

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 02.12.2014**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	13	110	W 4P +1	T6	-450	0	6	15	112 W 3SA =	C4	-600	40	11	14	107 W 2P =	TA	-110	22
1	7	113	O 3SA +1	C3	-430	11	6	13	108 W 3SA =	C4	-600	40	11	12	103 W 1C +1	TA	-110	22
1	1	101	O 4P =	TK	-420	44	6	12	106 W 3SA =	C5	-600	40	11	5	104 O 1SA =	K5	-90	50
1	12	108	W 4P =	T7	-420	44	6	11	104 W 3SA =	C4	-600	40	11	3	115 O 1SA =	K5	-90	50
1	11	106	W 4P =	TK	-420	44	6	9	115 W 3SA =	C5	-600	40	11	11	101 W 1P =	TA	-80	67
1	10	104	W 4P =	C6	-420	44	6	8	113 W 3SA =	PB	-600	40	11	2	113 S 2K -1	C2	-50	78
1	9	102	W 4P =	TK	-420	44	6	2	101 O 3P =	K2	-140	80	11	4	102 O 1SA -1	K5	50	94
1	8	115	W 3P +3	TK	-230	78	6	14	110 S 1P -2	KA	-100	90	11	1	111 W 3P -1	TA	50	94
1	14	112	O 3P +1	CD	-170	89	6	3	103 W 3SA -1	K4	100	100	12	5	104 N 4P -5	T3	-500	0
1	15	114	W 6P -1	TK	50	100	7	4	104 N 5K -2	PA	-200	0	12	12	103 S 3C -3	KA	-300	11
2	15	114	S 3SA -3	K7	-300	0	7	13	107 O 2C =	P4	-110	10	12	3	115 W 2T +1	PA	-110	22
2	10	104	S 1SA =	T9	90	11	7	9	114 O 3C -1	K8	100	20	12	4	102 S 2P -1	C7	-100	39
2	1	101	S 1SA +1	T5	120	28	7	10	101 S 3T =	C9	110	30	12	15	109 N 2P -1	T3	-100	39
2	14	112	S 2SA =	T4	120	28	7	3	102 N 3K +1	CA	130	45	12	1	111 W 2T =	T5	-90	56
2	7	113	S 2C +1	T9	140	44	7	11	103 N 3K +1	PA	130	45	12	13	105 W 3T -1	PK	50	67
2	12	108	N 1SA +2	K2	150	67	7	12	105 O 4C -2	KA	200	60	12	11	101 S 2SA =	T9	120	78
2	11	106	O 1C -3	PB	150	67	7	2	115 O 4C X -2	KA	500	70	12	14	107 S 2P +1	KA	140	89
2	9	102	S 1SA +2	T9	150	67	7	14	109 S 3SA =	C9	600	80	12	2	113 O 2SA -4	C3	200	100
2	13	110	S 1SA +3	P4	180	94	7	15	111 N 3SA +2	C5	660	90	13	14	106 O 3SA +2	KD	-660	0
2	8	115	S 1SA +3	K2	180	94	7	1	113 O 4C X -3	KA	800	100	13	3	114 W 4P =	TA	-620	17
3	1	115	O 5T X +1	P8	-950	0	8	11	103 W 2SA =	P2	-120	0	13	1	110 W 4P =	C2	-620	17
3	11	105	W 4C +2	PA	-680	10	8	1	113 S 3P -2	T4	-100	15	13	2	112 O 3SA =	K2	-600	39
3	2	102	O 5T +1	P9	-620	25	8	14	109 N 3C -2	P4	-100	15	13	12	102 O 3SA =	K9	-600	39
3	14	111	O 5T +1	T10	-620	25	8	4	104 S 3K -1	TK	-50	30	13	5	103 W 4P -1	C9	100	61
3	15	113	O 4T +2	P8	-170	60	8	13	107 W 2SA -1	P8	50	45	13	15	108 W 3SA -1	K3	100	61
3	13	109	O 3T +3	P8	-170	60	8	12	105 W 3SA -1	PD	50	45	13	7	107 O 3SA -2	T5	200	89
3	9	101	O 4T +2	PD	-170	60	8	10	101 S 2K =	T4	90	60	13	4	101 W 4P -2	C2	200	89
3	8	114	O 3T +3	P8	-170	60	8	3	102 W 4T -2	C6	100	70	13	13	104 O 3SA -2	K2	200	89
3	7	112	O 4T +2	PD	-170	60	8	2	115 S 2P +2	KA	170	85	14	2	112 O 1SA +1	P2	-120	0
3	10	103	N 3K -1	T8	-50	90	8	15	111 S 2P +2	KA	170	85	14	3	114 O 2K +1	CA	-110	28
3	12	107	N 2K +1	T9	110	100	8	9	114 S 3P X +2	KA	730	100	14	15	108 O 3K =	P8	-110	28
4	1	115	O 3SA =	T8	-600	15	9	2	114 W 4P +2	T10	-680	5	14	13	104 W 2K +1	CA	-110	28
4	15	113	W 3SA =	P7	-600	15	9	1	112 W 4P +2	T10	-680	5	14	12	102 O 2K +1	T9	-110	28
4	14	111	W 3SA =	P10	-600	15	9	15	110 W 4P +1	T10	-650	20	14	14	106 N 1SA -2	KA	-100	56
4	7	112	W 3SA =	P10	-600	15	9	5	105 N 4C X -2	P10	-300	35	14	1	110 O 2K =	PB	-90	67
4	12	107	N 2P -2	C6	-200	40	9	3	101 N 4C X -2	PB	-300	35	14	4	101 N 1SA -1	KA	-50	78
4	11	105	O 2SA +2	PB	-180	50	9	14	108 W 3P +1	C2	-170	50	14	5	103 W 2P -2	CA	100	89
4	13	109	W 3SA -1	P7	100	65	9	10	115 N 4C -3	TA	-150	60	14	7	107 W 2P -3	CA	150	100
4	10	103	O 2K -1	PB	100	65	9	13	106 N 4C -2	PB	-100	75	15	7	106 W 3SA +1	PA	-430	22
4	9	101	W 3SA -2	P10	200	85	9	11	102 N 4C -2	PB	-100	75	15	4	115 W 3SA +1	C3	-430	22
4	8	114	O 3SA -2	PB	200	85	9	4	103 N 3C -1	PB	-50	95	15	3	113 W 3SA +1	P8	-430	22
4	2	102	W 3SA -3	P10	300	100	9	12	104 N 3C -1	PB	-50	95	15	15	107 W 3SA +1	PA	-430	22
5	9	115	O 2P +1	CD	-140	0	10	5	105 W 3SA =	P7	-600	5	15	14	105 W 3SA +1	C2	-430	22
5	12	106	S 4C -1	KA	-100	10	10	12	104 W 3SA =	P7	-600	5	15	5	102 W 3SA =	PA	-400	56
5	11	104	O 5T -1	CD	50	20	10	4	103 S 2P -2	C6	-200	30	15	2	111 N 3C X -1	K3	-200	67
5	14	110	W 4K -3	C2	150	30	10	1	112 S 2P -2	KK	-200	30	15	1	109 W 2SA =	C3	-120	83
5	3	103	S 3C +1	KA	170	45	10	14	108 S 2P -2	KA	-200	30	15	13	103 W 1SA +1	PA	-120	83
5	13	108	S 2C +2	KA	170	45	10	2	114 W 1SA +2	P7	-150	55	15	8	108 W 5K -2	PA	100	100
5	2	101	W 4K -4	CK	200	65	10	13	106 W 2SA +1	P2	-150	55	16	7	106 S 3K -4	CK	-200	0
5	8	113	S 3C +2	KK	200	65	10	15	110 W 2SA =	P2	-120	80	16	8	108 W 2C +2	KB	-170	22
5	10	102	W 4K X -3	C3	500	80	10	11	102 W 1SA +1	P7	-120	80	16	5	102 W 3C +1	T8	-170	22
5	1	114	S 4C =	KA	620	95	10	10	115 W 1SA +1	P7	-120	80	16	4	115 W 3C +1	KB	-170	22
5	15	112	S 4C =	K9	620	95	10	3	101 O 2SA -1	TA	100	100	16	15	107 W 3C =	TB	-140	50
6	10	102	W 3SA +1	T7	-630	0	11	13	105 O 1SA +1	P5	-120	0	16	14	105 W 2P +1	TB	-140	50
6	1	114	W 3SA =	K4	-600	40	11	15	109 W 2P =	TA	-110	22	16	3	113 N 3T -2	C4	-100	67

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 02.12.2014**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	2	111	W 2C -1	KB	100	83	22	4	112 S 4P -1	T6	-50	17	27	11	108 S 4P +1	C6	450	78
16	13	103	W 4C -1	TB	100	83	22	5	114 O 4T -1	C9	100	33	27	10	106 S 4P +1	C4	450	78
16	1	109	W 3C -3	KB	300	100	22	11	111 S 2P +1	T6	140	44	27	5	111 S 4P +2	P5	480	100
17	9	109	O 2C +2	P7	-170	0	22	3	110 S 3P +1	T3	170	56	28	11	108 O 3P X =	C9	-530	0
17	4	114	O 3C =	K2	-140	17	22	10	109 S 4P +1	T6	450	83	28	13	112 O 2P =	C7	-110	11
17	15	106	W 2C +1	T7	-140	17	22	9	107 S 4P +1	T4	450	83	28	8	102 O 4P -2	T3	100	22
17	5	101	W 2SA =	P4	-120	33	22	8	105 S 4P +1	T6	450	83	28	9	104 O 4P -3	C9	150	33
17	7	105	O 4C -1	P6	50	61	22	2	108 S 4P +1	T6	450	83	28	5	111 N 3C +1	PB	170	50
17	3	112	O 4C -1	K2	50	61	23	10	108 S 5T +1	PK	620	11	28	4	109 N 2C +2	T5	170	50
17	2	110	W 2SA -1	KD	50	61	23	7	102 S 5T +1	PK	620	11	28	12	110 N 4C =	PB	620	78
17	1	108	W 1SA -1	KD	50	61	23	2	107 S 5T +1	KA	620	11	28	10	106 N 4C =	PB	620	78
17	8	107	W 4C X -1	P4	100	89	23	5	113 N 4C +1	KD	650	33	28	7	115 N 4C =	PB	620	78
17	14	104	S 2K +2	CB	130	100	23	3	109 S 4C +2	P8	680	44	28	14	114 N 4C +1	PB	650	100
18	5	101	N 3P -3	CA	-300	0	23	4	111 S 4SA +2	P8	690	56	29	13	111 N 4C X -4	T10	-1100	0
18	9	109	O 3K +1	PA	-130	33	23	12	112 S 4C +3	K5	710	83	29	15	115 N 3SA X -	CB	-200	11
18	7	105	O 2K +2	PA	-130	33	23	11	110 S 4C +3	PK	710	83	29	9	103 N 3SA -1	CB	-100	22
18	3	112	O 3K +1	PA	-130	33	23	9	106 S 4C +3	PK	710	83	29	7	114 N 2SA +1	CB	150	33
18	2	110	O 3K +1	PA	-130	33	23	8	104 N 4C +3	PB	710	83	29	12	109 W 3P -2	TA	200	44
18	15	106	O 2K +2	PA	-130	33	24	12	112 N 3C -2	K6	-100	11	29	5	110 W 3P X -2	C2	500	56
18	8	107	N 2P -1	K6	-100	67	24	9	106 N 4C -2	PB	-100	11	29	8	101 N 3SA =	C6	600	67
18	4	114	W 1SA =	P4	-90	78	24	4	111 N 3C -2	PB	-100	11	29	10	105 N 3SA X =	CB	750	78
18	1	108	O 5K -2	PA	100	94	24	11	110 N 3C -1	PB	-50	44	29	14	113 W 4P X -3	TA	800	94
18	14	104	O 3SA -2	P5	100	94	24	8	104 N 3C -1	PB	-50	44	29	11	107 W 4P X -3	C2	800	94
19	15	105	O 4C X =	TD	-790	0	24	7	102 N 3C -1	PB	-50	44	30	12	109 W 4C X +	K6	-690	0
19	9	108	O 3SA +1	T4	-630	11	24	10	108 N 2C =	PB	110	72	30	13	111 W 4C +1	P10	-450	17
19	10	110	N 1SA -3	CB	-150	28	24	5	113 N 2C =	KB	110	72	30	9	103 W 4C +1	KK	-450	17
19	7	104	O 2SA +1	T5	-150	28	24	2	107 W 3P -3	CA	150	89	30	15	115 W 4C =	KK	-420	56
19	8	106	W 3C =	TA	-140	44	24	3	109 N 2C +2	K4	170	100	30	11	107 W 4C =	KK	-420	56
19	5	115	O 1SA +1	T5	-120	56	25	11	109 N 5K -2	C8	-100	17	30	10	105 W 4C =	P3	-420	56
19	2	109	O 2C =	TD	-110	72	25	9	105 N 6T -2	C8	-100	17	30	8	101 W 4C =	KK	-420	56
19	1	107	W 2K +1	TA	-110	72	25	7	101 N 4K -2	C8	-100	17	30	5	110 W 4C =	PD	-420	56
19	4	113	W 3K -1	TA	100	94	25	4	110 N 4K -2	C8	-100	17	30	7	114 O 3C +2	KK	-200	89
19	3	111	O 3SA -1	T3	100	94	25	12	111 N 5T -1	C8	-50	56	30	14	113 O 4C -1	KK	50	100
20	5	115	O 3SA +2	C5	-660	0	25	10	107 S 3SA -1	CA	-50	56						
20	10	110	O 3SA +1	C2	-630	17	25	3	108 N 5T -1	C8	-50	56						
20	15	105	O 3SA +1	C5	-630	17	25	5	112 W 3C -1	TA	100	78						
20	9	108	N 2C -3	TK	-300	44	25	13	113 S 3SA =	C7	400	94						
20	4	113	N 2C -3	TK	-300	44	25	8	103 S 3SA =	CA	400	94						
20	1	107	N 2C -3	K9	-300	44	26	12	111 O 4C X =	K7	-790	0						
20	8	106	O 2SA +2	C5	-180	67	26	3	108 O 3SA +2	K7	-660	11						
20	7	104	O 3T +1	C5	-130	89	26	7	101 O 4C +1	K7	-650	22						
20	3	111	W 3K +1	C4	-130	89	26	13	113 O 4C =	K7	-620	39						
20	2	109	O 3T +1	C5	-130	89	26	4	110 O 4C =	K7	-620	39						
21	9	107	N 4C -2	KA	-200	11	26	5	112 W 3SA =	K3	-600	56						
21	7	103	N 4C -2	KA	-200	11	26	11	109 O 3C +1	PK	-170	67						
21	1	106	N 4C -2	KA	-200	11	26	10	107 W 3SA -2	K3	200	89						
21	11	111	S 3C -1	KA	-100	50	26	9	105 W 5T -2	CD	200	89						
21	5	114	N 3C -1	TA	-100	50	26	8	103 W 3SA -2	P9	200	89						
21	4	112	N 3C -1	TA	-100	50	27	9	104 S 4P -1	T5	-50	6						
21	2	108	N 3C -1	KA	-100	50	27	8	102 S 3SA -1	K4	-50	6						
21	10	109	O 1T +1	PA	-90	78	27	4	109 S 3SA =	P5	400	22						
21	8	105	N 2C =	KA	110	94	27	13	112 S 4P =	K4	420	44						
21	3	110	N 2C =	KA	110	94	27	12	110 S 4P =	T5	420	44						
22	1	106	S 4P -2	T6	-100	0	27	7	115 S 4P =	C6	420	44						
22	7	103	S 4P -1	T6	-50	17	27	14	114 N 4P +1	P6	450	78						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.