

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 11.11.2014**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	O 3SA +1	P9	-430	11	6	3	103 N 1SA -2	T10	-100	44	11	4	102 O 4P =	C9	-420	65
1	10	104	O 3SA +1	P5	-430	11	6	10	102 N 1SA -2	T10	-100	44	11	1	111 O 4P =	C9	-420	65
1	9	102	O 3SA +1	P9	-430	11	6	9	115 N 2C -2	P8	-100	44	11	11	101 O 4P =	C2	-420	65
1	15	114	O 4C =	P2	-420	44	6	2	101 N 1SA -1	T3	-50	78	11	14	107 W 2SA +1	C8	-150	90
1	12	108	O 4C =	TB	-420	44	6	12	106 S 1SA -1	PK	-50	78	11	6	106 O 4P -1	C9	50	100
1	8	115	O 4C =	P2	-420	44	6	8	113 N 1SA -1	T3	-50	78	12	6	106 O 4C +3	PA	-510	40
1	14	112	O 3SA =	T5	-400	67	6	15	112 O 2P -1	CB	100	100	12	5	104 O 4C +3	PA	-510	40
1	11	106	O 2SA +4	T5	-240	78	7	3	102 S 4C X -2	K10	-500	0	12	4	102 O 4C +3	K7	-510	40
1	7	113	N 2P -4	TK	-200	89	7	12	105 S 3C -2	K10	-200	10	12	2	113 O 4C +3	P7	-510	40
1	6	111	O 2SA +1	P8	-150	100	7	15	111 W 2SA +2	TB	-180	20	12	1	111 O 4C +3	PA	-510	40
2	10	104	S 4C -1	T8	-100	0	7	11	103 O 2SA +1	T2	-150	30	12	15	109 O 4C +3	K7	-510	40
2	11	106	S 3SA +1	T8	630	11	7	10	101 O 3P =	CA	-140	45	12	13	105 O 4C +3	PA	-510	40
2	8	115	N 4P +2	C5	680	22	7	9	114 O 3P =	CA	-140	45	12	12	103 O 4C +3	K7	-510	40
2	15	114	S 3SA +3	T5	690	39	7	13	107 S 2C -1	K10	-100	60	12	11	101 O 4C +3	P7	-510	40
2	12	108	S 5SA +1	T8	690	39	7	1	113 O 3P -1	KA	100	75	12	3	115 O 4C +2	K7	-480	90
2	14	112	S 5SA +2	P4	720	61	7	14	109 O 3P -1	T2	100	75	12	14	107 O 3C +4	PA	-260	100
2	9	102	S 3SA +4	P7	720	61	7	4	104 S 2C =	K10	110	90	13	7	107 W 3SA +2	K6	-660	6
2	1	101	N 6SA =	TB	1440	83	7	2	115 O 4P -2	T3	200	100	13	2	112 W 3SA +2	K6	-660	6
2	7	113	S 6SA =	T5	1440	83	8	3	102 O 3SA +2	C2	-460	10	13	6	105 O 4P +1	KA	-650	56
2	6	111	N 6P +1	TB	1460	100	8	12	105 O 3SA +2	C7	-460	10	13	5	103 O 4P +1	KA	-650	56
3	11	105	W 4C X =	TA	-790	0	8	11	103 O 3SA +2	C6	-460	10	13	4	101 O 4P +1	T10	-650	56
3	1	115	O 2C +1	K10	-140	25	8	2	115 O 3SA +1	C10	-430	35	13	3	114 O 4P +1	KA	-650	56
3	15	113	W 3C =	KA	-140	25	8	1	113 O 3SA +1	CB	-430	35	13	14	106 O 4P +1	KA	-650	56
3	14	111	O 3C =	K2	-140	25	8	13	107 O 2SA +2	C6	-180	50	13	13	104 O 4P +1	KA	-650	56
3	13	109	O 3C =	K2	-140	25	8	4	104 O 4P -1	C6	50	65	13	12	102 O 4P +1	KA	-650	56
3	12	107	O 4C -1	K10	100	70	8	9	114 O 3SA -1	CB	50	65	13	15	108 O 4P =	T10	-620	100
3	10	103	W 4C -1	TA	100	70	8	15	111 W 4P -2	C8	100	90	14	6	105 O 2P +1	C9	-140	0
3	9	101	O 2P -1	K10	100	70	8	14	109 O 4P -2	C8	100	90	14	7	107 O 2P =	T5	-110	33
3	8	114	W 4C -1	TA	100	70	8	10	101 W 3P -2	C8	100	90	14	5	103 O 2P =	TA	-110	33
3	7	112	O 4C -1	K2	100	70	9	4	103 S 4C -3	TK	-150	0	14	4	101 O 2P =	C9	-110	33
3	2	102	O 2P -4	K2	400	100	9	12	104 S 4C -1	P2	-50	11	14	2	112 O 2P =	C9	-110	33
4	2	102	N 3SA -1	CD	-100	10	9	10	115 N 3K +1	C5	130	22	14	14	106 O 2P =	TA	-110	33
4	10	103	N 3SA -1	K6	-100	10	9	3	101 S 2C +1	T10	140	39	14	3	114 O 2P -1	T5	50	78
4	9	101	N 2SA -1	CD	-100	10	9	14	108 S 2C +1	K8	140	39	14	15	108 O 3P -1	C9	50	78
4	15	113	O 3C -3	PD	300	30	9	13	106 W 4P -3	CA	300	56	14	13	104 O 2P -1	T7	50	78
4	1	115	N 3SA =	CD	600	50	9	1	112 N 3SA =	T10	400	67	14	12	102 O 4P -2	K9	100	100
4	14	111	N 3SA =	K6	600	50	9	2	114 S 4C =	T9	420	83	15	13	103 S 3P -2	KA	-200	0
4	13	109	N 3SA =	K6	600	50	9	11	102 S 4C =	TK	420	83	15	3	113 W 2K +1	P4	-110	15
4	12	107	N 3SA +1	K8	630	80	9	5	105 S 4C +1	P2	450	100	15	14	105 W 2K +1	PD	-110	15
4	11	105	N 3SA +1	K6	630	80	10	3	101 O 4P =	TD	-620	11	15	5	102 W 2K =	PD	-90	30
4	7	112	N 3SA +1	K4	630	80	10	14	108 O 4P =	KD	-620	11	15	15	107 W 2K -1	PD	50	40
4	8	114	N 3SA +2	P9	660	100	10	10	115 O 4P =	TD	-620	11	15	2	111 W 3K -2	PD	100	55
5	1	114	O 3C =	KA	-140	6	10	4	103 O 3P =	TD	-140	33	15	1	109 W 4K -2	CA	100	55
5	11	104	O 2C +1	K2	-140	6	10	13	106 O 2P =	TD	-110	44	15	6	104 S 3P =	KA	140	70
5	13	108	S 2T -1	C2	-100	28	10	5	105 O 4P -1	TD	100	72	15	8	108 W 4K -3	CA	150	85
5	12	106	S 2SA -1	CD	-100	28	10	2	114 O 4P -1	TD	100	72	15	4	115 W 4K -3	CA	150	85
5	15	112	N 2K =	CB	90	50	10	12	104 O 4P -1	TD	100	72	15	7	106 S 3P +1	KA	170	100
5	10	102	N 2K =	T9	90	50	10	11	102 O 4P -1	K8	100	72	16	3	113 N 4P -2	CA	-100	0
5	9	115	O 3C -2	T10	100	67	10	1	112 O 4P -2	TD	200	100	16	8	108 N 3P -1	T5	-50	45
5	3	103	N 4K =	C2	130	78	11	3	115 O 4P +2	C9	-480	0	16	7	106 N 3P -1	T5	-50	45
5	8	113	S 1SA +4	T5	210	89	11	13	105 O 4P +1	C5	-450	15	16	6	104 N 3P -1	T5	-50	45
5	2	101	S 3SA =	T6	600	100	11	12	103 O 4P +1	C9	-450	15	16	4	115 N 4P -1	T5	-50	45
6	1	114	O 1SA +1	CK	-120	11	11	2	113 W 3SA +1	C6	-430	35	16	2	111 N 3P -1	T5	-50	45
6	13	108	W 2SA =	K4	-120	11	11	15	109 W 3SA +1	C5	-430	35	16	1	109 N 3P -1	T5	-50	45
6	11	104	W 1SA +1	KB	-120	11	11	5	104 O 4P =	C2	-420	65	16	14	105 N 3P -1	T5	-50	45

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

# Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 11.11.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	13	103	N 3P -1	T5	-50	45	22	6	101 S 2K -1	C4	-50	17	27	5	111 W 3C +1	PD	-170	72
16	5	102	N 3P =	CA	140	95	22	2	108 S 1SA -1	P2	-50	17	27	7	115 S 3P -2	T4	-100	89
16	15	107	N 2P +1	C3	140	95	22	8	105 S 2K =	P2	90	44	27	8	102 S 2P =	T4	110	100
17	3	112	N 2SA -3	C3	-150	0	22	9	107 S 2K +1	CA	110	61	28	5	111 N 3C -4	P6	-400	0
17	9	109	W 1SA +1	T3	-120	17	22	1	106 S 2K +1	CA	110	61	28	9	104 N 3C -3	TA	-300	11
17	1	108	W 2SA =	T3	-120	17	22	10	109 S 1SA +1	C4	120	78	28	8	102 N 3C -2	P6	-200	28
17	14	104	W 2C =	TB	-110	33	22	5	114 O 2SA -2	P5	200	89	28	4	109 N 3C -2	P6	-200	28
17	6	103	N 1SA -2	P5	-100	44	22	4	112 S 2K X +1	CA	280	100	28	7	115 O 3K =	C5	-110	44
17	7	105	W 1SA =	T3	-90	56	23	10	108 W 6P =	KA	-1430	11	28	10	106 O 2K =	PA	-90	61
17	5	101	W 2C -1	K9	50	67	23	8	104 W 6P =	KA	-1430	11	28	6	113 O 2K =	C5	-90	61
17	4	114	W 2C -2	K9	100	78	23	5	113 W 6P =	KA	-1430	11	28	11	108 O 2SA -2	C4	100	78
17	8	107	N 1SA +1	KD	120	89	23	12	112 W 4P +2	T9	-680	44	28	14	114 N 2C =	TA	110	89
17	15	106	O 2P -3	T7	150	100	23	7	102 W 4P +2	P5	-680	44	28	13	112 O 2SA -3	C5	150	100
18	1	108	S 4T X -3	K5	-800	0	23	6	115 W 4P +2	T6	-680	44	29	15	115 W 6SA =	K7	-1440	0
18	8	107	N 4C -3	K6	-300	11	23	3	109 O 3SA +2	K3	-660	67	29	10	105 O 3SA +4	K8	-720	11
18	9	109	N 3SA -2	K3	-200	22	23	9	106 W 4P +1	T3	-650	89	29	13	111 O 3SA +3	K8	-690	28
18	7	105	O 2K +2	C2	-130	33	23	4	111 W 4P +1	T3	-650	89	29	7	114 O 3SA +3	K8	-690	28
18	3	112	O 3K =	C2	-110	50	23	2	107 W 4P +1	T4	-650	89	29	14	113 O 3SA +2	PD	-660	61
18	15	106	O 2K +1	P9	-110	50	24	5	113 W 3T =	K7	-110	0	29	12	109 O 3SA +2	K6	-660	61
18	6	103	N 4C -1	KK	-100	78	24	8	104 N 3K -2	T6	-100	17	29	9	103 O 3SA +2	K9	-660	61
18	4	114	N 3P -1	C8	-100	78	24	6	115 N 3K -2	P3	-100	17	29	8	101 O 3SA +2	KD	-660	61
18	14	104	N 3SA -1	K3	-100	78	24	12	112 N 2K -1	T6	-50	39	29	11	107 O 4SA =	K8	-630	94
18	5	101	S 3C =	T9	140	100	24	3	109 N 3K -1	P5	-50	39	29	6	112 O 3SA +1	K9	-630	94
19	7	104	O 4C =	K4	-620	6	24	10	108 W 2SA -1	P4	50	56	30	15	115 W 4P +1	KB	-450	17
19	5	115	O 4C =	K4	-620	6	24	7	102 W 2SA -2	KA	100	67	30	12	109 W 4P +1	KB	-450	17
19	4	113	O 2C +3	K2	-200	22	24	9	106 W 2SA -3	K7	150	78	30	9	103 W 4P +1	C10	-450	17
19	9	108	W 2SA +1	P4	-150	33	24	2	107 S 2SA +2	T7	180	89	30	6	112 W 4P +1	K9	-450	17
19	15	105	O 2P +1	K5	-140	44	24	4	111 O 2C -5	KB	250	100	30	13	111 W 4P =	C10	-420	61
19	8	106	W 2SA =	P4	-120	56	25	8	103 O 4P =	C10	-620	0	30	11	107 W 4P =	C10	-420	61
19	1	107	O 2C =	K5	-110	67	25	9	105 O 3P +2	C10	-200	11	30	10	105 W 4P =	T5	-420	61
19	6	102	O 4C -2	K6	200	83	25	13	113 O 2P +2	C10	-170	39	30	7	114 W 4P =	KB	-420	61
19	2	109	O 3C -2	K5	200	83	25	11	109 O 2P +2	C4	-170	39	30	14	113 W 4P -1	KB	50	94
19	3	111	O 4C -3	K2	300	100	25	6	114 O 2P +2	T6	-170	39	30	8	101 W 4P -1	KB	50	94
20	5	115	S 3T -2	K7	-200	0	25	5	112 O 3P +1	C10	-170	39						
20	9	108	O 2K +1	TA	-110	17	25	12	111 N 3C -2	K3	-100	67						
20	15	105	O 2K +1	TA	-110	17	25	7	101 N 2C -1	K2	-50	83						
20	4	113	O 2K =	TA	-90	33	25	3	108 N 3C -1	K2	-50	83						
20	2	109	Pass		0	44	25	10	107 O 4P -1	KA	100	100						
20	1	107	S 2T =	CA	90	56	26	6	114 S 4C X -3	P6	-800	0						
20	8	106	O 2K -1	TA	100	83	26	7	101 O 4P +1	TB	-650	17						
20	7	104	O 2K -1	TK	100	83	26	5	112 O 4P +1	CK	-650	17						
20	6	102	W 2C -1	T9	100	83	26	3	108 O 4P =	C2	-620	33						
20	3	111	O 2P -1	TA	100	83	26	10	107 S 4C -2	P6	-200	50						
21	7	103	O 4C =	P5	-420	0	26	9	105 S 4C X -1	P10	-200	50						
21	1	106	O 3C +1	P8	-170	11	26	13	113 O 3P =	TB	-140	67						
21	10	109	O 4C -1	KA	50	39	26	12	111 S 4C -1	P10	-100	83						
21	8	105	O 4C -1	KA	50	39	26	11	109 S 3C -1	P6	-100	83						
21	6	101	O 4C -1	KA	50	39	26	8	103 S 4C +1	P10	650	100						
21	5	114	W 3SA -1	P6	50	39	27	14	114 W 4C =	P6	-420	28						
21	11	111	O 4C -2	P5	100	83	27	13	112 O 4C =	PA	-420	28						
21	9	107	O 4C -2	KA	100	83	27	11	108 W 4C =	P6	-420	28						
21	4	112	O 4C -2	P5	100	83	27	10	106 W 4C =	PD	-420	28						
21	2	108	O 4C -2	T6	100	83	27	9	104 W 4C =	PD	-420	28						
22	11	111	S 3K -1	P2	-50	17	27	4	109 W 4C =	PD	-420	28						
22	7	103	S 3K -1	P2	-50	17	27	6	113 W 3C +1	PD	-170	72						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.