

# Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 16.09.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	13	111	S 3P X -4	C2	-800	0	6	11	105 N 4P +3	KA	510	39	12	13	105 W 3SA =	K2	-400	0
1	9	103	W 4C +1	TA	-450	11	6	8	112 N 4P +3	KA	510	39	12	6	106 W 2SA +1	K2	-150	22
1	10	105	W 4C =	PA	-420	22	6	13	109 S 6C +1	K5	1010	89	12	2	112 W 2SA +1	C10	-150	22
1	7	112	N 5T X -2	C9	-300	33	6	12	107 N 6P +1	KA	1010	89	12	12	103 O 2SA +1	C6	-150	22
1	6	110	W 3C +1	P6	-170	44	6	10	102 N 6P +1	KA	1010	89	12	5	104 W 2SA =	K2	-120	50
1	14	113	W 3C =	TA	-140	56	7	3	102 W 4P +1	KA	-650	6	12	14	108 O 2SA =	C4	-120	50
1	11	107	S 3P -2	CA	-100	67	7	14	110 W 4P +1	KA	-650	6	12	10	113 Pass		0	67
1	1	101	S 2P -1	CA	-50	83	7	4	104 W 4P =	KA	-620	44	12	4	102 W 3T -1	C10	50	89
1	5	108	S 3P -1	CK	-50	83	7	1	112 W 4P =	KA	-620	44	12	1	110 O 2SA -1	C4	50	89
1	12	109	W 3C -1	PA	50	100	7	11	103 W 4P =	KA	-620	44	12	11	101 O 2SA -1	K7	50	89
2	9	103	N 2SA -3	KK	-300	0	7	9	113 W 4P =	KA	-620	44	13	7	107 N 3P -1	K8	-100	0
2	13	111	S 2C -1	K7	-100	11	7	8	111 W 4P =	KA	-620	44	13	3	113 W 2K =	T8	-90	11
2	11	107	W 2SA -1	CB	50	22	7	13	108 N 5T -2	PA	-200	78	13	2	111 N 3T +1	K4	130	22
2	14	113	O 3K -2	CK	100	44	7	10	101 W 3P +1	KA	-170	89	13	1	109 N 1SA +4	K6	210	33
2	12	109	O 2K -2	P6	100	44	7	12	106 S 5K -1	CA	-100	100	13	5	103 S 3SA =	KK	600	50
2	6	110	W 2SA -2	CB	100	44	8	14	110 O 3SA +1	K5	-430	6	13	4	101 S 3SA =	KK	600	50
2	10	105	S 2C =	P7	110	67	8	8	111 W 3SA +1	P4	-430	6	13	13	104 S 3SA +1	K9	630	67
2	1	101	N 1SA +2	KK	150	89	8	4	104 W 3SA =	C10	-400	44	13	6	105 N 3SA +2	K6	660	89
2	7	112	W 2P -3	CB	150	89	8	3	102 W 3SA =	C3	-400	44	13	14	106 N 3SA +2	K2	660	89
2	5	108	O 3T -3	C4	150	89	8	11	103 W 3SA =	C3	-400	44	13	12	102 N 3SA +2	K5	660	89
3	7	111	W 6C =	KA	-1430	0	8	10	101 W 3SA =	C3	-400	44	14	3	113 N 5K -4	PK	-200	0
3	13	110	W 4C +2	T2	-680	28	8	9	113 W 3SA =	C3	-400	44	14	14	106 S 3SA -3	T3	-150	17
3	12	108	O 4C +2	KA	-680	28	8	1	112 W 3SA -1	C3	50	89	14	12	102 N 4P -3	K6	-150	17
3	10	104	W 4C +2	T2	-680	28	8	13	108 W 3SA -1	C3	50	89	14	6	105 S 3SA -2	T7	-100	39
3	9	101	W 4C +2	P2	-680	28	8	12	106 O 3SA -1	K6	50	89	14	5	103 S 2SA -2	T7	-100	39
3	2	102	W 4C +1	T2	-650	67	9	5	105 O 2SA +3	T2	-210	0	14	7	107 S 2SA -1	K3	-50	61
3	14	112	W 4C +1	T2	-650	67	9	2	113 O 2P +2	CD	-170	11	14	13	104 S 3C -1	PK	-50	61
3	8	113	W 4C +1	C2	-650	67	9	14	109 N 4C -3	PA	-150	28	14	2	111 S 2SA +1	K3	150	78
3	11	106	W 4C =	T4	-620	89	9	9	112 S 3C -3	T5	-150	28	14	1	109 S 2SA +2	KA	180	89
3	6	109	O 3SA -1	P9	100	100	9	3	101 O 2T +1	C7	-110	50	14	4	101 S 3SA =	T7	400	100
4	11	106	S 2P -2	C5	-200	6	9	1	111 O 3T =	CD	-110	50	15	7	106 W 4P =	C10	-420	11
4	7	111	N 3P -2	CK	-200	6	9	12	104 N 3C -2	TK	-100	72	15	14	105 W 4P =	KA	-420	11
4	13	110	S 2P -1	C3	-100	33	9	11	102 S 2K -2	T5	-100	72	15	12	101 W 4P =	C3	-420	11
4	10	104	S 3P -1	C5	-100	33	9	13	107 S 2C =	T5	110	89	15	6	104 W 3P +1	T5	-170	33
4	8	113	S 2P -1	C5	-100	33	9	4	103 W 4P -3	KB	300	100	15	8	108 W 3P =	C3	-140	50
4	12	108	N 1SA =	CK	90	56	10	5	105 O 6SA +1	K7	-1470	6	15	3	112 W 3P =	C10	-140	50
4	2	102	O 2C -1	PD	100	78	10	9	112 O 6SA +1	K9	-1470	6	15	2	110 W 5P -1	C10	50	72
4	14	112	O 2C -1	PD	100	78	10	12	104 O 6SA =	CA	-1440	22	15	13	103 W 4P -1	T6	50	72
4	6	109	O 2C -1	T5	100	78	10	4	103 W 6T =	C6	-1370	33	15	5	102 S 3C +2	PA	200	89
4	9	101	S 2P =	KK	110	100	10	2	113 O 3SA +3	K7	-690	56	15	1	107 S 5C =	PA	650	100
5	3	103	W 2P +1	CB	-140	17	10	14	109 O 3SA +3	K7	-690	56	16	3	112 W 4C X =	KK	-790	0
5	1	113	W 2P +1	CB	-140	17	10	11	102 O 3SA +3	K9	-690	56	16	8	108 W 3C X =	PB	-730	11
5	12	107	W 3P =	CB	-140	17	10	13	107 O 3SA +2	P7	-660	78	16	14	105 W 3C +2	KA	-200	22
5	7	110	W 3P =	CB	-140	17	10	3	101 W 4T +1	P2	-150	89	16	7	106 W 2C +1	KA	-140	39
5	10	102	O 2C =	K5	-110	44	10	1	111 W 6T -1	T7	100	100	16	6	104 W 3C =	KA	-140	39
5	14	111	W 4P -1	TA	50	67	11	6	106 W 3P =	C4	-140	11	16	1	107 S 4K -1	PA	-50	56
5	11	105	W 2P -1	K4	50	67	11	1	110 W 2P +1	T4	-140	11	16	13	103 S 2P +1	CK	140	67
5	8	112	W 3P -1	K4	50	67	11	11	101 W 2P +1	C4	-140	11	16	5	102 W 4C X -2	KA	500	89
5	2	101	O 4P -2	K7	100	94	11	5	104 N 3T -2	CA	-100	50	16	2	110 W 4C X -2	KA	500	89
5	13	109	W 4P -2	K6	100	94	11	4	102 N 2SA -2	KA	-100	50	16	12	101 W 5C X -2	KA	500	89
6	7	110	N 4P +1	KA	450	0	11	14	108 N 2SA -2	P3	-100	50	17	3	111 O 1P +2	T3	-140	0
6	3	103	N 4P +3	KA	510	39	11	12	103 N 2SA -2	K5	-100	50	17	6	103 O 2P =	C4	-110	10
6	2	101	N 5P +2	KA	510	39	11	13	105 N 1SA -1	K6	-50	78	17	1	106 N 4C -2	T4	-100	20
6	1	113	N 4P +3	KA	510	39	11	10	113 O 3K -1	P2	50	89	17	14	104 W 1SA =	C6	-90	30
6	14	111	N 4P +3	KA	510	39	11	2	112 O 3SA -3	T7	150	100	17	9	109 O 2P -1	TK	50	55

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

**Board-Anschriften (aus Sicht NS), Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 16.09.2014**

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
17	7	105	O 2P -1	T3	50	55	22	6	101 W 3SA -1	T5	100	70	27	5	109 N 4C =	TA	420	83
17	5	101	O 2P -1	C3	50	55	22	3	108 O 4P -1	TB	100	70	28	12	110 N 1SA -2	KB	-200	0
17	4	113	W 1SA -1	C6	50	55	22	1	104 W 3SA -1	T3	100	70	28	4	107 W 1SA =	T2	-90	11
17	8	107	N 2C =	P5	110	85	22	2	106 W 4P -2	T5	200	100	28	11	108 W 2C -1	P7	50	33
17	2	108	N 2C =	P5	110	85	23	3	107 N 4SA -4	C10	-400	0	28	10	106 W 2C -1	TA	50	33
17	13	102	S 2C +1	P7	140	100	23	9	106 N 2P -2	C10	-200	11	28	7	113 W 3K -1	C10	50	33
18	7	105	N 3K -3	CK	-300	0	23	11	110 S 3T -1	KA	-100	28	28	9	104 W 1SA -2	TA	100	61
18	8	107	O 3C +1	K8	-170	25	23	7	102 N 3SA -1	K5	-100	28	28	5	109 W 2C -2	P3	100	61
18	6	103	O 2C +2	TK	-170	25	23	8	104 S 2SA =	C5	120	56	28	13	112 N 3T =	KB	110	78
18	5	101	O 2C +2	T8	-170	25	23	5	111 S 1SA +1	KA	120	56	28	8	102 N 2T +2	KB	130	89
18	13	102	O 2C +2	TK	-170	25	23	2	105 S 1SA +1	C6	120	56	28	6	111 S 1SA X =	PK	180	100
18	1	106	O 2C +1	TK	-140	55	23	4	109 S 4T =	KA	130	78						
18	14	104	O 2C +1	PA	-140	55	23	10	108 S 1SA +2	P7	150	89						
18	3	111	O 2C =	K8	-110	75	23	12	112 W 2P X -3	PA	800	100						
18	2	108	O 2C =	TK	-110	75	24	10	108 S 3T X -3	K8	-500	0						
18	4	113	O 2C -1	TK	50	90	24	4	109 O 4C +1	PB	-450	11						
18	9	109	O 3C -2	TK	100	100	24	12	112 O 4C =	PB	-420	33						
19	3	109	N 3T -4	CA	-200	0	24	8	104 O 4C =	TK	-420	33						
19	2	107	S 1SA -3	PB	-150	17	24	7	102 W 4C =	TB	-420	33						
19	14	103	S 1SA -3	PB	-150	17	24	2	105 W 3C +2	TB	-200	56						
19	7	104	N 2C -2	K9	-100	39	24	11	110 W 2C +2	TB	-170	72						
19	6	102	S 2K -2	P9	-100	39	24	3	107 W 3C +1	P5	-170	72						
19	10	110	N 2C -1	PA	-50	67	24	9	106 W 3C =	TB	-140	89						
19	8	106	S 1SA -1	PB	-50	67	24	5	111 O 3K -1	PB	50	100						
19	1	105	S 3K -1	PB	-50	67	25	5	110 W 2P +2	TB	-170	5						
19	4	112			0	89	25	4	108 W 2P +2	C5	-170	5						
19	9	108	S 2SA =	C3	120	100	25	13	113 W 3P =	C5	-140	40						
20	8	106	N 4C -1	T7	-100	6	25	12	111 W 2P +1	P6	-140	40						
20	14	103	N 5C -1	PK	-100	6	25	10	107 W 2P +1	C5	-140	40						
20	6	102	N 3C +1	P5	170	22	25	8	103 W 3P =	C6	-140	40						
20	10	110	N 4C =	P6	620	61	25	6	112 W 3P =	T3	-140	40						
20	9	108	N 4C =	P6	620	61	25	9	105 W 2P =	T2	-110	75						
20	7	104	N 4C =	P6	620	61	25	7	101 O 1P +1	C4	-110	75						
20	4	112	N 4C =	K2	620	61	25	11	109 S 3C -2	K6	-100	90						
20	2	107	N 4C =	P5	620	61	25	3	106 W 3SA -1	C5	100	100						
20	1	105	N 4C =	P5	620	61	26	13	113 O 3C =	PA	-140	10						
20	3	109	N 4C +1	P5	650	100	26	12	111 O 2C +1	PA	-140	10						
21	3	108	S 2SA -2	CK	-200	0	26	9	105 O 3C =	PA	-140	10						
21	7	103	W 2C +2	TB	-170	10	26	11	109 S 2P -1	C5	-100	35						
21	9	107	W 2C +1	TB	-140	20	26	8	103 S 3P -1	C8	-100	35						
21	11	111	W 2C =	TB	-110	40	26	3	106 O 3C -1	PA	100	50						
21	4	110	W 2C =	TB	-110	40	26	10	107 S 2P =	TK	110	65						
21	2	106	W 2C =	KD	-110	40	26	4	108 S 2P =	C7	110	65						
21	8	105	S 1SA -1	C9	-100	65	26	7	101 S 2P +1	TK	140	85						
21	1	104	S 3T -1	K4	-100	65	26	5	110 S 2P +1	TK	140	85						
21	6	101	W 3C -1	KD	50	85	26	6	112 O 4C -2	PA	200	100						
21	5	113	W 3C -1	TB	50	85	27	4	107 N 4C -3	P4	-150	0						
21	10	109	W 3C -2	TB	100	100	27	9	104 N 4C -2	K9	-100	11						
22	11	111	W 4P =	T3	-620	0	27	12	110 N 4P -1	K9	-50	28						
22	5	113	W 3SA =	P5	-600	10	27	6	111 S 3C -1	T4	-50	28						
22	9	107	W 2SA +1	T5	-150	25	27	11	108 N 2C +1	T8	140	50						
22	8	105	W 2SA +1	T5	-150	25	27	7	113 N 3P =	TA	140	50						
22	4	110	O 2SA =	CK	-120	40	27	13	112 N 4P =	TA	420	83						
22	10	109	W 4P -1	K8	100	70	27	10	106 N 4P =	C2	420	83						
22	7	103	W 4P -1	K8	100	70	27	8	102 N 4C =	T8	420	83						

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbiter-Entscheiden berechnet.