

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 09.12.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	W 4C =	K3	-420	5	6	8	113 S 3C -2	T9	-100	0	11	15	109 N 4P -1	K10	-50	0
1	9	102	W 4C =	K3	-420	5	6	1	114 S 3C -1	KA	-50	15	11	13	105 N 2P =	K2	110	10
1	14	112	O 3SA =	K2	-400	20	6	13	108 S 2C -1	KA	-50	15	11	6	106 N 3P =	K6	140	55
1	13	110	W 3C +1	K3	-170	40	6	15	112 S 2C =	T2	110	45	11	5	104 N 2P +1	C4	140	55
1	11	106	W 3C +1	K9	-170	40	6	14	110 S 2C =	KA	110	45	11	4	102 N 2P +1	K10	140	55
1	6	111	W 3C +1	P4	-170	40	6	10	102 S 2C =	KA	110	45	11	3	115 N 2P +1	K10	140	55
1	15	114	O 3SA -1	K6	50	80	6	9	115 S 2C =	KA	110	45	11	2	113 N 2P +1	K10	140	55
1	12	108	W 5C -1	K3	50	80	6	2	101 S 2C +1	KA	140	75	11	1	111 N 3P =	K10	140	55
1	10	104	O 3SA -1	K2	50	80	6	11	104 S 3C =	T8	140	75	11	12	103 N 2P +1	K10	140	55
1	8	115	O 3SA -1	K2	50	80	6	3	103 S 3C +1	KA	170	95	11	11	101 N 2P +1	K2	140	55
1	7	113	O 3SA -1	K2	50	80	6	12	106 S 2C +2	KA	170	95	11	14	107 W 4C X -3	PA	500	100
2	15	114	S 6P -1	C9	-100	0	7	3	102 W 3K +1	CK	-130	10	12	6	106 S 3P -1	TA	-100	5
2	12	108	S 4P +2	C9	680	20	7	15	111 W 3K +1	CK	-130	10	12	11	101 S 3P -1	C10	-100	5
2	10	104	S 4P +2	C9	680	20	7	12	105 W 4K =	C7	-130	10	12	3	115 S 2P =	TA	110	30
2	7	113	S 4C +2	K3	680	20	7	4	104 W 3K =	CK	-110	40	12	2	113 S 2P =	TA	110	30
2	1	101	S 4P +3	C9	710	50	7	2	115 W 3K =	CK	-110	40	12	12	103 S 2P =	TA	110	30
2	11	106	S 4P +3	K9	710	50	7	14	109 W 3K =	CK	-110	40	12	5	104 S 3P =	C10	140	70
2	6	111	S 4P +3	C6	710	50	7	11	103 N 3C -1	K6	-100	60	12	4	102 S 3P =	TA	140	70
2	14	112	S 6P =	TD	1430	75	7	1	113 O 4K -1	CK	100	80	12	1	111 S 2P +1	TA	140	70
2	13	110	S 6P =	TD	1430	75	7	13	107 W 4K -1	PA	100	80	12	15	109 N 2P +1	TA	140	70
2	8	115	S 6P +1	TD	1460	90	7	10	101 W 4K -1	PA	100	80	12	14	107 S 2P +1	TA	140	70
2	9	102	S 6SA +1	K7	1470	100	7	9	114 N 4C =	K2	620	100	12	13	105 S 3P +1	TA	170	100
3	2	102	O 6SA =	K7	-1440	0	8	14	109 O 4C =	PA	-420	0	13	3	114 O 3SA +1	K2	-630	5
3	15	113	O 3SA +4	K7	-720	15	8	12	105 S 4P -4	CA	-200	10	13	2	112 O 3SA +1	K7	-630	5
3	8	114	O 3SA +4	K7	-720	15	8	10	101 S 4P -3	K2	-150	20	13	6	105 O 3SA =	K7	-600	40
3	11	105	W 4C +3	K3	-710	30	8	15	111 O 3C =	PA	-140	30	13	1	110 O 3SA =	K7	-600	40
3	1	115	W 4C +2	K3	-680	45	8	1	113 S 3P -2	CA	-100	40	13	14	106 O 3SA =	K2	-600	40
3	12	107	W 4C +2	K3	-680	45	8	13	107 S 2P -1	CA	-50	50	13	13	104 O 3SA =	K2	-600	40
3	13	109	O 3SA +2	TD	-660	65	8	4	104 O 4C -1	PA	50	70	13	12	102 O 3SA =	K2	-600	40
3	9	101	O 3SA +2	K7	-660	65	8	11	103 O 4C -1	PA	50	70	13	5	103 O 3SA -1	K7	100	75
3	14	111	W 4C +1	K3	-650	90	8	9	114 O 4C -1	PA	50	70	13	15	108 O 3SA -1	K7	100	75
3	10	103	W 4C +1	P8	-650	90	8	3	102 O 4C X -1	K4	100	95	13	7	107 O 3SA -2	K7	200	95
3	7	112	W 4C +1	K5	-650	90	8	2	115 W 4K -2	P2	100	95	13	4	101 O 4C -2	TA	200	95
4	10	103	S 4SA -2	T7	-200	0	9	2	114 N 2SA -2	K2	-100	0	14	13	104 S 2P +1	T4	140	0
4	15	113	N 4C -1	T10	-100	20	9	4	103 S 4C -1	K3	-50	20	14	1	110 S 2P +2	T4	170	10
4	13	109	N 4C -1	K2	-100	20	9	3	101 S 4C -1	T4	-50	20	14	5	103 S 2P +3	T4	200	40
4	8	114	S 2SA -1	T7	-100	20	9	12	104 S 3C -1	K4	-50	20	14	2	112 S 2P +3	T4	200	40
4	12	107	N 3P =	T10	140	45	9	1	112 S 2C =	K3	110	65	14	15	108 S 3P +2	T4	200	40
4	7	112	N 2P +1	TB	140	45	9	15	110 S 2C =	K3	110	65	14	14	106 S 3P +2	T4	200	40
4	11	105	N 2C +2	T4	170	60	9	14	108 S 2C =	T9	110	65	14	12	102 S 2P +3	K8	200	40
4	2	102	S 3SA =	K5	600	75	9	13	106 S 2C =	K4	110	65	14	7	107 S 2P +4	T4	230	75
4	1	115	S 3SA =	T7	600	75	9	11	102 S 2C =	PA	110	65	14	6	105 S 2P +4	T4	230	75
4	14	111	N 4C =	K2	620	95	9	10	115 S 2C =	P2	110	65	14	4	101 S 4P +1	K2	450	95
4	9	101	N 4C =	T4	620	95	9	5	105 S 2C +1	K8	140	100	14	3	114 S 4P +1	T4	450	95
5	8	113	O 3SA +2	PK	-460	0	10	10	115 N 1SA +4	K2	210	0	15	5	102 S 4C -1	P3	-100	10
5	15	112	O 4C +1	PK	-450	15	10	5	105 N 4P +1	T7	650	50	15	15	107 S 4C -1	TA	-100	10
5	11	104	O 4C +1	T2	-450	15	10	4	103 N 5P =	T8	650	50	15	14	105 N 4P -1	KA	-100	10
5	2	101	O 4C =	PK	-420	40	10	3	101 N 4P +1	T6	650	50	15	3	113 O 4K -1	P5	50	30
5	10	102	O 4C =	PK	-420	40	10	2	114 N 4P +1	C2	650	50	15	1	109 O 5K -2	CA	100	40
5	9	115	O 4C =	PK	-420	40	10	1	112 N 4P +1	P3	650	50	15	4	115 O 5K X -2	CA	300	55
5	1	114	O 1C +2	PK	-140	60	10	15	110 N 4P +1	K6	650	50	15	2	111 O 5K X -2	P5	300	55
5	3	103	O 4C -1	PK	50	80	10	14	108 N 4P +1	K3	650	50	15	8	108 N 4P =	KA	620	85
5	14	110	O 4C -1	PK	50	80	10	13	106 N 4P +1	K2	650	50	15	7	106 S 4C =	K7	620	85
5	12	106	O 4C -1	PK	50	80	10	11	102 N 4P +1	K2	650	50	15	6	104 S 4C =	P9	620	85
5	13	108	O 4C -2	PK	100	100	10	12	104 N 4P +2	PB	680	100	15	13	103 S 4C =	TA	620	85

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 09.12.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	14	105	O 6P +1	C5	-1460	0	21	10	109 W 4P +2	T2	-480	0	26	8	103 O 4C +2	P8	-680	5
16	3	113	O 4P +3	T4	-710	20	21	11	111 W 4P =	KA	-420	50	26	6	114 O 4C +2	P8	-680	5
16	2	111	O 4P +3	T7	-710	20	21	9	107 W 4P =	KA	-420	50	26	13	113 O 4C +1	TB	-650	40
16	1	109	O 4P +3	T7	-710	20	21	8	105 W 4P =	TD	-420	50	26	12	111 O 4C +1	K5	-650	40
16	7	106	O 4P +2	T7	-680	40	21	6	101 O 4P =	TD	-420	50	26	9	105 O 4C +1	T3	-650	40
16	8	108	O 5P =	K7	-650	60	21	5	114 W 4P =	C10	-420	50	26	5	112 O 5C =	K6	-650	40
16	6	104	O 4P +1	K3	-650	60	21	4	112 W 4P =	TD	-420	50	26	3	108 O 4C +1	T6	-650	40
16	13	103	O 5P =	KK	-650	60	21	3	110 O 4P =	KA	-420	50	26	10	107 O 4C =	T8	-620	75
16	5	102	O 3P +3	T7	-230	80	21	2	108 W 4P =	C2	-420	50	26	4	110 O 4C =	T2	-620	75
16	15	107	O 3P +2	K7	-200	90	21	1	106 W 4P =	KA	-420	50	26	7	101 W 5C -1	T8	100	90
16	4	115	O 6SA -4	K3	400	100	21	7	103 W 4P -1	T3	50	100	26	11	109 O 6C -2	P3	200	100
17	14	104	N 4P X -4	T8	-800	0	22	2	108 S 4P -1	KD	-50	0	27	9	104 S 4C =	P6	420	0
17	5	101	N 5P X -3	KA	-500	10	22	8	105 N 3T +1	C8	130	10	27	12	110 S 4C +1	K7	450	20
17	9	109	W 5T +1	P9	-420	20	22	11	111 N 5T =	K2	400	20	27	10	106 S 4C +1	KB	450	20
17	3	112	W 5T =	PK	-400	30	22	10	109 N 3SA +1	C4	430	40	27	4	109 S 4C +1	KB	450	20
17	15	106	N 4P -4	T10	-200	40	22	9	107 N 3SA +1	C4	430	40	27	14	114 S 4C +2	P6	480	60
17	8	107	W 3T +2	P8	-150	50	22	4	112 N 3SA +1	C4	430	40	27	11	108 S 4C +2	P6	480	60
17	4	114	N 3P -2	T8	-100	65	22	6	101 N 3SA +2	C4	460	70	27	8	102 S 4C +2	TA	480	60
17	2	110	N 4P -2	T3	-100	65	22	3	110 N 3SA +2	C9	460	70	27	7	115 S 4C +2	KB	480	60
17	1	108	N 3P -1	C3	-50	80	22	1	106 N 3SA +2	C4	460	70	27	6	113 S 4P +2	KB	480	60
17	7	105	O 4C -2	P5	100	90	22	7	103 N 3SA +3	P4	490	95	27	13	112 N 4P +3	CD	510	95
17	6	103	N 2P =	T9	110	100	22	5	114 N 3SA +3	C4	490	95	27	5	111 N 4P +3	CD	510	95
18	3	112	O 2SA +1	CK	-150	0	23	4	111 S 3SA -2	P4	-200	0	28	13	112 W 3SA =	C6	-400	10
18	9	109	S 2C -1	T10	-100	25	23	3	109 S 3SA -1	P3	-100	10	28	12	110 O 3SA =	P6	-400	10
18	6	103	S 3C -1	T9	-100	25	23	9	106 S 2SA =	P3	120	20	28	7	115 W 3SA =	P5	-400	10
18	5	101	S 4C -1	KA	-100	25	23	10	108 N 3T +1	P5	130	30	28	6	113 O 4T =	P8	-130	35
18	15	106	S 4C -1	KA	-100	25	23	11	110 S 2SA +2	K5	180	40	28	4	109 W 3K +1	P7	-130	35
18	2	110	W 2K =	P9	-90	50	23	12	112 S 3SA =	P3	600	65	28	11	108 W 3K =	CA	-110	60
18	14	104	O 3SA -1	CK	50	60	23	8	104 S 3SA =	P3	600	65	28	10	106 O 3T =	P4	-110	60
18	8	107	W 3K -3	CB	150	70	23	7	102 S 3SA =	P3	600	65	28	5	111 W 3K =	P5	-110	60
18	7	105	S 3P +1	KA	170	80	23	2	107 S 3SA =	K5	600	65	28	8	102 O 2T =	P8	-90	80
18	1	108	N 4C =	KB	620	90	23	6	115 S 3SA +1	K3	630	95	28	9	104 W 3SA -1	P6	50	90
18	4	114	S 3C X =	T10	730	100	23	5	113 S 3SA +1	P4	630	95	28	14	114 O 5K -4	P4	200	100
19	7	104	N 4C X -6	KA	-1400	0	24	4	111 W 2C +1	PD	-140	0	29	12	109 S 4C -2	KA	-200	0
19	6	102	O 4P +2	TB	-680	15	24	3	109 W 2C =	T8	-110	10	29	15	115 S 4C -1	KA	-100	25
19	4	113	O 4P +2	C5	-680	15	24	7	102 N 2C -2	KK	-100	20	29	10	105 S 3C -1	KA	-100	25
19	5	115	O 4P +1	TK	-650	30	24	12	112 O 3C -1	T4	50	40	29	9	103 S 4C -1	KA	-100	25
19	3	111	O 4P =	TK	-620	40	24	10	108 W 1SA -1	PB	50	40	29	5	110 S 4C -1	KA	-100	25
19	10	110	O 3P +2	C5	-200	55	24	8	104 W 1SA -1	PD	50	40	29	14	113 S 2C +1	KK	140	50
19	9	108	O 3P +2	CK	-200	55	24	6	115 O 3T -2	CB	100	65	29	6	112 S 2C +2	KA	170	60
19	8	106	O 3P +1	TK	-170	75	24	5	113 O 3C -2	T5	100	65	29	13	111 S 4C =	KA	620	80
19	15	105	O 2P +2	TK	-170	75	24	11	110 S 2P =	TA	110	90	29	11	107 S 4C =	TA	620	80
19	1	107	N 3C -1	T3	-50	90	24	9	106 S 2P =	C2	110	90	29	7	114 S 4C =	KA	620	80
19	2	109	O 3K -1	TK	100	100	24	2	107 S 1P +1	TA	110	90	29	8	101 S 4C +1	KA	650	100
20	15	105	W 4P +1	K3	-650	0	25	10	107 S 4C -1	K10	-50	5	30	14	113 N 4C -2	PK	-100	0
20	6	102	W 3SA +1	K3	-630	10	25	7	101 S 5C -1	K4	-50	5	30	12	109 N 1P -1	T10	-50	20
20	9	108	W 4P =	CA	-620	20	25	11	109 N 3SA =	K6	400	20	30	7	114 S 3C -1	PB	-50	20
20	4	113	N 2C X -2	KD	-500	30	25	12	111 S 4C +1	K4	450	40	30	6	112 N 4C -1	PA	-50	20
20	2	109	N 3K -2	CK	-200	40	25	8	103 S 4C +1	K4	450	40	30	15	115 N 1P =	T10	80	50
20	7	104	W 2SA +1	C2	-150	55	25	3	108 N 4C +1	T4	450	40	30	13	111 N 1P =	K3	80	50
20	5	115	W 2SA +1	C5	-150	55	25	13	113 S 3SA +2	PB	460	60	30	5	110 N 1P =	K8	80	50
20	10	110	O 2P -1	C7	100	75	25	9	105 N 3SA +3	K2	490	70	30	11	107 N 2C +1	PA	140	75
20	3	111	O 3P -1	C7	100	75	25	6	114 N 4C +3	K6	510	90	30	10	105 N 2C +1	PA	140	75
20	8	106	W 4P -2	CA	200	90	25	5	112 N 5C +2	C4	510	90	30	8	101 N 2C +2	PA	170	90
20	1	107	O 3P -3	C7	300	100	25	4	110 S 4C +3	K4	510	90	30	9	103 N 4C =	PA	420	100

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.