

NS-Resultate Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 09.09.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
1	1	101	N 1K =	C9	70	20	16	3	113 O 1SA +1	C2	-120	50	1	6	111 N 1K +3	C6	130	50
2	1	101	S 1C +1	PB	110	80	17	3	112 N 4C -1	TA	-50	60	2	6	111 N 1SA -1	P5	-100	30
3	1	115	W 2SA +4	K5	-240	0	18	3	112 O 4P -3	CA	150	75	11	6	106 W 2P =	C10	-110	70
4	1	115	W 4C +2	TD	-680	30	19	3	111 W 3SA -2	K3	200	80	12	6	106 W 2C -1	KD	50	95
5	1	114	S 4T =	C2	130	80	20	3	111 N 5K =	CA	600	65	13	6	105 N 3SA +2	T8	660	85
6	1	114	O 3K =	T4	-110	15	21	3	110 N 4C +1	K2	650	75	14	6	105 S 3SA -1	KB	-50	55
7	1	113	S 2C =	T10	110	100	22	3	110 W 1SA +1	T3	-120	30	15	6	104 W 3SA -2	CB	100	90
8	1	113	S 4P =	P7	420	95	23	3	109 S 3SA -2	T2	-200	20	16	6	104 O 1SA -1	TB	100	85
9	1	112	N 3C -2	TD	-100	80	24	3	109 W 4C =	P4	-420	10	17	6	103 W 3P =	CA	-140	15
10	1	112	W 3P X -2	CA	500	75	25	3	108 W 3SA +1	K5	-630	30	18	6	103 S 2C +3	TB	200	90
11	1	111	W 2P +1	T3	-140	55	26	3	108 W 4P +2	K3	-680	55	19	6	102 W 2SA -2	T2	200	80
12	1	111	W 1SA =	T2	-90	70	7	4	104 O 2K +1	TB	-110	60	20	6	102 N 3SA +1	P10	630	85
13	1	110	S 3SA +1	C5	630	65	8	4	104 O 5K -2	PA	100	40	21	6	101 N 4C -1	TK	-100	5
14	1	110	S 2SA -3	KB	-150	10	9	4	103 W 3T +2	CA	-150	55	22	6	101 O 1SA +1	CB	-120	30
15	1	109	O 3SA =	C6	-400	30	10	4	103 S 3P X -3	C3	-800	0	23	6	115 N 3SA =	C8	600	90
16	1	109	O 1SA +1	TB	-120	50	11	4	102 W 4P =	KA	-420	15	24	6	115 W 3C -1	T5	50	70
17	1	108	N 3C =	PK	140	100	12	4	102 W 2C =	K6	-110	25	25	6	114 W 3SA =	P4	-600	60
18	1	108	N 2C X +2	KK	1070	100	13	4	101 N 2K +2	TK	130	30	26	6	114 O 4C =	P6	-620	90
19	1	107	W 1SA +1	K3	-120	5	14	4	101 O 3K -1	TA	50	75	27	6	113 W 4P =	KD	-420	55
20	1	107	S 3SA +3	P5	690	100	15	4	115 W 3P -2	CB	100	90	28	6	113 S 2P -1	T3	-100	45
21	1	106	N 2C +2	K2	170	20	16	4	115 O 2C =	K9	-110	70	29	6	112 N 1SA +3	C9	180	70
22	1	106	O 2SA =	P3	-120	30	17	4	114 W 3P -1	CA	50	90	30	6	112 W 4C +1	K7	-450	80
3	2	102	O 3SA -1	P5	100	85	18	4	114 N 3C =	PA	140	45	1	7	113 S 4C +1	T7	450	80
4	2	102	W 4C +2	P8	-680	30	19	4	113 W 2SA -2	TB	200	80	2	7	113 S 2C =	KB	110	80
5	2	101	O 3C =	TA	-140	10	20	4	113 N 5K =	T4	600	65	3	7	112 N 2P -2	CB	-100	55
6	2	101	S 2C -2	P3	-100	35	21	4	112 N 4C =	K2	620	40	4	7	112 W 4C +2	TD	-680	30
7	2	115	S 3C -2	K5	-200	40	22	4	112 O 2SA -1	P3	100	90	13	7	107 S 3SA +3	P6	690	100
8	2	115	S 2P +1	K5	140	60	23	4	111 N 3K +1	C7	130	80	14	7	107 N 4C -2	P6	-100	40
9	2	114	O 3T +2	K5	-150	55	24	4	111 O 4C -1	P3	50	70	15	7	106 O 3SA +2	P6	-460	5
10	2	114	S 3T -1	PA	-100	20	25	4	110 W 3SA =	KA	-600	60	16	7	106 O 1SA +2	P4	-150	15
11	2	113	W 2P -1	TB	50	85	26	4	110 O 6C =	KA	-1430	5	17	7	105 N 3C -1	PK	-50	60
12	2	113	S 1SA -1	PA	-100	50	27	4	109 W 4P +1	C8	-450	15	18	7	105 N 3C =	PA	140	45
13	2	112	S 3SA +1	CA	630	65	28	4	109 O 3C -1	K9	50	70	19	7	104 W 4P -1	TB	100	35
14	2	112	S 3SA +1	CA	430	100	9	5	105 N 2C -1	T5	-50	90	20	7	104 N 2K +1	P10	110	20
15	2	111	O 3SA +1	P6	-430	20	10	5	105 S 3T +1	PA	130	45	21	7	103 S 3SA -1	P8	-100	5
16	2	111	O 2SA =	T5	-120	50	11	5	104 W 3P -1	C9	50	85	22	7	103 O 1SA -1	KD	100	90
17	2	110	W 3P =	CA	-140	15	12	5	104 W 1SA +1	KB	-120	10	23	7	102 S 3SA -2	T4	-200	20
18	2	110	N 2C +1	PA	140	45	13	5	103 S 2P +2	C4	170	50	24	7	102 W 4C =	T5	-420	10
19	2	109	W 3SA -2	TB	200	80	14	5	103 N 3SA -3	CB	-150	10	25	7	101 W 3SA +1	P4	-630	30
20	2	109	S 3K +2	P10	150	40	15	5	102 W 3SA +2	C9	-460	5	26	7	101 O 4C +3	P4	-710	25
21	2	108	N 4C +1	K2	650	75	16	5	102 O 1SA +2	C2	-150	15	27	7	115 W 4P -1	C5	50	100
22	2	108	O 1SA +2	P7	-150	0	17	5	101 W 3P =	CA	-140	15	28	7	115 S 2P -1	T3	-100	45
23	2	107	S 3SA -1	T5	-100	45	18	5	101 O 1SA -1	T5	50	0	29	7	114 W 2P +1	KD	-140	10
24	2	107	W 3C =	T6	-140	45	19	5	115 W 3P -1	TB	100	35	30	7	114 W 4C +3	K7	-510	15
5	3	103	O 3P =	TA	-140	10	20	5	115 N 3K +2	C10	150	40	1	8	115 S 4C =	T7	420	60
6	3	103	O 3K -1	C9	100	70	21	5	114 N 4C +1	K2	650	75	2	8	115 O 2P =	K9	-110	15
7	3	102	S 2C -1	T10	-100	75	22	5	114 O 1SA +1	P3	-120	30	3	8	114 S 2P -1	CA	-50	70
8	3	102	S 4P X -1	K10	-100	10	23	5	113 S 3SA -2	K9	-200	20	4	8	114 W 4C +2	PD	-680	30
9	3	101	W 3SA =	K4	-600	0	24	5	113 W 4C -2	PD	100	95	5	8	113 S 4T -1	P10	-100	30
10	3	101	W 3C -2	P2	200	60	25	5	112 W 3SA +1	KA	-630	30	6	8	113 N 2SA -1	PA	-50	50
11	3	115	W 4P =	TK	-420	15	26	5	112 W 4P +2	KB	-680	55	15	8	108 W 3T +2	CB	-150	50
12	3	115	W 2C =	K6	-110	25	27	5	111 N 4C -3	T10	-150	90	16	8	108 O 3SA -2	TB	200	100
13	3	114	N 2K +1	P8	110	10	28	5	111 W 4C -1	KA	50	70	17	8	107 N 4C -1	PD	-50	60
14	3	114	N 3SA -3	CB	-150	10	29	5	110 O 2SA -1	TA	100	45	18	8	107 O 4P -3	T4	150	75
15	3	113	W 1P +1	C7	-110	60	30	5	110 W 4C +2	K7	-480	40	19	8	106 N 1T X =	PA	140	50

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	
20	8	106	O 3P -1	KA	100	10	1	11	106 S 4C +1	T7	450	80	12	13	105 O 1P =	C4	-80	80
21	8	105	S 3SA +2	P7	660	100	2	11	106 W 1SA -2	T2	100	60	13	13	104 N 2SA =	TK	120	20
22	8	105	O 1SA =	P3	-90	70	3	11	105 N 2K -2	C7	-100	55	14	13	104 N 3T -1	CB	-50	55
23	8	104	S 3SA -3	T2	-300	0	4	11	105 W 4C =	P3	-620	80	15	13	103 O 3SA -2	C3	100	90
24	8	104	W 4C -1	P4	50	70	5	11	104 W 3C X -2	TD	300	90	16	13	103 O 2C -1	K9	100	85
25	8	103	W 3SA +2	KA	-660	5	6	11	104 O 5K X -1	P8	200	95	25	13	113 O 3SA =	C6	-600	60
26	8	103	O 6P =	C8	-1430	5	7	11	103 W 2P -1	KA	100	90	26	13	113 W 4P +2	K2	-680	55
27	8	102	W 4P =	C5	-420	55	8	11	103 S 4P =	K8	420	95	27	13	112 W 3P +1	C3	-170	80
28	8	102	O 3C =	PK	-140	10	9	11	102 O 3T +3	P4	-170	25	28	13	112 S 4P -3	T3	-300	0
29	8	101	W 3P -1	CK	100	45	10	11	102 S 1P +1	C2	110	30	29	13	111 O 2C -2	TA	200	85
30	8	101	W 4C +1	K7	-450	80	11	11	101 W 4P =	T3	-420	15	30	13	111 W 4C +1	K4	-450	80
1	9	102	N 1P -1	C9	-50	5	12	11	101 O 1P -1	KA	50	95	1	14	112 N 1K +1	C9	90	30
2	9	102	W 3K -1	P9	50	40	21	11	111 N 4C +1	T6	650	75	2	14	112 O 2P =	K9	-110	15
3	9	101	W 2C +3	T9	-200	10	22	11	111 S 2P -2	C4	-100	60	3	14	111 W 2C +1	T9	-140	30
4	9	101	W 4C +2	TD	-680	30	23	11	110 N 3K =	P5	110	65	4	14	111 W 4C +2	K10	-680	30
5	9	115	W 3C -2	TD	100	60	24	11	110 W 4C =	P3	-420	10	5	14	110 W 3C -2	TD	100	60
6	9	115	O 3K -1	K5	100	70	25	11	109 W 3SA +2	P4	-660	5	6	14	110 N 3SA -2	T10	-100	35
7	9	114	S 3C -1	K7	-100	75	26	11	109 O 5C =	P4	-650	80	7	14	109 S 2SA -3	K4	-300	20
8	9	114	O 4K -1	PA	50	30	27	11	108 W 4P +1	C3	-450	15	8	14	109 S 4P -2	K7	-100	10
17	9	109	W 3P =	CA	-140	15	28	11	108 W 2K +1	P10	-110	25	9	14	108 O 3T +3	K3	-170	25
18	9	109	N 2C +1	PA	140	45	29	11	107 O 1C X -1	TA	200	85	10	14	108 S 4T =	PA	130	45
19	9	108	W 2SA =	TB	-120	5	30	11	107 W 4C +2	K7	-480	40	11	14	107 O 4P X -3	CA	500	100
20	9	108	N 3SA -1	P6	-100	0	1	12	108 N 1K +2	P2	110	40	12	14	107 S 2SA -1	C9	-100	50
21	9	107	N 4C =	TD	620	40	2	12	108 N 1SA =	P5	90	50	13	14	106 S 3SA +2	C5	660	85
22	9	107	O 2SA -1	K3	100	90	3	12	107 W 1C +2	T9	-140	30	14	14	106 O 3K =	TD	-110	30
23	9	106	S 3SA -1	T4	-100	45	4	12	107 W 3C +2	TD	-200	90	15	14	105 N 2C -2	P4	-200	40
24	9	106	W 3C +1	P4	-170	30	5	12	106 O 4P -1	TA	50	40	16	14	105 O 1SA +2	P4	-150	15
25	9	105	W 1SA =	P4	-90	100	6	12	106 O 4K -1	C5	100	70	17	14	104 N 4C -1	PK	-50	60
26	9	105	W 4P +2	K3	-680	55	7	12	105 S 3C -2	K8	-200	40	18	14	104 O 1SA -2	T7	100	15
27	9	104	W 4P +1	C5	-450	15	8	12	105 S 4P -2	K10	-100	10	27	14	114 W 4P =	C8	-420	55
28	9	104	O 3C -1	PK	50	70	9	12	104 O 3T +2	K8	-150	55	28	14	114 W 3K =	P10	-110	25
29	9	103	S 2K +2	C10	130	60	10	12	104 W 4C X -4	P2	1100	100	29	14	113 S 2K =	TD	90	30
30	9	103	W 4C +3	K7	-510	15	11	12	103 W 3P +1	K7	-170	40	30	14	113 O 4C +1	P10	-450	80
1	10	104	N 4C +1	C10	450	80	12	12	103 S 1SA -2	PA	-200	0	1	15	114 N 1K -1	C9	-50	5
2	10	104	S 3T =	CA	110	80	13	12	102 S 3P =	C4	140	40	2	15	114 N 2SA =	K4	120	100
3	10	103	W 3C =	T9	-140	30	14	12	102 W 2K -1	TB	50	75	3	15	113 O 3SA -2	P5	200	100
4	10	103	O 3SA -1	K9	100	100	23	12	112 S 3SA +2	T2	660	100	4	15	113 W 4C +1	T5	-650	70
5	10	102	O 3P =	TA	-140	10	24	12	112 W 4C -2	T5	100	95	5	15	112 W 4P -2	T9	100	60
6	10	102	O 4K -2	P6	200	95	25	12	111 W 2SA +2	C3	-180	85	6	15	112 W 3K =	TA	-110	15
7	10	101	S 2SA -2	K4	-200	40	26	12	111 O 4C +3	P4	-710	25	7	15	111 S 2C -4	T10	-400	5
8	10	101	S 3P +1	K5	170	75	27	12	110 W 4P +1	KD	-450	15	8	15	111 S 3P +1	K10	170	75
9	10	115	O 3T +2	K3	-150	55	28	12	110 O 4C -3	PK	150	100	9	15	110 Pass		0	100
10	10	115	W 4C X -3	P2	800	90	29	12	109 W 2P +1	KD	-140	10	10	15	110 W 2C +1	P2	-140	10
19	10	110	W 3SA -2	TB	200	80	30	12	109 W 6C =	K6	-980	0	11	15	109 W 4P =	KA	-420	15
20	10	110	S 3SA +1	C5	630	85	1	13	110 N 2C X +2	KA	670	100	12	15	109 S 1SA -1	C3	-100	50
21	10	109	N 4C =	K2	620	40	2	13	110 O 2P +1	TA	-140	0	13	15	108 S 3SA -3	C4	-300	0
22	10	109	O 1SA +1	P3	-120	30	3	13	109 O 3SA -1	P5	100	85	14	15	108 N 3SA =	P6	400	90
23	10	108	N 2K +1	T3	110	65	4	13	109 W 4C +2	P10	-680	30	15	15	107 W 3SA -1	CB	50	70
24	10	108	W 3C =	T5	-140	45	5	13	108 W 4C X -3	T9	500	100	16	15	107 O 1SA +2	P4	-150	15
25	10	107	W 2SA +2	P4	-180	85	6	13	108 W 2SA +1	K6	-150	0	17	15	106 N 4C -1	PK	-50	60
26	10	107	W 3P +3	K3	-230	100	7	13	107 S 2SA -4	K8	-400	5	18	15	106 O 1SA -2	T5	100	15
27	10	106	W 4P =	C5	-420	55	8	13	107 S 2P =	K10	110	50	19	15	105 W 1SA =	T2	-90	20
28	10	106	O 4C -2	PK	100	90	9	13	106 O 1SA +3	P4	-180	10	20	15	105 N 2K +3	C8	150	40
29	10	105	W 3P =	KD	-140	10	10	13	106 W 3C X -2	P2	500	75	29	15	115 O 2SA -5	TA	500	100
30	10	105	W 4C +1	PB	-450	80	11	13	105 W 3P =	C3	-140	55	30	15	115 W 4C +2	K4	-480	40

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

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Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
1	1	101	N 1K =	C9	-70	80	14	5	103	N 3SA -3	CB	150	90	1	11	106	S 4C +1	T7	-450	20
2	1	101	S 1C +1	PB	-110	20	15	13	103	O 3SA -2	C3	-100	10	2	11	106	W 1SA -2	T2	-100	40
3	9	101	W 2C +3	T9	200	90	16	13	103	O 2C -1	K9	-100	15	5	12	106	O 4P -1	TA	-50	60
4	9	101	W 4C +2	TD	680	70	17	6	103	W 3P =	CA	140	85	6	12	106	O 4K -1	C5	-100	30
5	2	101	O 3C =	TA	140	90	18	6	103	S 2C +3	TB	-200	10	9	13	106	O 1SA +3	P4	180	90
6	2	101	S 2C -2	P3	100	65	21	7	103	S 3SA -1	P8	100	95	10	13	106	W 3C X -2	P2	-500	25
7	10	101	S 2SA -2	K4	200	60	22	7	103	O 1SA -1	KD	-100	10	11	6	106	W 2P =	C10	110	30
8	10	101	S 3P +1	K5	-170	25	25	8	103	W 3SA +2	KA	660	95	12	6	106	W 2C -1	KD	-50	5
9	3	101	W 3SA =	K4	600	100	26	8	103	O 6P =	C8	1430	95	13	14	106	S 3SA +2	C5	-660	15
10	3	101	W 3C -2	P2	-200	40	29	9	103	S 2K +2	C10	-130	40	14	14	106	O 3K =	TD	110	70
11	11	101	W 4P =	T3	420	85	30	9	103	W 4C +3	K7	510	85	15	7	106	O 3SA +2	P6	460	95
12	11	101	O 1P -1	KA	-50	5	1	10	104	N 4C +1	C10	-450	20	16	7	106	O 1SA +2	P4	150	85
13	4	101	N 2K +2	TK	-130	70	2	10	104	S 3T =	CA	-110	20	17	15	106	N 4C -1	PK	50	40
14	4	101	O 3K -1	TA	-50	25	5	11	104	W 3C X -2	TD	-300	10	18	15	106	O 1SA -2	T5	-100	85
17	5	101	W 3P =	CA	140	85	6	11	104	O 5K X -1	P8	-200	5	19	8	106	N 1T X =	PA	-140	50
18	5	101	O 1SA -1	T5	-50	100	7	4	104	O 2K +1	TB	110	40	20	8	106	O 3P -1	KA	-100	90
21	6	101	N 4C -1	TK	100	95	8	4	104	O 5K -2	PA	-100	60	21	1	106	N 2C +2	K2	-170	80
22	6	101	O 1SA +1	CB	120	70	9	12	104	O 3T +2	K8	150	45	22	1	106	O 2SA =	P3	120	70
25	7	101	W 3SA +1	P4	630	70	10	12	104	W 4C X -4	P2	-1100	0	23	9	106	S 3SA -1	T4	100	55
26	7	101	O 4C +3	P4	710	75	11	5	104	W 3P -1	C9	-50	15	24	9	106	W 3C +1	P4	170	70
29	8	101	W 3P -1	CK	-100	55	12	5	104	W 1SA +1	KB	120	90	27	10	106	W 4P =	C5	420	45
30	8	101	W 4C +1	K7	450	20	13	13	104	N 2SA =	TK	-120	80	28	10	106	O 4C -2	PK	-100	10
1	9	102	N 1P -1	C9	50	95	14	13	104	N 3T -1	CB	50	45	3	12	107	W 1C +2	T9	140	70
2	9	102	W 3K -1	P9	-50	60	15	6	104	W 3SA -2	CB	-100	10	4	12	107	W 3C +2	TD	200	10
3	2	102	O 3SA -1	P5	-100	15	16	6	104	O 1SA -1	TB	-100	15	7	13	107	S 2SA -4	K8	400	95
4	2	102	W 4C +2	P8	680	70	17	14	104	N 4C -1	PK	50	40	8	13	107	S 2P =	K10	-110	50
5	10	102	O 3P =	TA	140	90	18	14	104	O 1SA -2	T7	-100	85	11	14	107	O 4P X -3	CA	-500	0
6	10	102	O 4K -2	P6	-200	5	19	7	104	W 4P -1	TB	-100	65	12	14	107	S 2SA -1	C9	100	50
7	3	102	S 2C -1	T10	100	25	20	7	104	N 2K +1	P10	-110	80	13	7	107	S 3SA +3	P6	-690	0
8	3	102	S 4P X -1	K10	100	90	23	8	104	S 3SA -3	T2	300	100	14	7	107	N 4C -2	P6	100	60
9	11	102	O 3T +3	P4	170	75	24	8	104	W 4C -1	P4	-50	30	15	15	107	W 3SA -1	CB	-50	30
10	11	102	S 1P +1	C2	-110	70	27	9	104	W 4P +1	C5	450	85	16	15	107	O 1SA +2	P4	150	85
11	4	102	W 4P =	KA	420	85	28	9	104	O 3C -1	PK	-50	30	17	8	107	N 4C -1	PD	50	40
12	4	102	W 2C =	K6	110	75	3	11	105	N 2K -2	C7	100	45	18	8	107	O 4P -3	T4	-150	25
13	12	102	S 3P =	C4	-140	60	4	11	105	W 4C =	P3	620	20	19	1	107	W 1SA +1	K3	120	95
14	12	102	W 2K -1	TB	-50	25	7	12	105	S 3C -2	K8	200	60	20	1	107	S 3SA +3	P5	-690	0
15	5	102	W 3SA +2	C9	460	95	8	12	105	S 4P -2	K10	100	90	21	9	107	N 4C =	TD	-620	60
16	5	102	O 1SA +2	C2	150	85	9	5	105	N 2C -1	T5	50	10	22	9	107	O 2SA -1	K3	-100	10
19	6	102	W 2SA -2	T2	-200	20	10	5	105	S 3T +1	PA	-130	55	23	2	107	S 3SA -1	T5	100	55
20	6	102	N 3SA +1	P10	-630	15	11	13	105	W 3P =	C3	140	45	24	2	107	W 3C =	T6	140	55
23	7	102	S 3SA -2	T4	200	80	12	13	105	O 1P =	C4	80	20	25	10	107	W 2SA +2	P4	180	15
24	7	102	W 4C =	T5	420	90	13	6	105	N 3SA +2	T8	-660	15	26	10	107	W 3P +3	K3	230	0
27	8	102	W 4P =	C5	420	45	14	6	105	S 3SA -1	KB	50	45	29	11	107	O 1C X -1	TA	-200	15
28	8	102	O 3C =	PK	140	90	15	14	105	N 2C -2	P4	200	60	30	11	107	W 4C +2	K7	480	60
3	10	103	W 3C =	T9	140	70	16	14	105	O 1SA +2	P4	150	85	1	12	108	N 1K +2	P2	-110	60
4	10	103	O 3SA -1	K9	-100	0	17	7	105	N 3C -1	PK	50	40	2	12	108	N 1SA =	P5	-90	50
5	3	103	O 3P =	TA	140	90	18	7	105	N 3C =	PA	-140	55	5	13	108	W 4C X -3	T9	-500	0
6	3	103	O 3K -1	C9	-100	30	19	15	105	W 1SA =	T2	90	80	6	13	108	W 2SA +1	K6	150	100
7	11	103	W 2P -1	KA	-100	10	20	15	105	N 2K +3	C8	-150	60	9	14	108	O 3T +3	K3	170	75
8	11	103	S 4P =	K8	-420	5	21	8	105	S 3SA +2	P7	-660	0	10	14	108	S 4T =	PA	-130	55
9	4	103	W 3T +2	CA	150	45	22	8	105	O 1SA =	P3	90	30	13	15	108	S 3SA -3	C4	300	100
10	4	103	S 3P X -3	C3	800	100	25	9	105	W 1SA =	P4	90	0	14	15	108	N 3SA =	P6	-400	10
11	12	103	W 3P +1	K7	170	60	26	9	105	W 4P +2	K3	680	45	15	8	108	W 3T +2	CB	150	50
12	12	103	S 1SA -2	PA	200	100	29	10	105	W 3P =	KD	140	90	16	8	108	O 3SA -2	TB	-200	0
13	5	103	S 2P +2	C4	-170	50	30	10	105	W 4C +1	PB	450	20	17	1	108	N 3C =	PK	-140	0

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.

OW-Resultate Mitchell-Turnier Dienstag - Pfäffikon, Mensa - 09.09.2014

Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz	Bd	NS	OW	ASpKonErgAus	Sco	Prz			
18	1	108	N 2C X +2	KK	-1070	0	1	6	111	N 1K +3	C6	-130	50	16	3	113	O 1SA +1	C2	120	50
19	9	108	W 2SA =	TB	120	95	2	6	111	N 1SA -1	P5	100	70	19	4	113	W 2SA -2	TB	-200	20
20	9	108	N 3SA -1	P6	100	100	3	14	111	W 2C +1	T9	140	70	20	4	113	N 5K =	T4	-600	35
21	2	108	N 4C +1	K2	-650	25	4	14	111	W 4C +2	K10	680	70	23	5	113	S 3SA -2	K9	200	80
22	2	108	O 1SA +2	P7	150	100	7	15	111	S 2C -4	T10	400	95	24	5	113	W 4C -2	PD	-100	5
23	10	108	N 2K +1	T3	-110	35	8	15	111	S 3P +1	K10	-170	25	25	13	113	O 3SA =	C6	600	40
24	10	108	W 3C =	T5	140	55	11	1	111	W 2P +1	T3	140	45	26	13	113	W 4P +2	K2	680	45
25	3	108	W 3SA +1	K5	630	70	12	1	111	W 1SA =	T2	90	30	27	6	113	W 4P =	KD	420	45
26	3	108	W 4P +2	K3	680	45	15	2	111	O 3SA +1	P6	430	80	28	6	113	S 2P -1	T3	100	55
27	11	108	W 4P +1	C3	450	85	16	2	111	O 2SA =	T5	120	50	29	14	113	S 2K =	TD	-90	70
28	11	108	W 2K +1	P10	110	75	19	3	111	W 3SA -2	K3	-200	20	30	14	113	O 4C +1	P10	450	20
3	13	109	O 3SA -1	P5	-100	15	20	3	111	N 5K =	CA	-600	35	1	15	114	N 1K -1	C9	50	95
4	13	109	W 4C +2	P10	680	70	21	11	111	N 4C +1	T6	-650	25	2	15	114	N 2SA =	K4	-120	0
7	14	109	S 2SA -3	K4	300	80	22	11	111	S 2P -2	C4	100	40	3	8	114	S 2P -1	CA	50	30
8	14	109	S 4P -2	K7	100	90	23	4	111	N 3K +1	C7	-130	20	4	8	114	W 4C +2	PD	680	70
11	15	109	W 4P =	KA	420	85	24	4	111	O 4C -1	P3	-50	30	5	1	114	S 4T =	C2	-130	20
12	15	109	S 1SA -1	C3	100	50	25	12	111	W 2SA +2	C3	180	15	6	1	114	O 3K =	T4	110	85
15	1	109	O 3SA =	C6	400	70	26	12	111	O 4C +3	P4	710	75	7	9	114	S 3C -1	K7	100	25
16	1	109	O 1SA +1	TB	120	50	27	5	111	N 4C -3	T10	150	10	8	9	114	O 4K -1	PA	-50	70
17	9	109	W 3P =	CA	140	85	28	5	111	W 4C -1	KA	-50	30	9	2	114	O 3T +2	K5	150	45
18	9	109	N 2C +1	PA	-140	55	29	13	111	O 2C -2	TA	-200	15	10	2	114	S 3T -1	PA	100	80
19	2	109	W 3SA -2	TB	-200	20	30	13	111	W 4C +1	K4	450	20	13	3	114	N 2K +1	P8	-110	90
20	2	109	S 3K +2	P10	-150	60	1	14	112	N 1K +1	C9	-90	70	14	3	114	N 3SA -3	CB	150	90
21	10	109	N 4C =	K2	-620	60	2	14	112	O 2P =	K9	110	85	17	4	114	W 3P -1	CA	-50	10
22	10	109	O 1SA +1	P3	120	70	3	7	112	N 2P -2	CB	100	45	18	4	114	N 3C =	PA	-140	55
23	3	109	S 3SA -2	T2	200	80	4	7	112	W 4C +2	TD	680	70	21	5	114	N 4C +1	K2	-650	25
24	3	109	W 4C =	P4	420	90	5	15	112	W 4P -2	T9	-100	40	22	5	114	O 1SA +1	P3	120	70
25	11	109	W 3SA +2	P4	660	95	6	15	112	W 3K =	TA	110	85	25	6	114	W 3SA =	P4	600	40
26	11	109	O 5C =	P4	650	20	9	1	112	N 3C -2	TD	100	20	26	6	114	O 4C =	P6	620	10
27	4	109	W 4P +1	C8	450	85	10	1	112	W 3P X -2	CA	-500	25	27	14	114	W 4P =	C8	420	45
28	4	109	O 3C -1	K9	-50	30	13	2	112	S 3SA +1	CA	-630	35	28	14	114	W 3K =	P10	110	75
29	12	109	W 2P +1	KD	140	90	14	2	112	S 3SA +1	CA	-430	0	29	7	114	W 2P +1	KD	140	90
30	12	109	W 6C =	K6	980	100	17	3	112	N 4C -1	TA	50	40	30	7	114	W 4C +3	K7	510	85
1	13	110	N 2C X +2	KA	-670	0	18	3	112	O 4P -3	CA	-150	25	1	8	115	S 4C =	T7	-420	40
2	13	110	O 2P +1	TA	140	100	21	4	112	N 4C =	K2	-620	60	2	8	115	O 2P =	K9	110	85
5	14	110	W 3C -2	TD	-100	40	22	4	112	O 2SA -1	P3	-100	10	3	1	115	W 2SA +4	K5	240	100
6	14	110	N 3SA -2	T10	100	65	23	12	112	S 3SA +2	T2	-660	0	4	1	115	W 4C +2	TD	680	70
9	15	110	Pass		0	0	24	12	112	W 4C -2	T5	-100	5	5	9	115	W 3C -2	TD	-100	40
10	15	110	W 2C +1	P2	140	90	25	5	112	W 3SA +1	KA	630	70	6	9	115	O 3K -1	K5	-100	30
13	1	110	S 3SA +1	C5	-630	35	26	5	112	W 4P +2	KB	680	45	7	2	115	S 3C -2	K5	200	60
14	1	110	S 2SA -3	KB	150	90	27	13	112	W 3P +1	C3	170	20	8	2	115	S 2P +1	K5	-140	40
17	2	110	W 3P =	CA	140	85	28	13	112	S 4P -3	T3	300	100	9	10	115	O 3T +2	K3	150	45
18	2	110	N 2C +1	PA	-140	55	29	6	112	N 1SA +3	C9	-180	30	10	10	115	W 4C X -3	P2	-800	10
19	10	110	W 3SA -2	TB	-200	20	30	6	112	W 4C +1	K7	450	20	11	3	115	W 4P =	TK	420	85
20	10	110	S 3SA +1	C5	-630	15	1	7	113	S 4C +1	T7	-450	20	12	3	115	W 2C =	K6	110	75
21	3	110	N 4C +1	K2	-650	25	2	7	113	S 2C =	KB	-110	20	15	4	115	W 3P -2	CB	-100	10
22	3	110	W 1SA +1	T3	120	70	3	15	113	O 3SA -2	P5	-200	0	16	4	115	O 2C =	K9	110	30
23	11	110	N 3K =	P5	-110	35	4	15	113	W 4C +1	T5	650	30	19	5	115	W 3P -1	TB	-100	65
24	11	110	W 4C =	P3	420	90	5	8	113	S 4T -1	P10	100	70	20	5	115	N 3K +2	C10	-150	60
25	4	110	W 3SA =	KA	600	40	6	8	113	N 2SA -1	PA	50	50	23	6	115	N 3SA =	C8	-600	10
26	4	110	O 6C =	KA	1430	95	7	1	113	S 2C =	T10	-110	0	24	6	115	W 3C -1	T5	-50	30
27	12	110	W 4P +1	KD	450	85	8	1	113	S 4P =	P7	-420	5	27	7	115	W 4P -1	C5	-50	0
28	12	110	O 4C -3	PK	-150	0	11	2	113	W 2P -1	TB	-50	15	28	7	115	S 2P -1	T3	100	55
29	5	110	O 2SA -1	TA	-100	55	12	2	113	S 1SA -1	PA	100	50	29	15	115	O 2SA -5	TA	-500	0
30	5	110	W 4C +2	K7	480	60	15	3	113	W 1P +1	C7	110	40	30	15	115	W 4C +2	K4	480	60

Die Prozentwerte sind ohne Anwendung der Neuberg-Formel und ohne Einfluss von Arbitr-Entscheiden berechnet.