110	W 4P +3	T10	-510	78	8	10	105	W 3C +2	P9	-200	11	13	3	110	W 4C =	TK	-620	61
2	5	109	W 4C +3	K8	-510	78	8	6	108	W 2C +2	P2	-170	22	13	1	106	S 3P -3	KA	-300	78
2	2	103	W 4P +3	T2	-510	78	8	4	104	W 3C =	P9	-140	44	13	10	102	W 1C +4	TK	-200	89
2	9	106	W 3SA +3T10	-490	100		8	3	102	W 2C +1	TA	-140	44	13	8	109	W 2C +2	TK	-170	100
3	8	103	N 5K X -4	PK	-800	0	8	8	101	W 3C =	P9	-140	44	14	1	106	S 2SA -2	KD	-100	0
3	7	101	O 4C +1	K6	-650	11	8	9	103	N 3P -2	C9	-100	67	14	5	103	S 1SA -1	C7	-50	33
3	11	109	O 3C +1	K10	-170	33	8	1	109	N 2P -1	KA	-50	78	14	4	101	S 1SA -1	C6	-50	33
3	10	107	O 3C +1	K10	-170	33	8	7	110	W 3C -1	TA	50	89	14	3	110	S 2T -1	KD	-50	33
3	5	108	O 3C +1	K10	-170	33	8	5	106	W 4C -2	P9	100	100	14	2	108	S 2SA -1	K6	-50	33
3	6	110	N 5K -3	PK	-150	56	9	6	107	W 2K +1	P6	-110	0	14	8	109	S 2SA -1	C6	-50	33
3	3	104	W 3P =	KA	-140	67	9	4	103	N 4C -2	TK	-100	11	14	7	107	S 2T =	PK	90	78
3	2	102	O 4C -1	K10	100	89	9	3	101	W 1K +1	C2	-90	22	14	11	104	S 1SA =	K6	90	78
3	9	105	O 4C -1	K10	100	89	9	5	105	S 3P -1	C7	-50	50	14	10	102	S 2T =	C6	90	78
3	4	106	W 4P -1	KA	100	89	9	1	108	N 1SA -1	TK	-50	50	14	6	105	W 3K -2	PB	100	100
4	7	101	W 3SA +3	C2	-690	0	9	11	106	S 3P -1	C7	-50	50	15	11	103	W 1SA +1	P3	-120	0
4	2	102	W 3SA +1	C2	-630	39	9	9	102	N 2SA -1	C4	-50	50	15	7	106	N 2P -1	K7	-100	11
4	11	109	W 3SA +1	C2	-630	39	9	10	104	O 1SA -1	P7	100	78	15	10	101	N 2T =	K7	90	22
4	10	107	W 3SA +1	T5	-630	39	9	7	109	N 1SA +1	TB	120	89	15	8	108	S 1SA +1	C6	120	56
4	9	105	O 3SA +1	C3	-630	39	9	2	110	S 2P +1	K3	140	100	15	6	104	S 1SA +1	C4	120	56
4	8	103	W 3SA +1	C2	-630	39	10	2	110	S 5K -1	P3	-100	11	15	2	107	S 1SA +1	K5	120	56
4	5	108	W 3SA +1C10	-630	39		10	7	109	S 3SA -1	P9	-100	11	15	1	105	S 2SA =	K3	120	56
4	6	110	W 3SA =	C2	-600	78	10	6	107	S 3SA -1	P9	-100	11	15	9	110	S 2SA =	C4	120	56
4	3	104	O 1P +3	CA	-170	89	10	5	105	S 5K =	TB	600	33	15	5	102	S 1SA +2	C4	150	94
4	4	106	O 4P -1	CA	100	100	10	4	103	N 4C =	PA	620	67	15	3	109	O 2P -3	KA	150	94
5	3	103	S 3P -2	C2	-200	11	10	3	101	N 4C =	PA	620	67	16	7	106	O 3SA +3	C7	-690	0
5	11	108	S 4P -2	K6	-200	11	10	1	108	N 4C =	PA	620	67	16	8	108	O 3SA +2	C7	-660	39
5	9	104	S 4P -2	C2	-200	11	10	10	104	N 4C =	PA	620	67	16	6	104	O 3SA +2	T9	-660	39
5	2	101	S 4P -1	K6	-100	44	10	9	102	N 4C =	PA	620	67	16	5	102	O 3SA +2	T8	-660	39
5	1	110	N 4P -1	C3	-100	44	10	11	106	S 3SA +1	P8	630	100	16	3	109	O 3SA +2	T6	-660	39
5	10	106	S 4P -1	K6	-100	44	11	11	105	S 4C +1	C9	450	6	16	10	101	W 3SA +2	T3	-660	39
5	5	107	N 3SA =	TB	600	67	11	9	101	S 4C +1	KK	450	6	16	9	110	W 3SA +2	T4	-660	39
5	8	102	S 4P =	C4	620	83	11	6	106	S 4C +2	KK	480	61	16	2	107	O 3SA +1	C7	-630	83
5	4	105	S 4P =	C2	620	83	11	5	104	S 4C +2	P2	480	61	16	11	103	O 3SA +1	P3	-630	83
5	6	109	S 3SA +1	C3	630	100	11	4	102	S 4C +2	KK	480	61	16	1	105	O 6SA -2	P9	200	100
6	4	105	S 4T -1	CA	-50	0	11	2	109	S 4C +2	KK	480	61	17	7	105	W 1SA +2	T6	-150	0
6	3	103	S 3T =	CA	110	11	11	1	107	S 4C +2	TK	480	61	17	3	108	S 3T -1	PA	-50	17
6	11	108	N 2SA =	C9	120	33	11	10	103	S 4C +2	C9	480	61	17	1	104	S 3SA -1	P6	-50	17
6	6	109	N 2SA =	C9	120	33	11	8	110	S 4C +2	TK	480	61	17	11	102	W 1SA -2	T6	100	33
6	5	107	S 1SA +1	P5	120	33	11	7	108	S 4C +2	T2	480	61	17	9	109	S 3T =	K5	110	67

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	
17	6	103	N 2T +1	C6	110	67
17	5	101	S 2T +1	K8	110	67
17	4	110	S 3T =	K5	110	67
17	2	106	S 2T +1	PA	110	67
17	8	107	S 2C +2	K5	170	100
18	6	103	O 2P +1	CB	-140	11
18	4	110	O 2C +1	KA	-140	11
18	1	104	O 2P +1	CB	-140	11
18	9	109	O 2P =	CB	-110	50
18	8	107	O 2P =	CB	-110	50
18	7	105	O 2P =	K8	-110	50
18	5	101	O 2P =	CB	-110	50
18	3	108	O 4P -1	KA	50	83
18	2	106	O 2P -1	T6	50	83
18	11	102	O 1SA -3	T6	150	100
19	9	108	S 6C -1	C5	-50	17
19	6	102	S 6C -1	PA	-50	17
19	4	109	S 6C -1	PA	-50	17
19	1	103	S 6C -1	PA	-50	17
19	3	107	N 4C =	K4	420	44
19	10	110	N 4C +1	K4	450	72
19	8	106	N 4C +1	P8	450	72
19	2	105	S 4C +1	TB	450	72
19	11	101	S 4C +1	PA	450	72
19	7	104	S 3SA +4	P4	520	100
20	3	107	S 2T +1	CA	110	0
20	7	104	S 2SA +1	T3	150	11
20	11	101	N 3SA =	K6	600	22
20	10	110	N 3SA +1	P6	630	61
20	9	108	N 3SA +1	C7	630	61
20	8	106	N 3SA +1	C3	630	61
20	4	109	N 3SA +1	C7	630	61
20	2	105	N 3SA +1	P6	630	61
20	1	103	N 3SA +1	C7	630	61
20	6	102	N 3SA +2	C3	660	100
21	7	103	O 3K +1	C9	-130	0
21	9	107	W 3K =	CK	-110	11
21	8	105	N 2C -1	KA	-100	22
21	10	109	O 3T -1	C3	50	39
21	6	101	W 3K -1	CK	50	39
21	2	104	N 2C =	KA	110	56
21	5	110	N 2C +1	KA	140	83
21	4	108	S 3P =	TA	140	83
21	3	106	N 3C =	KA	140	83
21	1	102	N 2C +1	KA	140	83
22	5	110	W 4C =	TA	-620	0
22	7	103	W 3C +2	TA	-200	11
22	9	107	W 3C +1	TA	-170	28
22	3	106	W 3C +1	TA	-170	28
22	6	101	N 4T -3	C5	-150	44
22	10	109	N 3T -2	P8	-100	61
22	2	104	N 3T -2	C5	-100	61
22	4	108	N 3T -1	C5	-50	83
22	1	102	N 3T -1	C5	-50	83
22	8	105	O 2P -1	K6	100	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.