

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 04.11.2014**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	12	108	W 3C +1	P3	-170	0	6	2	101 S 3P =	KD	140	50	11	3	115 O 2T -1	PA	50	45
1	15	114	N 4P -3	TK	-150	11	6	11	104 S 3P =	KD	140	50	11	15	109 O 3T -1	PA	50	45
1	1	101	W 2C +1	KB	-140	33	6	8	113 S 3P =	KD	140	50	11	1	111 S 2C =	KA	110	70
1	13	110	W 2C +1	KB	-140	33	6	9	115 S 3P +2	CA	200	70	11	12	103 S 2C =	TA	110	70
1	11	106	W 3C =	P3	-140	33	6	15	112 S 4P =	KD	420	80	11	11	101 S 2C =	KA	110	70
1	6	111	N 3P -1	TA	-50	56	6	3	103 S 4P +1	KD	450	95	11	4	102 N 1SA +1	T9	120	90
1	14	112	W 4C -1	KB	50	72	6	14	110 S 4P +1	KD	450	95	11	5	104 S 2C +1	K5	140	100
1	10	104	W 4C -1	KB	50	72	7	11	103 O 3SA +3	K10	-690	0	12	14	107 O 4C +3	KK	-510	0
1	8	115	W 4C -2	KB	100	89	7	9	114 O 3SA +2	K3	-660	10	12	15	109 O 4C +2	PA	-480	10
1	9	102	N 2P =	TA	110	100	7	12	105 O 4P +1	T6	-650	20	12	6	106 O 4C +1	K3	-450	55
2	14	112	W 2K =	TK	-90	0	7	3	102 O 4P =	K2	-620	35	12	5	104 O 4C +1	KK	-450	55
2	15	114	W 2T -1	CA	50	33	7	1	113 O 4P =	K2	-620	35	12	3	115 O 4C +1	KK	-450	55
2	12	108	W 1K -1	TK	50	33	7	10	101 N 3SA -3	CK	-300	50	12	2	113 O 4C +1	KK	-450	55
2	10	104	W 1SA -1	TK	50	33	7	13	107 O 2C +2	P9	-170	60	12	1	111 O 4C +1	KK	-450	55
2	9	102	W 1SA -1	TK	50	33	7	4	104 O 3P =	K3	-140	75	12	13	105 O 4C +1	C6	-450	55
2	8	115	O 2P -1	T9	50	33	7	15	111 W 2C +1	PA	-140	75	12	12	103 O 4C +1	KK	-450	55
2	1	101	W 2T -2	TK	100	72	7	2	115 W 4C -1	K5	100	95	12	11	101 O 4C +1	KK	-450	55
2	6	111	W 1SA -2	P10	100	72	7	14	109 O 4P -1	K7	100	95	12	4	102 O 3C =	KK	-140	100
2	13	110	W 2SA -3	TK	150	94	8	15	111 S 2SA -2	P8	-100	15	13	14	106 S 2K =	TD	90	0
2	11	106	W 2P -3	TK	150	94	8	12	105 S 4C X -1	KA	-100	15	13	6	105 W 2P -1	KB	100	22
3	15	113	S 3P +3	T2	230	0	8	11	103 S 4C -2	P4	-100	15	13	5	103 W 2P -1	KB	100	22
3	14	111	S 4P +1	KA	450	22	8	9	114 S 4C -2	P8	-100	15	13	3	114 W 2P -1	KB	100	22
3	11	105	S 5P =	C4	450	22	8	4	104 N 3C -1	T4	-50	45	13	1	110 N 2T +1	PB	110	44
3	9	101	S 5P =	C6	450	22	8	14	109 N 2SA -1	T8	-50	45	13	2	112 N 3T +1	P6	130	56
3	8	114	S 5P +1	KA	480	44	8	13	107 W 3P -1	TA	50	60	13	12	102 S 2C +1	P10	140	67
3	2	102	S 6P =	K7	980	78	8	3	102 N 1C +2	K3	140	85	13	4	101 S 3C +1	PA	170	78
3	1	115	S 6P =	KA	980	78	8	2	115 S 2C +1	KA	140	85	13	15	108 W 3P -2	TA	200	89
3	13	109	S 6P =	KA	980	78	8	1	113 N 2C +1	PB	140	85	13	13	104 W 3P -3	KB	300	100
3	12	107	S 6P =	KA	980	78	8	10	101 S 3C =	KA	140	85	14	6	105 N 3SA -3	P7	-150	6
3	10	103	S 6P =	KA	980	78	9	2	114 O 1SA +3	P6	-180	5	14	5	103 N 3SA -3	P7	-150	6
4	15	113	N 3SA -2	K9	-200	0	9	14	108 O 2SA +2	PD	-180	5	14	2	112 N 3SA -2	P8	-100	33
4	10	103	N 3SA -1	C7	-100	17	9	5	105 O 2SA +1	PD	-150	30	14	1	110 S 4T -2	P2	-100	33
4	9	101	N 3SA -1	K6	-100	17	9	3	101 O 1SA +2	CB	-150	30	14	15	108 N 3SA -2	P10	-100	33
4	1	115	N 1SA +2	K5	150	44	9	15	110 O 2T +3	K3	-150	30	14	3	114 S 3T -1	P2	-50	61
4	13	109	N 2SA +1	T7	150	44	9	4	103 N 2P -1	CA	-50	55	14	14	106 N 3SA -1	K7	-50	61
4	12	107	N 1SA +2	K6	150	44	9	10	115 S 2P -1	C6	-50	55	14	12	102 S 3T =	C10	110	78
4	14	111	N 1SA +3	K9	180	67	9	1	112 W 4C -1	T8	100	70	14	4	101 S 3SA +2	K3	460	94
4	11	105	S 3SA =	C5	600	83	9	13	106 W 4C X -1	PA	200	85	14	13	104 S 3SA +2	K2	460	94
4	8	114	N 3SA =	C10	600	83	9	12	104 O 1SA -2	PD	200	85	15	3	113 W 3SA +2	C2	-460	0
4	2	102	N 3SA +1	K6	630	100	9	11	102 W 2C -3	P2	300	100	15	6	104 O 3SA +1	P7	-430	17
5	13	108	N 2K -1	P4	-100	0	10	12	104 N 3C -2	T10	-200	0	15	15	107 W 3SA +1	C2	-430	17
5	11	104	W 1SA =	K2	-90	10	10	4	103 O 3K =	C10	-110	15	15	8	108 O 3SA =	P5	-400	50
5	3	103	O 2P -1	T6	50	50	10	2	114 O 3K =	C10	-110	15	15	4	115 O 3SA =	P5	-400	50
5	2	101	W 1SA -1	K2	50	50	10	1	112 N 3C -1	KA	-100	35	15	1	109 O 3SA =	P8	-400	50
5	1	114	W 1SA -1	K2	50	50	10	15	110 N 3C -1	T10	-100	35	15	14	105 O 3SA =	K7	-400	50
5	15	112	O 2P -1	KA	50	50	10	14	108 O 3K -1	C10	100	55	15	5	102 O 1SA +1	P5	-120	78
5	14	110	W 1SA -1	K2	50	50	10	10	115 O 3K -1	C10	100	55	15	2	111 O 1SA -1	P5	50	94
5	9	115	W 1SA -1	K3	50	50	10	3	101 N 2C =	T10	110	70	15	13	103 O 3SA -1	P9	50	94
5	8	113	W 1SA -1	K2	50	50	10	11	102 N 2C +2	KA	170	80	16	13	103 N 5K X -3	CK	-500	0
5	12	106	O 2P -2	K4	100	90	10	13	106 N 3C +2	KA	200	90	16	15	107 N 4K X -2	CK	-300	11
5	10	102	S 2C =	T10	110	100	10	5	105 W 3SA X	CA	800	100	16	3	113 S 4P -5	CA	-250	22
6	1	114	S 4P -1	T5	-50	15	11	6	106 S 4P X -3	KA	-500	0	16	4	115 S 5P -4	TA	-200	33
6	13	108	S 4P -1	KD	-50	15	11	2	113 O 3T +1	P7	-130	10	16	1	109 N 4K -3	CK	-150	50
6	12	106	S 4P -1	CA	-50	15	11	14	107 S 2C -2	K5	-100	20	16	14	105 N 3T -3	CK	-150	50
6	10	102	S 4P -1	K10	-50	15	11	13	105 S 3C -1	TA	-50	30	16	8	108 W 3C =	KA	-140	67

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.

# Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 04.11.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
16	6	104	N 4K -2	CK	-100	78	22	8	105 O 2P =	C5	-110	28	27	10	106 O 2P -3	TB	150	72
16	2	111	N 2K =	CK	90	89	22	4	112 O 2P =	C5	-110	28	27	8	102 O 2P -4	TB	200	89
16	5	102	W 4C -2	KA	200	100	22	3	110 O 2P =	TD	-110	28	27	6	113 W 4C -5	PB	250	100
17	9	109	W 2K +1	T3	-110	17	22	6	101 N 3C -2	PA	-100	56	28	8	102 S 6C -1	T7	-100	6
17	8	107	W 2K +1	T6	-110	17	22	11	111 N 2C -1	P9	-50	67	28	6	113 S 6C -1	T6	-100	6
17	6	103	W 2K +1	T2	-110	17	22	9	107 O 3P -1	K8	100	78	28	14	114 S 4C +1	T9	650	50
17	4	114	W 2K +1	P3	-110	17	22	5	114 O 3P -2	CB	200	94	28	13	112 S 4C +1	T9	650	50
17	15	106	W 2K =	C2	-90	44	22	1	106 W 3K -2	TA	200	94	28	12	110 N 5C =	KA	650	50
17	5	101	N 3C -1	K7	-50	61	23	11	110 W 4P +1	K3	-650	6	28	11	108 S 5C =	T4	650	50
17	14	104	S 1SA -1	KA	-50	61	23	5	113 W 4P +1	TA	-650	6	28	9	104 S 4C +1	T9	650	50
17	3	112	W 3K -1	T6	50	83	23	9	106 W 4P =	TA	-620	22	28	5	111 S 4C +1	T9	650	50
17	2	110	W 3K -1	C5	50	83	23	12	112 W 3P +2	C4	-200	50	28	10	106 S 5C +1	K6	680	94
17	1	108	N 3C =	KB	140	100	23	8	104 W 2P +3	TA	-200	50	28	4	109 S 5C +1	K6	680	94
18	1	108	O 3SA +3	T2	-490	0	23	3	109 O 3P +2	TA	-200	50	29	12	109 W 4C +1	PK	-650	11
18	9	109	O 3SA +2	P2	-460	44	23	2	107 W 3P +2	K5	-200	50	29	10	105 W 4C +1	PK	-650	11
18	8	107	O 3SA +2	P2	-460	44	23	4	111 W 3P +1	K5	-170	78	29	8	101 W 4C +1	PK	-650	11
18	6	103	O 5SA =	T5	-460	44	23	6	115 S 2K =	T6	90	89	29	13	111 W 4C =	PK	-620	33
18	5	101	O 3SA +2	T3	-460	44	23	10	108 S 2T +2	PK	130	100	29	14	113 W 2C +3	PK	-200	56
18	4	114	W 3SA +2	T6	-460	44	24	10	108 S 4K -1	C2	-50	6	29	11	107 W 3C +2	PK	-200	56
18	3	112	O 3SA +2	T3	-460	44	24	2	107 S 4K -1	TK	-50	6	29	9	103 W 3C +2	PK	-200	56
18	15	106	O 3SA +2	T3	-460	44	24	3	109 O 4P -2	K6	100	22	29	15	115 W 2SA +2	PK	-180	78
18	14	104	W 3SA =	C5	-400	89	24	12	112 S 3K +1	T5	130	61	29	6	112 N 3P -1	KA	-100	94
18	2	110	W 4SA -3	C5	150	100	24	11	110 S 4K =	P5	130	61	29	5	110 N 3P -1	KA	-100	94
19	9	108	S 3SA -1	CB	-50	0	24	9	106 S 2K +2	T3	130	61	30	13	111 N 4P -4	CD	-200	0
19	4	113	S 2T =	P4	90	11	24	8	104 S 4K =	C2	130	61	30	9	103 S 4P -3	K6	-150	11
19	8	106	N 2K +1	T6	110	33	24	6	115 S 4K =	CD	130	61	30	15	115 W 2C =	PA	-110	22
19	3	111	S 3T =	CA	110	33	24	5	113 S 4K =	P5	130	61	30	12	109 S 3P -2	K6	-100	33
19	15	105	N 3T =	P6	110	33	24	4	111 S 3K +2	PB	150	100	30	11	107 S 2P -1	K6	-50	56
19	10	110	S 2SA +1	CB	150	61	25	8	103 S 3SA -3	K3	-150	0	30	6	112 N 3P -1	CD	-50	56
19	1	107	N 2SA +1	P3	150	61	25	4	110 N 3SA -2	T7	-100	11	30	5	110 S 3P -1	K6	-50	56
19	5	115	N 3SA =	P2	400	83	25	9	105 S 1SA -1	K4	-50	22	30	10	105 W 3C -2	PA	100	78
19	2	109	N 3SA =	P3	400	83	25	5	112 S 1SA =	K3	90	33	30	8	101 S 2P =	K6	110	89
19	6	102	N 3SA +1	P3	430	100	25	11	109 S 1SA +1	C4	120	56	30	14	113 S 3P +1	CA	170	100
20	10	110	N 5C +1	P6	680	39	25	6	114 S 2SA =	C4	120	56						
20	9	108	N 4C +2	K9	680	39	25	3	108 S 2SA =	C4	120	56						
20	6	102	N 4C +2	K3	680	39	25	12	111 N 2P +1	KA	140	78						
20	5	115	N 4C +2	K9	680	39	25	10	107 N 2SA +2	T5	180	89						
20	3	111	N 4C +2	K9	680	39	25	13	113 N 3SA =	T5	400	100						
20	2	109	N 4C +2	K2	680	39	26	9	105 O 2P -1	CA	100	0						
20	1	107	N 4C +2	K7	680	39	26	10	107 S 2K +1	P2	110	11						
20	15	105	S 4C +2	T8	680	39	26	11	109 S 2K +2	P9	130	28						
20	8	106	N 6C =	P6	1430	94	26	6	114 S 3K +1	PA	130	28						
20	4	113	N 6C =	P3	1430	94	26	12	111 N 2C +1	PA	140	50						
21	4	112	O 3P +1	T5	-170	0	26	8	103 N 2C +1	PA	140	50						
21	9	107	O 2P +1	T5	-140	28	26	13	113 N 3C +1	PA	170	72						
21	5	114	O 3C =	K9	-140	28	26	3	108 N 2C +2	PA	170	72						
21	3	110	O 3C =	KA	-140	28	26	5	112 N 3SA =	PA	600	94						
21	2	108	O 3P =	K6	-140	28	26	4	110 N 3SA =	PA	600	94						
21	10	109	O 2P =	T6	-110	56	27	14	114 O 2C =	TB	-110	0						
21	6	101	S 3K -1	C8	-100	67	27	12	110 S 2T -2	KA	-100	11						
21	8	105	O 3P -1	KA	50	83	27	9	104 S 2C -1	P6	-50	22						
21	1	106	O 3C -1	KA	50	83	27	11	108 W 2SA -1	T10	50	33						
21	11	111	S 2K +1	C8	110	100	27	4	109 W 2SA -2	PB	100	44						
22	2	108	N 3C -3	PA	-150	0	27	5	111 N 2P =	K10	110	56						
22	10	109	O 2P =	K2	-110	28	27	13	112 O 3C -3	TB	150	72						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.